LEVEL II PORTLAND CEMENT CONCRETE

2007-2008

INSTRUCTION MANUAL









TECHNICAL
TRAINING &
CERTIFICATION
PROGRAM



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LEVEL II PCC GLOSSARY

Absolute Volume – Space occupied by materials in a cubic yard of concrete.

Absorption – The condition of an aggregate when all of the aggregate's pores are not full so it can absorb water.

Accelerator – A chemical admixture used to speed up the set of cement in a concrete mixture.

Aggregate - Sand, rock, or gravel used as a portion of a concrete mixture.

Air – A chemical admixture used in concrete to produce air voids.

Batch – One cubic yard of concrete. When on a project you may hear someone reference a batch of concrete as the total cubic yards of concrete being mixed at one time but for this training a batch of concrete is considered one cubic yard.

Cement – The fine gray powder that holds aggregates together in a concrete mixture.

Chemical Admixture – A chemical (air, water reducer, etc.) that is added to concrete to produce varying results on the concrete.

Concrete - A mass of sand and rock bound together by cementitous materials.

Dry Batch Weights – The weights of the aggregate, cementitous materials, and water calculated from the absolute volumes and specific gravities before the aggregate weights are adjusted for moisture content.

Fly Ash – A common mineral admixture used in concrete mixtures. Fly ash is a by-product of the burning of finely ground coal in electricity generating power plants. The two types of fly ash are Type C (cementitous) or Type F (non-cementitous).

Free Moisture – The excess water on an aggregate after the aggregate is completely saturated.

Ground Granulated Blast Furnace Slag (GGBFS) – A mineral admixture that is a byproduct of steel production. GGBFS is made from slag floating on top of an iron blast furnace.

Instructional Memorandum (IM) – Four volumes of manuals issued by the Iowa DOT Materials Department containing specifications on material's inspection and testing.

Load – The total amount of concrete being batched out.

Lot System – The system used in the decision of when to sample materials i.e., in a paving plant a lot is one day's run.

Pozzolan – A finely divided, siliceous or aluminosiliceous material that reacts with water and calcium hydroxide released by Portland cement hydration to form cementing compounds.

Retarder – A chemical admixture used to delay the set of cement in a concrete mixture.

Saturated Surface Dry – The condition of an aggregate when it contains all the water it can hold but has no moisture on the surface.

Specific Gravity – The ratio of the density of water to the density of a material.

Water to Cement Ratio (W/C) – The ratio of the amount of water in a batch of concrete to the amount of cement. Maximum W/C is the highest ratio of water and cement that can be used in concrete and still be within specification.

Water Reducer – A chemical admixture used in concrete to reduce the amount of water required to produce slump which allows the lowering of the amount of cement required.

Wet Batch Weights – The weights of the ingredients of a batch of concrete after the aggregate weights have been adjusted for moisture.

ROUNDING & DECIMALS

Rounding is uniform throughout the certification training. You would look at the place to the right of the number you are rounding to and if it is 5 or above round up or 4 and below it remains the same.

Examples:

Rounding to whole numbers-

Rounding to tenths-

Rounding to hundredths-

Rounding to thousandths-

There are many equations used in Level II PCC to obtain percentages, weights, ratios, etc. The answers to these equations are expressed with the decimals in different locations. The following is a listing of how many places to round each answer.

Specific Gravity – hundredths – 2.62 2.77

Moisture – tenths – 2.7 0.6

Air – tenths – 6.5 5.8

Slump - $\frac{1}{4}$ inch - $\frac{3}{2}$ 2 $\frac{3}{4}$

Beam size – hundredths – 6.02 5.98

Absolute Volumes – thousandths - .082 .334

Water Cement Ratio (W/C) – thousandths - .480 .468

Cement Yield – tenths – 99.7 100.3

Pounds (lbs) - whole - 1450 385

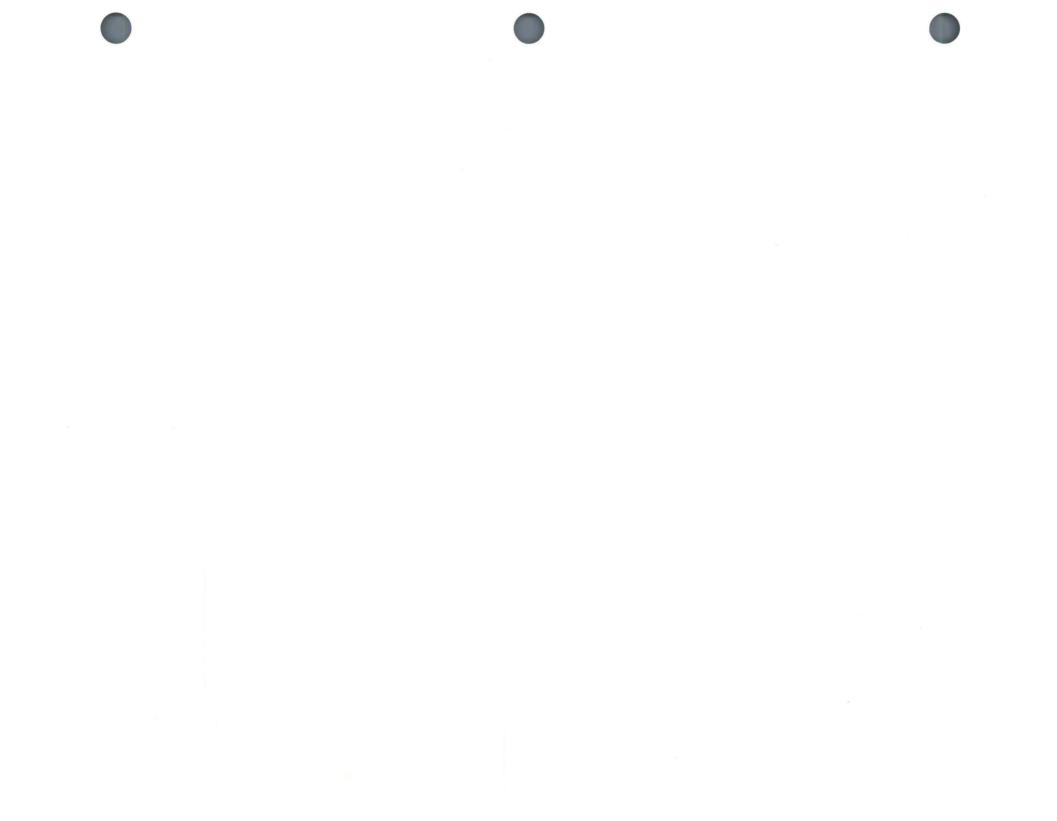
Gallon (gal) – whole - 28 34

Cement Tons - hundredths - 117.0 54.50

Cubic Yards – hundredths – 117.00 54.50 (Concrete is batched in ½ cubic yard increments)

There will be given numbers that are used in calculations that may be rounded differently than shown above. When given a number for use in a calculation, use the number in the form required. For example: 8.33 lbs./gal; 62.4 lbs. = unit weight of water, etc.





PCC Level II Introduction

I. Introduction

This course is intended for the training of Certified Concrete Plant Technicians. The training manual that accompanies this course has been prepared to provide assistance not only for classroom use, but also as a self-training manual and a reference to be used in the field.

At the beginning of each section, references are given to:

- Iowa Department of Transportation Standard Specifications with the Specification Article listed
- Materials Instructional Memorandums (IM)

These references will enable the Certified Plant Technician to refer to those documents for more detailed information. The actual documents are not included in this material because they are periodically updated. The documents are included in the PCC Reference Book. The PCC Reference Book is a good tool for technicians and contains the IMs and Specifications needed to perform inspection and testing of Portland Cement Concrete. **NOTE:** IMs and Specifications are updated each spring and fall and the technician should always make sure the most current IMs and specifications are in the Reference Book



Remember to check for IM and Specification changes each spring and fall to update your PCC Reference Manual







II. Certification Program for Certified Plant Technicians

IM 213

A. Requirements

The requirements for obtaining a Certified Portland Cement Concrete Plant Technician Level II certification are:

- Certification in Level I and Level II Aggregate
- Certification in Level I PCC Concrete Testing
- A score of at least 80% on the Level II PCC Exam

In addition to the above requirements, recommended experience includes:

- Performing Gradation Tests
- Performing Moisture Tests
- · Calculating Batch Weights
- Performing Specific Gravity Tests
- Checking Slump, Air and Flexural Strength
- Maturity Meter Testing
- Checking Tolerances and Sensitivity of Scales
- Complete Plant Inspection: Stockpiling, Admixture Dispensers, Scales, etc.
- Completing Reports
- Keeping Proper Records and Plant Diaries

The Technician should have experience performing the above duties under a certified technician before performing plant inspection duties on their own.

B. Certifications

Certifications are issued by the Program Director (Director of the Office of Materials) in mid-May. The Certified Plant Technician's Certification Number will be the same as their Aggregate Certification Number.

Certifications are issued for a five-year period, but if two updates are not obtained in that five-year period, the applicant must retake all applicable schooling, as opposed to taking a refresher course.



If two updates are not obtained in a five-year period, the applicant must retake the entire course! Refer to I.M. 213 for details

C. Performance Requirements

Suspension of Certification

A Certified Technician will be suspended for unsatisfactory and/or inadequate performance. (See Unsatisfactory Performance form on the following page)

- After 2 such notices, a technician will receive a three-month suspension
- A third notice will result in Decertification.

Technician Decertification

A Technician's Certificate will become invalid for any one of the following:

- Failure to renew the Certificate prior to regular expiration
- Use of false or fraudulent information to secure or renew
- False or fraudulent actions or documentation
- Not performing tests and duties properly in accordance with specifications

Federal Code 1020, Iowa Code 714.8

Certified Technicians need to be aware of the consequence of issuing a false statement (refer to Codes on pages 2-4 and 2-5)

D. Responsibilities

IM 213

The Certified Plant Technician will:

- Sample
- Test
- Perform prescribed inspections, all at the specified frequencies
- Be responsible for quality control

The Project Engineer will:

- Be responsible for monitoring inspections
- · Be responsible for verification

UNSATISFACTORY PERFORMANCE NOTICE

Issued To:	Date:
	performance as a Certified tory for the reason(s) listed below. After receipt a three-month suspension. After three notices,
This notice will be placed in your per which you reside. It will also be place	manent file with the District Materials Office in ed on the statewide computer file.
contractors, producers, cities, and co lowa's construction projects. We hop	nd Certification Program (TTCP) is to work with bunties to continually improve the quality of pe you will work with us to achieve this goal.
Unsatisfactory Performance:	
	District Materials Engineer

cc: Program Director – Materials Engineer Ames TTCP Coordinator Resident Construction Engineer



FEDERAL CODE 1020 and IOWA CODE 714.8

IM 213 discusses the Unsatisfactory Notice that Certified Technicians are given when they are not performing their job duties satisfactorily. This can be given for a number of reasons including, improper sampling and/or testing, not performing their duties and reporting in the time frame required, reporting incorrect information, etc. The technician is given one written notice, the second notice is three-month certification suspension, and the third notice is decertification. According to IM 213 the Certified Technician can automatically be decertified for false statements without going through the Unsatisfactory Notice procedure. The Certified Technician also needs to be aware of the false statement clause that is applicable to all federal-aid projects and the fraudulent practice clause that applies to all non-federal aid projects. Certified Technicians need to read and be aware of U.S.C. 1020 and Iowa Code 714.8 since these do apply to them. They read as follows:

FEDERAL AID PROJECTS

IX. FALSE STATEMENTS CONCERNING HIGHWAY PROJECTS

In order to assure high quality and durable construction in conformity with approved plans and specifications and a high degree of reliability on statements and representations made by engineers, contractors, suppliers, and workers on Federal-aid highway projects, it is essential that all persons concerned with the project perform their functions as carefully, thoroughly, and honestly as possible. Willful falsification, distortion, or misrepresentation with respect to any facts related to the project is a violation of Federal law. To prevent any misunderstanding regarding the seriousness of these and similar acts, the following notice shall be posted on each Federal-aid highway project (23 CFR 635) in one or more places where it is readily available to all persons concerned with the project:

NOTICE TO ALL PERSONNEL ENGAGED ON FEDERAL-AID HIGHWAY PROJECTS

18 U.S.C. 1020 reads as follows:

"Whoever, being an officer, agent, or employee of the United States, or of any State or Territory, or whoever, whether a person, association, firm, or corporation, knowingly makes any false statement, false representation, or false report as to the character, quality, quantity, or cost of the material used or to be used, or the quantity or quality of work performed or to be performed, or the cost thereof in connection with the submission of plans, maps, specifications, contracts, or costs of construction on any highway or related project submitted for approval to the Secretary of Transportation; or

Whoever knowingly makes any false statement, false representation, false report or false claim with respect to the character, quality, quantity, or cost of any work performed or to be performed, or materials furnished or to be furnished, in connection with the construction of any highway or related project approved by the Secretary of Transportation; or

Whoever knowingly makes any false statement or false representation as to material fact in any statement, certificate, or report submitted pursuant to provisions of the Federal-aid Roads Act approved July 1, 1916, (39 Stat. 355), as amended and supplemented;

Shall be fined not more than \$10,000 or imprisoned not more than 5 years or both"

NON-FEDERAL AID PROJECTS

Iowa Code 714.8, subsection 3, defines fraudulent practices. "A person who does any of the following acts is guilty of a fraudulent practice. Subsection 3, Knowingly executes or tenders a false certification under penalty of perjury, false affidavit, or false certificate, if the certification, affidavit, or certificate is required by law or given in support of a claim for compensation, indemnification, restitution, or other payment." Depending on the amount of money claimed for payment, this could be a Class C or Class D felony, with potential fines and/or prison.

The above codes refer to the individual making the false statement. Standard Specification Article 1102.03, paragraph C. section 5 refers to the Contractor.

Article 1102.03, paragraph C, section 5 states, "A contractor may be disqualified from bidder qualification if or when: The contractor has falsified documents or certifications, or has knowingly provided false information to the Department or the Contracting Authority."

Section 2521. Certified Plant Inspection

2521.01 DESCRIPTION.

This describes certified plant inspection. Certified plant inspection will be required for Interstate, Primary, state park, and institutional projects. It will apply to other projects only when designated. When this specification applies, the Contractor shall furnish or be responsible for certified plant inspection for the work, as specified herein.

Based on satisfactory correlation with the Contracting Authority's test results, in accordance with Materials I.M. 216, the Contractor's process control test results for aggregate gradation shall be the basis of acceptance. The minimum frequency for acceptance testing shall be in accordance with Materials I.M. 204.

2521.02 REQUIREMENTS.

Certified plant inspection shall be in accordance with <u>Materials I.M. 213</u>, utilizing personnel certified for the type of inspection to be accomplished and utilizing prescribed test equipment furnished by the Contractor. The equipment shall also be available for use by the Engineer for monitoring purposes.

When a field laboratory or office is furnished, as provided in <u>Section 2520</u>, exclusive use by the Engineer for inspection purposes is intended. Additional field laboratory space and equipment and/or office space, for use by the Contractor to fulfill the requirements of Certified Plant Inspection, are incidental to the contract unit price for the item for which this inspection is required.

Delivery of samples to the District Materials Laboratory may also be required. The provisions for this are in accordance with <u>Section 2534</u>.

2521.03 APPLICATION.

This specification applies to all HMA, HMA patching material, PCC, structural concrete, and flowable mortar, except where excluded by a note in the contract documents.

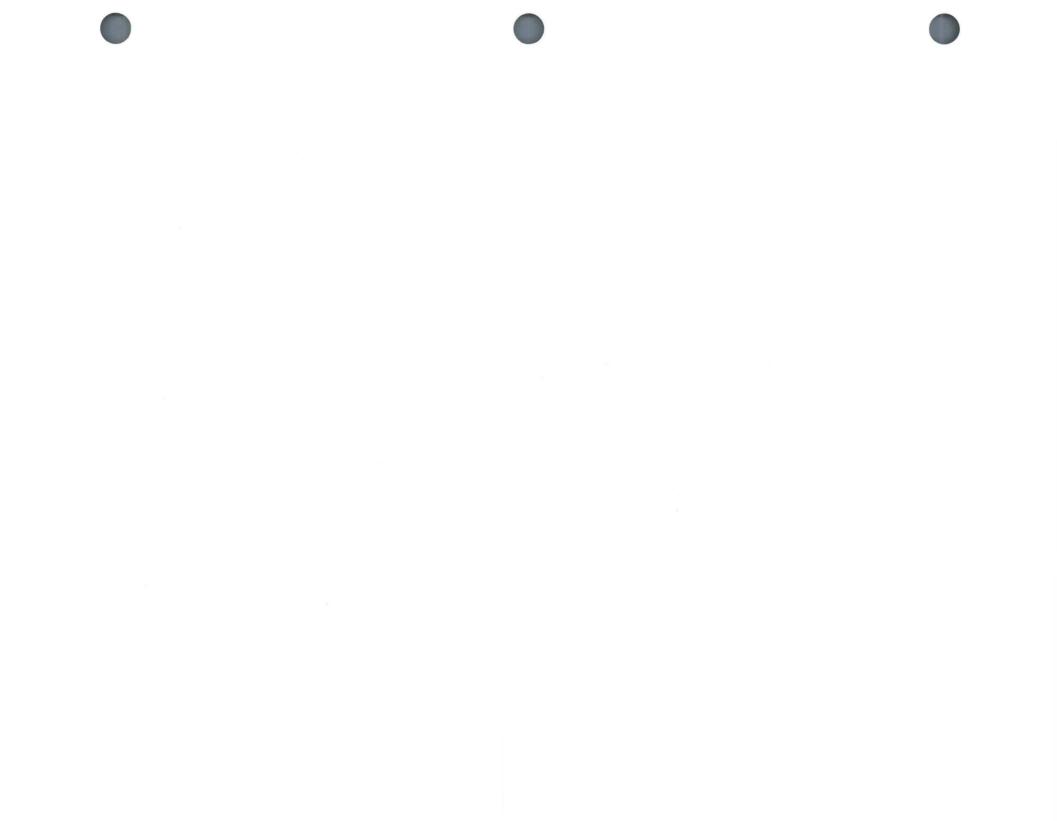
The Engineer may waive aggregate gradations, moisture, and specific gravity tests based on previous satisfactory experience with the plant for PCC which is furnished at a maximum rate of 25 cubic yards (25 m²) per day, whether from one or more sources. This may be based on quantities planned by the Contractor several days ahead of placement.

2521.04 METHOD OF MEASUREMENT AND BASIS OF PAYMENT.

Certified plant inspection will not be measured or paid for separately. It shall be included in the contract unit price for the item for which this inspection is required.

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PCC Level II Materials

III. CONCRETE MATERIALS

Concrete consists of three basic components-aggregates (both sand and rock), cement, and water. When mixed together and the chemical reaction is allowed to proceed, they form concrete. This material is one of the most versatile construction materials and has tremendous compressive strength. It is widely used for both pavements and structures.

- Cement is the fine gray powder that holds the aggregates together.
- Concrete is a mass of sand and rock bound together by cement.



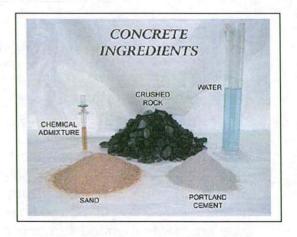
Portland cement is the most important and the most expensive component in a concrete mixture. It is the glue that holds the aggregates together and is the primary ingredient that will determine the strength of the concrete. The strength is developed through a process called hydration described as follows:

- Water contacts cement grain
- Exothermic reaction occurs
- Small needle-like crystals form on the surface of the cement particle
- Crystals interlock and form a gel-like mass.

Types

ASTM C150 / AASHTO M85

- I -Normal
- II -Moderate Sulfate Resistance
- III -High Early Strength
- IV -Low Heat of Hydration
- V -High Sulfate Resistance





Blended Cements

ASTM C595 / AASHTO M240

IP -15 to 40% Pozzolan

I(PM) - 0 to 15% Pozzolan

IS -25 to 75% GGBFS

I(SM) - 0 to 25% GGBFS

Type I used for most highway work and structures. Type II required on paving, except transit mix furnished less than 3000 m³ (3600 yd³). Type III ground finer than Type I cement. Blended cements may be furnished at Contractor's option when Type I or II is specified.

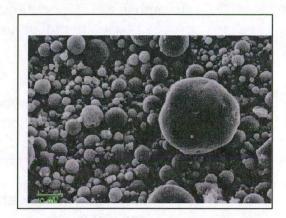
Storage and Handling

- Stored in weatherproof enclosures
- If lumps develop
 - Less than 1% okay
 - 1 to 5% requires batch weight adjustments
 - Rejected if exceeds 5% maximum on 840 μm (No. 20) sieve

2. Fly Ash - Article 4108, IM 491.17

Fly ash is a common mineral admixture used in most concrete paving mixtures. It is by-product of the burning of finely ground coal in electricity generating power plants.

This fine, powdery material, which is almost totally spherical in shape, is known as a pozzolan. Pozzolans are finely divided, siliceous or aluminosiliceous materials that react with water and calcium hydroxide released by Portland cement hydration to form cementing compounds.



Types - ASTM C618 / Article 4108

- Class C Fly Ash
 - o Cementing
 - o High Lime (CaO)
- Class F Fly Ash
 - Non-cementing
 - o Low Lime (CaO)

Approved sources of each are listed in IM 491.17.

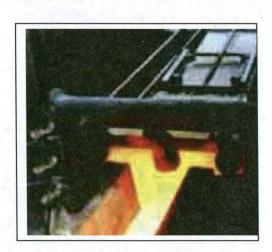
Some of the benefits that can often be achieved by using fly ash in the concrete include:

- Economical mix
- Increased long term strength
- Increased workability
- · Reduced heat of hydration
- Reduce permeability

3. Ground Granulated Blast Furnace Slag (GGBFS) - Article 4108

Ground granulated blast furnace slag (GGBFS) is a mineral admixture is a by-product of steel production.
GGBFS is made from slag floating on top of an iron blast furnace. The slag is tapped off and quenched in water to produce a glassy sand-like material. This material is ground to a fine powder.





The powder has slight cementing properties and minerals similar to those found in cement such as

- Silica
- Calcium
- Magnesim
- Aluminum

Advantage to using GGBFS

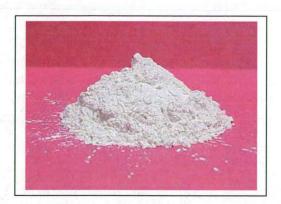
- Increased workability
- Increased strength
- Reduced permeability
- Increased sulfate resistance
- Decreased alkali aggregate reactivity

GGBFS is commonly blended or inter-ground with cement to form a I(SM) or IS blended cement.
Use of cement, fly ash, and GGBFS as a ternary mix is allowed in ready mix concrete only.

4. Aggregates - Articles 4109, 4110, 4111, 4115, 4117 and IM T-203

The aggregates in the concrete mixture make up the largest portion of the volume of the concrete, often about two thirds.

- Standard Iowa DOT mixes
 - Fine aggregate sand
 - Coarse aggregate gravel or crushed stone
- QMC mixes
 - Well graded
 - o Intermediate aggregate
 - Increases workability





a. Gradation

Gradation table

b. Durability

IM T-203

5. Water - Article 4102

The water used in batching concrete can come from almost any source. Each source must be tested and approved if it is not potable. Often lakes or streams are used because they are close to the project. This water must meet hardness, alkalinity, and acidity requirements. During the summer, warm water will add to the temperature of the concrete, which can lead to placement problems.

Chemical Admixtures - Article 4103, IM 403

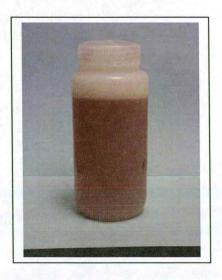
Admixtures can be classified by function and include:

- Air-entraining admixtures
- Water-reducing admixtures
- Retarding admixtures
- Accelerators
- Superplasticizers

Accelerators and super plasticizers are not commonly used in paving. Calcium Chloride is commonly used as an accelerator in patching work.

Reasons for using admixtures are:

- To reduce the cost
- Achieve certain concrete properties effectively
- Ensure the quality of concrete in adverse weather conditions



Admixtures cannot make "bad concrete" good, nor should they be used as a substitute for good concrete practices.

a. Air Entraining

Air-entraining admixtures are used to entrain millions of microscopic air bubbles in concrete.

- Freeze Thaw Durability
- Increase Workability

Types

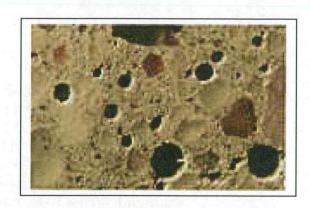
- Neutralized Salt of Pine Wood Resins (normally called Vinsol Resins)
- 2. Synthetic Detergents

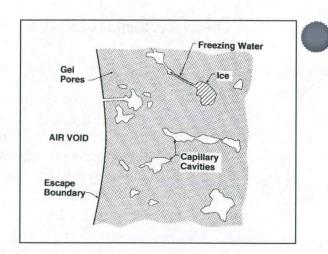
Why entrain air in concrete?

- Concrete is a porous material
- Exposed to moisture, water moves through the pores
- Below freezing, water turns to ice at 9% more volume
- Expanding ice forces water through capillaries
- Air voids act as pressure relief

Without air voids, the repeated freezing and thawing will damage the concrete. This damage is increased with deicing salts.

A listing of the many factors affecting the air entraining ability of the concrete is found at the end of this chapter.

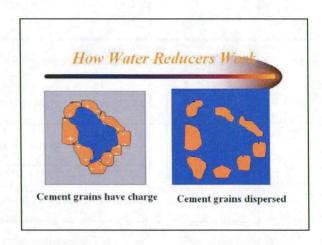




Concrete Materials

b. Water Reducer

- A water reducer is a liquid used to reduce the "static cling" produced by the electrical charges on cement particles.
- Reduce the quantity of mixing water required to produce concrete of a certain slump, reduce water/cement ratio, or increase slump. Typical water reduction is 7% to 10% with low range water reducers.



c. Retarders

- Delay the set of cement
- Act as water reducer
- Increase working time in hot weather

Concrete Mixes

Classes of Mix - IM 529 Typical Uses

•	Class A	County Paving
•	Class B	County Paving
•	Class C	Primary Paving
		& Structures
•	Class D	Structural
•	Class M	Patching/ high
		early strength
	Class O	Deck Overlay

Factors Affecting Control of Air in Concrete

Category	Characteristic	Effects	Guidance
Cement	Alkali Content	Air content increases with increased alkali content	Dosage may be reduced up to 40% for high alkali cements
		Very low alkali cements (less than 0.3%) reduces air content	Dosage may need to be increased by 100%
	Fineness	Air content decreases with increased fineness	Dosage may be increased up to 100% for Type III cements
	Blended Cements	As fineness of cement increases air content decreases Air content decreases with increase in LOI	Increase dosage rates of up to 100% Increase dosage rates of up to 100% or more
	Content	Air content decreases with increased amount of cement	Increase dosage as cement content increases
	Admixture Compatibility	Rapid slump loss is observed when a cement containing anhydrite is used in conjunction with a lignosulfonate based water reducer - hard to control air content	Use a retarding type admixture. Delay addition of water reducer by 15 secs. Increase mix time

Factors Affecting Control of Air in Concrete

Category	Characteristic	Effects	Guidance
Mineral Admixtures	Fly ash (LOI)	Air content decreases with higher LOI (carbon content) Carbon adsorbs the air agent reducing effectiveness	LOI's may vary as the peak load at the power plant causing variability load to load
		Air may be unstable with some combinations of fly ash, cement, and AEA's	Prepare trial mixes and evaluate air
		LOI's greater than 1%	Usually increases AEA demand
		LOI's greater than 2% may cause air to be very unstable over time	May increase AEA demand 5 times or more. May not be able to stabilize entrained air or attain required amount of air
		Finer fly ashes decreases air content	
	GGBFS	Air content decreases as GGBFS fineness increases	May need up to 100% or more AEA with finely ground slags
	Silica Fume	Air content decreases with increase in silica fume content	May need up to 100% increase in AEA
Chemical Admixtures	Water Reducers	Air content increases with increase water reducer dosage rates (lignin-based water reducers)	Reduce AEA dosage by up to 50%
	Retarders	Similar to water reducers	Reduce AEA dosage

Factors Affecting Control of Air in Concrete

Category	Characteristic	Effects	Guidance
Aggregates	Maximum Size	Air content requirements decrease as maximum size increases (up to 1.5")	Total air content required to protect concrete decreases
		Well graded aggregates aid in retention of smaller entrained air bubbles	Monitor gradations
	Sand	Air content increases with increased sand content	Decrease AEA content
	Sand Grading	Increased amounts retained on No. 30 to 50 sieves promote air entrainment	Monitor sand gradations
		Increased amount of fines passing the No. 100 sieve will decrease air content	Monitor sand gradations
		Organic contaminants may result in large fluctuations in air	Use clean sands
	Moisture Absorption	Many coarse aggregates are highly absorptive. Some will indicate moisture and still absorb water from the mix.	Manage stockpiles - moisture contents can vary load to load causing increases and decreases in slump and air content
	Minus No. 100	Increased amounts of crushed fines decreases air content Clay or silt fines in sand decrease air content	Total combined of greater than 2% passing the #100 sieve will affect ability to entrain air
		Combined totals greater than 2% may decrease air contents Combined totals greater than 2.5% will decrease air contents	May require dosage increases up to 5 times

Factors Affecting Control of Air in Concrete

Category	Characteristic	Effects	Guidance
Water	Hardness	Batching air agent with hard water or wash water first will decrease air content	Increase AEA by up to 50%
	Organic Contaminants	May increase or decrease air	Test water before using if not potable
	w/c ratio	Air content increases with increase in w/c ratio	1 gallon water = 0.5 to 1" slump
	Slump	Increase in slump increases air content (Up to 6 in.) Increase in slump to greater than 6 in. decreases air content	Increase slump 1" -increase air 0.5%
		Difficult to entrain air in low slump concrete (less than 1in.)	Increase slump

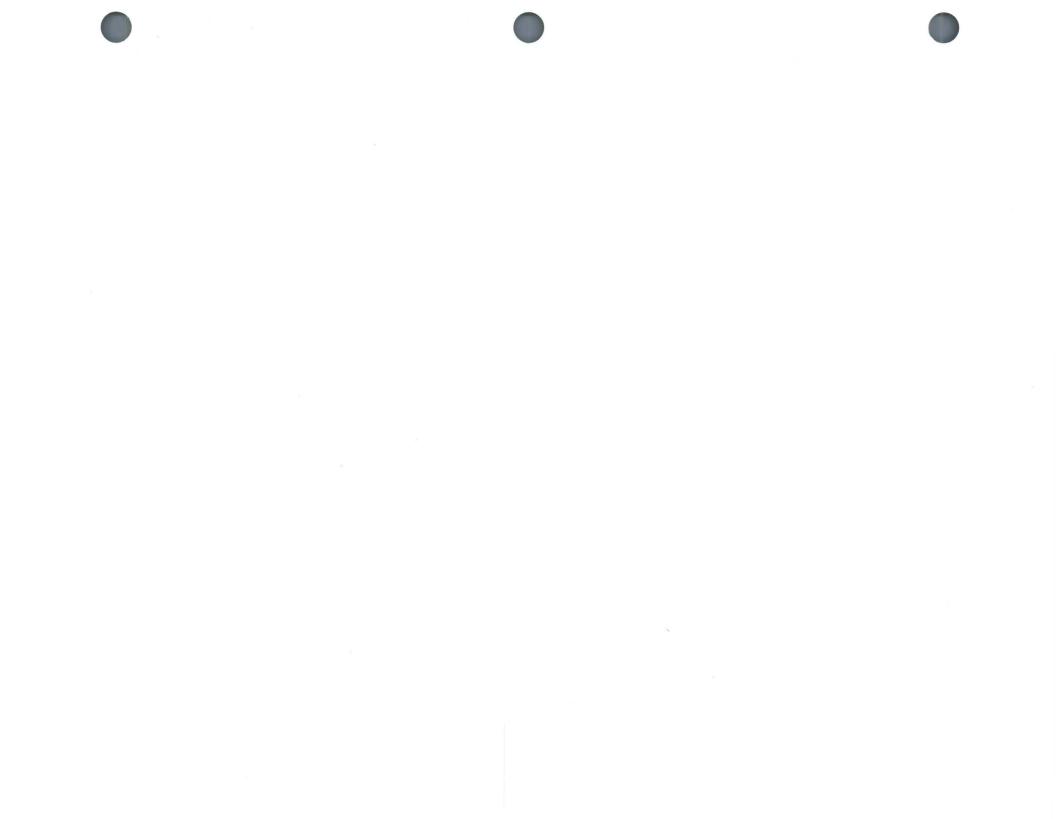
Factors Affecting Control of Air in Concrete

Category	Characteristic	Effects	Guidance
Production	Batching Sequence	Simultaneous batching may lower air content Batching AEA on to cement reduces AEA effectiveness	Discharge AEA into water or water line or on to sand
		Blending all materials promotes better mixing and entrained air development	
	Mixer Capacity	Air content increases as capacity is approached Overloaded mixer decreases air content	Run 80 to 85% of capacity gives best mixing action
	Mixing Time	Air content increases up to 5 min. mixing (central plant) Air content will decrease after 20 minutes of mixing (transit)	1 to 3 min. mix time optimum for central
		Mixing times less than 60 seconds may not develop proper air void system for freeze thaw protection	
	Mixing Speed	Air content increases to 20 rpm and decreases as speed increases	
	Admixture metering	Accuracy and reliability of dispensing system affects uniformity of air	Visually check bottles for accuracy
		Add all chemical admixtures separately	

Factors Affecting Control of Air in Concrete

Category	Characteristic	Effects	Guidance
Placement Procedures	Transport and delivery	Transport in non agitated equipment worse than for agitated	When using non-agitated haul units use smoothest and shortest haul routes
	Haul Time	Loss of 1 to 4 percent air depending on time Worse in hot weather	Use haul route that results in shortest time
	Mixing Drum	Air content decreases as mixer blades are worn or if concrete has hardened on or around the blades and pedestals	Perform regular maintenance
	Belt Conveyors	Reduces air content by up to 1 percent for less than 3000 ft.	
	Pumping	Pumping can lose up to 4% air	Don't allow high vertical drop Distance, slump, and line pressure all affect air content
	Vibration	Air content decreases under prolonged vibration at high frequencies (>10,000 vpm)	Closely spaced vibrators recommended 8000 vpm max. internal vibrators
	Finishing	Air content reduced in surface layer by excessive finishing	Avoid finishing with bleed water on surface DO NOT add water to surface to finish
	Temperature	Air content decreases with increasing temperature In low slump concrete (< 2 in.) at a temperature above 90 F is has been found to be more difficult to hold the slump and increase air contents. Likewise a small amount of water	Watering of stockpiles will help cool coarse aggregate and reduce absorption of mix water
		generates larger slump gains and a larger entrained air increase for concrete at 70F	Utilize coldest water possible for Hot Weather Concreteing (well water)





IV. METRICS

I. Tables of metric unit names, prefixes, and symbols

Following are terms commonly used in (or with) the metric system and the symbols for each.

Name	Symbol
Celsius Temperature	°C
centimeter	cm
square centimeter	cm ²
cubic centimeter	cm ³
day (time)	d
gram	g
hectare	ha
hour (time)	h
kilogram	kg
kilometer	km

Name	Symbol
square kilometer	km²
liter	a Las
megagram	Mg
meter	m
square meter	m ²
cubic meter	m ³
metric ton	A.t
millimeter	mm
minute (time)	min
second (time)	S

Following are some technical metric units and the symbols for each:

Name	Symbol
ampere (electric current)	а
candela (luminous intensity)	cd
hertz (frequency)	Hz
joule (energy, work)	J
lumen (luminous flux)	lm
newton (force)	N
pascal (pressure, stress)	Pa
volt (electric potential)	V
watt (power)	W

Following are prefixes used in the metric system, along with the symbol and magnitude for each.

Prefix	Symbol	Magnitude						
micro	μ	0.000001	millionth	10-6				
milli	m	0.001	thousandth	10-3				
centi	С	0.01	hundredth	10-2				
deci	d	0.1	tenth	10-1				
deka	da	10	ten	10				
hecto	h	100	hundred	10 ²				
kilo	k	1000	thousand	10 ³				
mega	М	1,000,000	million	10 ⁶				

The above table depicts the progression, by multiples of ten, from one prefix to the next. In practice, the prefixes *deci*, *deka*, and *hecto* are rarely used. Also the prefix *centi* is normally used only with *meter*. Preferred metric practice is to use units which represent multiples of 1000. Therefore, use of the centimeter and square centimeter while not disallowed, is discouraged. Another preferred practice is to choose a prefix so that the numerical value expressed is between 0.1 and 1000; e.g., 10 kilometers rather than 10,000 meters. Tables of numbers would be an exception to the practice.

Proper expression

Spacing 1.

Do NOT leave a space between a prefix and unit symbol or name

Right: km

Wrong: k m

Right: kilometer

Wrong: kilo meter

2. **Plurals**

Do NOT add an s to a unit symbol to make it plural

Right: 45 kg

Wrong: 45 kgs

Exception: 20°C

However, if a quantity is used as an adjective, use a hyphen instead of a space.

Examples: 35-mm film 3-meter pole

Area and Volume 3.

The symbol for square is the superscript ²

Example: 10 square meters is 10 m²

The symbol for *cubic* is the superscript ³

Example: 5 cubic meters is 5 m³

Product and Quotient 4.

With unit symbols, indicate the product of two or more units with a dot above the line. With unit names, use a space between words.

Examples: NAm

newton meter

With unit symbols, indicate a quotient or rate with a forward slash (/). With unit names, use the word per.

Examples: km/h

kilometers per hour

5. Mixing Names and Symbols

Do NOT mix unit names and symbols.

Right: km/h

Wrong: km/hour

WordPerfect 5.1 Hints 6.

The following symbols can be produced by holding down the ALT key and typing numbers on the keypad (do not use the numbers at the top of the keyboard):

micro (μ) = ALT 230

degree (°) = ALT 248 product (A) = ALT 249

(See Appendix A of the WordPerfect 5.1 Reference Manual for further information.)

Conversion factors: When converting a quantity from U.S. customary units to metric units, multiply the quantity by a conversion factor that is more accurate than required. Do not round either the conversion factor or the quantity before multiplication, as accuracy may be reduced. After multiplication, round the result so that the converted value does not imply a greater degree of precision (i.e., more decimal places or more significant digits) than existed in the original value.

The next page is a table of simple conversion factors. Others may be found on ASTM E 380-92.

Conversion Factors

Quantity	From U.S. Customary Units	To Metric Units	Multiply By		
Length	mile (U.S. Statute)* mile (international) yard foot (U.S. Survey)* foot (international) inch	km km m m m m	1.609347 1.609344** 0.9144** 0.3048333 0.3048** 25.4**		
Area	square mile (U.S. Statute)* square mile (international) acre (U.S. Statute)* square yard square foot square inch	km² m² ha (10,000 m²) m² m² mm²	2.589998 4046.873 0.4046873 0.83612736** 0.09290304** 645.16**		
Volume	acre foot (U.S. Survey)* cubic yard cubic foot cubic foot tubic foot 100 board feet gallon cubic inch cubic inch	m ³ m ³ m ³ cm L (1000 cm ³) m ³ L cm ³ mm ³	1233.489 0.76455486 0.02831685 28316.85 28.31685 0.2359737 3.785412 16.387064** 16387.064**		
Mass	Pound kip (1000 pounds)	kg Mg (1000 kg)	0.45359237** 0.45359237**		
Temperature	°F	°C	Formula: °C = (°F - 32)1.8**		

^{*} Conversion factors referenced to this footnote are based on the U.S. survey foot. The U.S. survey foot equals 1200/3937 meter.

^{**}exact conversion

Visualizing or Relating to Metric Quantities

Length:

1 mm
Approximately the thickness of a dime
1 m
About 3 inches longer than a yardstick
1 km
A little more than 1/2 mile (0.62 mile)

Weight:

1 g - About the weight of a large paper clip 1 kg - A little heavier than 2 lb (2.2 lb)

1 metric ton - 200 lb heavier than 1 short ton (2200 lb)

Volume:

1 mL - Approximately 1/3 quantity held in a teaspoon

1 L - Slightly more than 1 quart (1.06 quarts)
1 L - Approximately 34 fluid ounces (33.8 fl. oz)

1 gallon - Approximately 4 liters (3.785 liters)

 1 m^3 - 1.3 yd^3

1 m³ - Approximately 265 gallons

Strength: (all approximate conversions)

1 MPa - 145 psi 20 MPa - 3000 psi 35 MPa - 5000 psi 48 MPa - 7000 psi 100 MPa - 14,500 psi

Temperature:

Water Freezes - 0°C - 32°F Water Boils - 100°C - 212°F Body Temperature - 37°C - 98.6°F

Density (unit weight):

Aggregate dry rodded unit weight = 105 lb/ft^3 = 1680 kg/m^3 Aggregate solid density = 2.60×62.4 = 162.24 lb/ft^3 = 2.60×1 = 2.60 g/cm^3 = 2.60×1000 = 2600 kg.m^3

(where 2.60 is the specific gravity of the aggregate)

(where 2.00 is the specific gravity of the aggregate)

Unit weight of water - 62.4 lb/ft³

- 1 g/cm³

1000 kg/m³

Conversion Factors

Units of Length

To Convert From	Multiply by	To Obtain	To Convert From	Multiply by	To Obtain	
Mm	0.03937 in/mm	In	in	25.40 mm/in	mm	
Cm	0.3937 in/cm	ln	in	2.540 cm/in	cm	
М	3.281 ft/m	Ft	ft	0.3048 m/ft	m	
М	1.094 yd/m	Yd	yd	0.9144 m/yd	m	
Km	0.6214 mile/km	Mile	mile	1.609 km/mile	km	

Example: Convert 50 ft to meters

50 ft x 0.3048 m $= 15.24 \, \mathrm{m}$

Units of Area

To Convert From	Multiply by	To Obtain	To Convert From	Multiply by	To Obtain
mm²	0.001550 in ² /mm ²	In ²	in²	645.2 mm²/in²	mm²
m ²	10.76 ft²/m²	ft²	ft²	0.09290 m ² /ft ²	m²
m²	1.196 yd²/m²	Yd ²	yd²	0.8361 m²/yd²	m²
На	2.471 acre/ha	Acre	acre	0.4047 ha/acre	ha

Example: Convert 30 ft² to m²

 $30 \text{ ft}^2 \times 0.0929 \, \underline{m}^2 \\ \text{ft}^2$ $= 2.79 \text{ m}^2$

Units of Volume

To Convert From	Multiply by	To Obtain	To Convert From	Multiply by	To Obtain mL	
ML	0.03381 fl oz/mL	fl oz	fl oz	29.57 fl oz/mL		
L 0.2642 gallon/L m³ 264.2 gallon/m³ 35.32 ft³/m³		gallon	gallon	3.785 L/gallon	L	
		gallon	gallon	0.003785 m³/ gallon	m³	
		ft³	ft³	0.02832 m³/ft³	m ³	
m^3	1.308 yd³/m³	yd³	yd³	0.7645 m³/yd³	m^3	

Example: Convert 10 yd3 to m3

 $10 \text{ yd}^3 \times 0.7645 \underline{\text{m}}^3 = 7.6 \text{ m}^3$

Units of Weight (mass)

To Convert From	Multiply by	To Obtain	To Convert From	Multiply by	To Obtain	
G 0.0353 oz/g		OZ	OZ	28.35 g/oz	g	
Kg	2.205 lb/kg	lb	lb lb		kg	
Metric Ton (1000 kg)	1.103	Short Ton (2000 lb)	Short Ton (200 lb)	0.9072	Metric Ton (1000 kg	

Example: Convert 94 lb to kg

94 lb x 0.4536 kg = 42.64 kg

Temperature:

$$^{\circ}F = (^{\circ}C \times 1.8) + 32$$

To Derive Necessary Metric Conversion Factors

Tip: Carry the units in the calculation to ensure accuracy

Example: Derive the conversion factor to convert admixture dosage expressed in fl oz/cwt (fl oz/10 cement) to mL/kg

$$\left(1 \text{ f.o.} \times 2 \text{ .5 } \frac{\text{ f.o.}}{\text{ f.o.}}\right) \times \left(\frac{1}{100 b} \times \frac{1}{0.4536 \text{ g.}}\right) = \frac{1 \times 2 \text{ .5}}{100 \times 0.4536} = 0652 \text{ f.o.} / \text{ g.o.}$$

Other Conversion Factors (derived from basic units):

To Convert From	Multiply by	To Obtain			To Obtain	
kg/m³	0.06242	lb/ft³	lb/ft³	16.02	kg/m³	
kg/m³ 1.685		lb/yd³	lb/yd³	0.5935	kg/m³	
L/m³	0.2022	gallon/yd³	gallon/yd³	4.944	L/m³	
mL/kg	1.534	fl oz/cwt	fl oz/cwt	0.6519	mL/kg	
L/m³ 25.84		fl oz/yd³	fl oz/yd³	0.03870	L/m³	
Mpa 145.0		psi	psi	0.006895	MPa	

Metric Equivalents of Typical Quantities in Concrete and Aggregate Technology

Note: Some converted quantities have been rounded off.

Example Concrete Mixture Proportions

Quantity	U.S System	Metric (SI) Equivalents
Cement	600 lb/yd³	360 kg/m³
Water	300 lb/yd³ 36 gallon/yd³	180 kg/m³ 178 L/m³
Sand	1400 lb/yd³	830 kg/m ³
Stone	1800 lb/yd³	1070 kg/m³
Water Reducer	5 fl oz/cwt (100 lb cement) 30 fl oz/yd ³	3.3 mL/kg 1.2 L/m³

Aggregate Properties:

Specific gravity, absorption, moisture content, and fineness modulus are either unitless quantities or expressed as percentages. The numerical values should not be conveerted for these quantities.

Dry rodded unit weight = 105 lb/ft³ = 1680 kg/m³

Sieve Sizes: (Based on ASTM E 11- Standard Specification for Wire-Cloth Sieves for Testing Purposes)

Sieve	Opening in Inches	Metric SI Equivalent	Sieve	Opening in Inches	Metric SI Equivalent
3 in	3.0	75.0 mm	No. 8	0.0937	2.36 mm
2 in	2.0	50.0 mm	No.16	0.0469	1.18 mm
1 2 in	1.5	37.5 mm	No.30	0.0234	600 µm
1 in	1.0	25.0 mm	No. 50	0.0117	300 µm
3/4 in	0.75	19.0 mm	No. 100	0.0059	150 µm
3/8 in	0.375	9.5 mm	No.200	0.0029	75 µm
No. 4	0.187	4.75 mm			

Water:

Unit weight of water = 62.4 lb/ft³

= 1000 kg/m³ = 1 g/cm³ = 1 kg/L

1 gallon of water = 8.33 lb = 3.78 kg

Concrete Properties:

Property	U.S System	Metric SI Eqivalents				
Slump	6 inches	150 mm				
Temperature	80°F	27°C				
Unit Weight	150 lb/ft ³	2400 kg/m ³				
Air Content	6%	6%				
Compressive Strength	4000 psi	28 Mpa				
Flexural Strength	800 psi					
Elastic Modulus	4 x 10 psi	27,580 MPa or 27.6 GPa				

Metric Conversion

Soft conversion

Soft conversion is where the exact metric measurement is used.

Hard conversion

Hard conversion is where an equivilant rounded metric measurement is used

The number is divisible by 10, 5, 2, or 1

Note: Hard conversion will be used for converting from English to Metric measurements when practical.

Examples

Soft conversion

For 10 foot shoulder $(10 \text{ ft.}) \cdot (0.3048 \text{ m/ft.}) = 3.048 \text{ m}$

For 2 inch thick ACC Resurfacing (2 in.) · (25.40 mm/in.) = 50.8 mm

Hard conversion

For 10 foot shoulder

The metric measurement that will probably be used is 3 meters

For 2 inch thick ACC Resurfacing

The metric measurement that will probably be used is 50 millimeters

V. SAMPLING & TESTING

GGREGATES

Test Methods

IM 307 Specific Gravity of Aggregates

- Ratio of materials density to water
- Used to convert volumes to equivalent weights (masses)

Cement 3.14 (Type I/II)

Water 1.00Air 0

- Aggregates IM T-203 determine
 - 1. Sample splitter
 - Immerse (+ #4 sieve) in water for period of not less than 15 hours



IM 308 Free Moisture and Absorption of Aggregates

- Same as IM 307 except test sample is wet as received
- Needed to determine moisture content of aggregates

TEST FREQUENCY

- A. Paving Plants (IM 527)
 - a. Once per day for continuous operation
 - b. Once per week for small quantities (less than 250 yd³ per day)
- B. Ready Mix Plants (IM 528)
 - a. One day's run or 250 cubic yards (190 m³), whichever is greater.
 - b. Once per week if less than 250 cubic yards (190 m³) produced in week.

Specific Gravity

A. Paving Plants

1. One sample (each aggregate) per day for the first 3 days - then every third day thereafter

a. It is a good idea to try to test each aggregate before the work begins. b. This gives the pycnometer weight for the moisture test

B. Ready Mix Plants

- 1. One sample (each aggregate) per week for the first 2 weeks.
- 2. One sample (each aggregate) every other week thereafter.
- 3. If sample varies more that 0.02 from the T-203 Sp.Gr. Contact District Materials Lab and begin testing another sample.

Moisture

A. Paving Plant

- 1. Minimum of 1 test per half day
- 2. Moisture shall not vary between batches by more than 0.5%
- 3. Spec. 2301.16 A
 - a. Coarse aggregate with an absorption of 0.5% or more shall be wetted and allowed to drain at least one hour before batching.
 - b. It is recommended to soak a pile if it shows absorption.
- 4. When water can be observed dripping from bins between batches, the material must not be used.
 - a. Allow the stockpile to drain

B. Ready Mix Plants

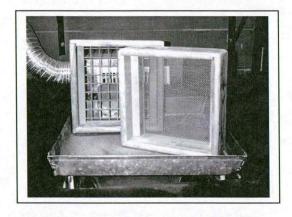
- 1. Minimum of one sample (each aggregate) per lot.
 - a. Use common sense on moisture samples.
 - 1. If it rains or snows, sample more often
- 2. Moisture shall not vary, between batches by more than 0.5%

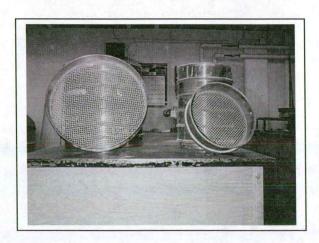
- 3. Spec. 2301.16 A
 - a. Coarse aggregate with an absorption of 0.5% or more shall be wetted and allowed to drain at least one hour before batching.
- 4. When water can be observed dripping from the bins between batches, the material must not be used.
 - a. Allow the stockpile to drain.

Gradations

A. When certified plant inspection is required, the Contractor's test results for aggregate gradation shall be quality control. Quality control tests are used to ensure proper material being delivered from the source and to identify stockpile changes. A lot is accepted when a verification test by the agency is determined to be in compliance. The minimum frequency for quality control and verification testing shall be in accordance with IM 204.

- B. CPI –Sample and test once per day (or lot).
 - 1. If a sample result is near or exceeds the specification limits, the CPI should inform the contractor and the agency so they can increase monitor frequency.
 - 2. The District Materials Engineer may investigate sampling and testing procedures.
 - 3. The producer needs to be notified if gradations continue to fail.
- C. Agency –Sample and test first day, thereafter, sample once per day and test once per week for paving, sample and test once per lot for structures.
 - 1. In accordance with IM 205,





agency will randomly select sample location and time, witness sampling, and take immediate possession of samples.

- Contractor may provide assistance in obtaining samples.
- Contractor may elect to have agency split verification sample. This allows both parties to check testing differences; however, IM 216 correlation is not required.
- A lot is accepted when a verification test by the agency is determined to be in compliance.

AGGREGATE GRADATION TABLE - ENGLISH

Grad.	Section No.	Std. Sieve Size	11/2"	1"	3/4"	1/2"	3/8"	#4	#8	#30	#50	#100	#200	- 7
No.		Intended Use		The state of			Pero	ent Passing				1		*Note
1	4110,4125, 4133	PCC FA Cover Agg.		_TT 34	2 4 7		100	90-100	70-100	10-60	1		0-1.5	1
3	4115 (57, 2-8)	PCC CA	100	95-100	- 1177	25-60	4 4 4	0-10	0-5	1. 182			0-1.5	2,11
4	4115 (2-8)	PCC CA	100	50-100	30-100	20-75	5-55	0-10	0-5	En Maria			0-1.5	11
5	4115 (67, 2-8)	PCC CA	180 to	100	90-100	E 1 1 -	20-55	0-10	0-5	Sellie.	17.37		0-1.5	11
6	4115.06 (Repair & Overlay)	PCC CA			100	97-100	40-90	0-30					0-1.5	11
7	4117 (Class V)	PCC FA & CA	100	DE CONTRACTOR				80-92	60-75	20-40		3,43-1	4	
8	4117.03 (Class V)	Fine Limestone	1393.1				100	90-100				10 E	0-30	
10	4120.02, 4120.03 (C Gravel)	Granular Surface			100		134	50-80	25-60	0.1		4		3
11	4120.02, 4120.04, 4120.05, 4120.07 (A, B, Cr. St.)	Granular Surface & Shoulder		100	95-100	70-90		30-55	15-40				6-16	4, 5
12a	4121 (Cr. St.)	Granular Subbase	100			40-80	4	100	5-25	1	-/		0-6	6
12b	4121 (Cr. Gravel)	Granular Subbase	100	200		50-80	Table 1880		10-30		5-15		3-7	7
13	4122.02 (Cr. St.)	Macadam St. Base		12.7		3" nomir	nal maximum	n size – scree	ened over 3/	4" or 1" so	reen			
14	4123	Modified Subbase	100	CHARLE I	70-90	The las	AC 74Eur	J. S. dh	10-40		23 34 5	W. 45.5	3-10	5,7
19	4125 (1/2" Cr. Gr. or Cr. St.)	Cover Aggregate			100	97-100	40-90	0-30	0-15		837		0-2	
20	4125 (1/2" Scr. Gr.)	Cover Aggregate		and the same	100	95-100	40-80	0-15	0-7				0-1.5	
21	4125 (3/8")	Cover Aggregate	Jun 2			100	90-100	10-55	0-20	0-7			0-1.5	
22	4124.02	Fine Slurry Mixture	F12.54				100	85-100	40-95	20-60	14-35	10-25	5-25	10
23	4124.02 (Cr. St.)	Coarse Slurry Mixture					100	70-90	45-70	19-34	12-25	7-18	5-15	
29	4131	Porous Backfill			100	95-100	50-100	0-50	0-8					
30	4132.02 (Cr. St.)	Special Backfill	100			137 DE			15-45				0-10	5
31	4132.03 (Gravel)	Special Backfill	1 to	100	90-100	75-100			30-55			10.0	3-7	
32	4133 (Sand/Gr./Cr. St.)	Granular Backfill			100% passir	ng the 3" scre	een		20-100		3.14		0-10	8, 9
35	4133.05 (Natural Sand/Gr.)	Floodable Backfill	100	1,27		A F			20-90				0-4	
36	4133.05 (Natural Sand)	Floodable Backfill		7,00	1 734		F - F 11	12	100		7		0-2	2 =

Notes: (Gradations Nos. 2, 9, 15, 16, 17, 18, 24, 26, 27, 28, 33 and 34 have been deleted.)

*For numbered notes, see page 2.

5-6

- 1. For Section 4110, when the fine aggregate is sieved through the following number sieves 4, 8, 16, 30, 50, and 100 not more than 40% shall pass one sieve and be retained on the sieve with the next higher number.
- When used in precast and prestressed concrete bridge beams, 100% shall pass the 1" sieve.
- 3. When compaction of material is a specification requirement, the minimum percent passing the No. 200 sieve is 6%.
- 4. See specifications for combination of gravel and limestone.
- Unwashed air-dried samples of crushed composite material shall be tested for gradation compliance except that no gradation determination will be made for the material passing the No. 200 sieve.
- 6. The gradation requirement for the No. 8 sieve shall be 5% to 20% when recycled material is supplied.
- 7. For 4121 gravel, one fractured face on 30% or more of the particles retained on the 3/8-inch sieve. For 4123 gravel, one fractured face on 75% or more of the particles retained on the 3/8-inch sieve.
- 8. Crushed stone shall have 100% passing the 1" sieve.
- 9. When granular backfill is used in floodable applications use gradation 35 or 36. When granular backfill is used under flowable mortar, one of the following alternative materials shall be used: natural sand compliant with Section 4110, except the % passing the No. 200 sieve shall not exceed 4%; gravel, crushed stone, or crushed concrete meeting the gradation requirements of Section 4121.
- 10. Gradation limitations for the 30, 50 and 100 sieves shall not apply when slurry mixture is applied by hand lutes, such as for slurry leveling.
- 11. Maximum of 2.5% passing the No. 200 sieve allowed if generated from the parent material when documented production is 1% or less as determined by the Office of Materials.

HMA Gyratory gradation requirements are listed in IM 510, Appendix A.





VI. Proportions

- 1. Contractor representative makes batch weight calculations
- 2. Plant Inspector or Monitor cross check batch weights
- 3. No batching until both independent determinations have been made

IM 529

- Standard Iowa DOT Mixes
- Absolute Volumes
- SSD Batch Weights
- Basic and Maximum w/c

Source Information

To find specific gravities, source name, etc.

- IM 401
- Cement sources
- IM 491.14
- GGBFS sources
- IM 491.17 Fly ash sources
- IM T-203
- Aggregate sources
- IM 403
- Admixtures

Batch Weight Calculations

- Based on absolute volumes
- 1 cubic yard basic unit of volume
- Aggregate percentages

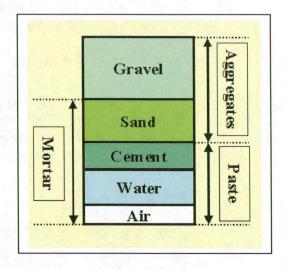
Mix	Percent	Percent	
No.	Coarse	Fine	
2	60	40	
3	55	45	
4	50	50	
5	45	55	
6	40	60	

w/c Ratio

- Basic w/c
- Maximum w/c ratio
- All cementitous materials are included in w/c calculation

Specific Gravity

- Used to convert volumes to equivalent weights
- · Ratio of materials density to the density of water
- Use 3.14 for Type I or II cements



Example

An A-3, B-3, or C-3 Mix-

55% coarse aggregate & 45% Fine aggregate

- Use 1.00 for water
- Air has no specific gravity, occupies a volume

Standard Measurements

- Weight of water per cubic foot = 62.4 lbs./cu. ft.
- Weight of water per gallon = 8.33 lbs./gallon
- Cu. ft. per cu. yd. = 27 cu. ft.

Examples

To figure weight per unit volume

Absolute Volume × Specific Gravity × Unit Weight of water × cu. ft. per cu. yd.

To figure absolute volume

Batch Weight ÷ Specific Gravity ÷ Unit Weight of water ÷ cu. ft. per cu. yd.

Example 1 - C-3WR Mix Proportions - IM 529

Absolute Volumes

Cement 0.108
Water 0.146
Air 0.060
Fine Agg. 0.309
Coarse Agg. 0.377

Assume Sp. G. of 2.65 for both coarse and fine aggregates

Batch Weights - SSD

Cement weight = $0.108 \times 3.14 \times 62.4 \text{ lbs/ft}^3 \times 27 \text{ ft}^3/\text{yd}^3 = 571 \text{ lbs. per cubic yard}$ Basic Water = $0.146 \times 1.00 \times 62.4 \text{ lbs/ft}^3 \times 27 \text{ ft}^3/\text{yd}^3 = 246 \text{ lbs. per cubic yard}$ Fine agg. = $0.309 \times 2.65 \times 62.4 \text{ lbs/ft}^3 \times 27 \text{ ft}^3/\text{yd}^3 = 1380 \text{ lbs. per cubic yard}$ Coarse agg. = $0.377 \times 2.65 \times 62.4 \text{ lbs/ft}^3 \times 27 \text{ ft}^3/\text{yd}^3 = 1683 \text{ lbs. per cubic yard}$ PCC Level II Proportions

Mineral Admixture Substitution

- Weight replacement (not volume)
- Pound for pound basis (1:1)
- Fly Ash 20% maximum
- GGBFS 35% Maximum
- Maximum total mineral admixture substitution rate of 50% for structures and 40% for paving.
- Fly ash permitted in concrete when GGBFS is substituted in ready mix concrete only (ternary mix)
- Ternary mixes substitute fly ash first
- Time Period Allowed
 - o Paving -Article 2301.04
 - Structural Article 2403.03
 - New Decks Article 2412.02

Calculate Batch Weights

- Multiply weight of cement by percent replacement
- Subtract amount from cement
- Absolute volume with fly ash more than cement alone
- Must adjust absolute volumes changes coarse and fine aggregate batch weights

Example 2 - Fly ash substitution

C-3WR in Example 1 20% fly ash substitution Assume 2.59 Sp. G. for fly ash

571 lbs. per cubic yard \times 0.20 = 114 lbs. fly ash 571 – 114 = 457 lbs. cement

Abs. Vol. Cement = $457 \div 3.14 \div 62.4 \text{ lbs/ft}^3 \div 27 \text{ ft}^3/\text{yd}^3$ Abs. Vol. Fly Ash = $114 \div 2.59 \div 62.4 \text{ lbs/ft}^3 \div 27 \text{ ft}^3/\text{ yd}^3$	= 0.086 = 0.026
Weight Water = $0.430 \times 571 = 246$ lbs. per cubic yard Abs. Vol. Water = $246 \div 1.00 \div 62.4$ lbs/ft ³ ÷ 27 ft ³ /yd ³	= 0.146
Abs. Vol. Air	= 0.060
Abs. Vol.	= 0.318
1 – Subtotal	= 0.682
%Coarse = 0.55 × 0.682	= 0.375
%Fine = 0.45 x 0.682	= 0.307

Fine agg. = $0.307 \times 2.65 \times 62.4 \text{ lbs/ft}^3 \times 27 \text{ ft}^3/\text{yd}^3 = 1371 \text{ lbs. per cubic yard}$ Coarse agg. = $0.375 \times 2.65 \times 62.4 \text{ lbs/ft}^3 \times 27 \text{ ft}^3/\text{yd}^3 = 1674 \text{ lbs. per cubic yard}$ **PCC Level II Proportions**

Check to make sure Absolute Volumes = 1.00

Cement	0.086
Fly Ash	0.026
Water	0.146
Air	0.060
Coarse	0.375
Fine	0.307
Total	1.000

Example Fly ash and GGBFS substitution

C-3WR in Example 1 15% fly ash substitution 35% GGBFS substitution Assume 2.59 Sp. G. for fly ash, 2.88 for GGBFS

Substitute for fly ash first 571 lbs. per cubic yard \times 0.15 = 86 lbs. fly ash 571 - 86 = 485 lbs. cement left

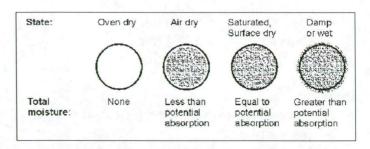
Substitute for GGBFS with remaining cement 485 lbs. per cubic yard \times 0.35 = 170 lbs. GGBFS 485 - 170 = 315 lbs. cement

Abs. Vol. Cement = $315 \div 3.14 \div 62.4 \text{ lbs/ft}^3 \div 27 \text{ ft}^3/\text{yd}^3$ = 0.060Abs. Vol. Fly Ash = $86 \div 2.59 \div 62.4 \text{ lbs/ft}^3 \div 27 \text{ ft}^3/\text{ yd}^3$ = 0.020Abs. Vol. GGBFS = $170 \div 2.88 \div 62.4 \text{ lbs/ft}^3 \div 27 \text{ ft}^3/\text{ vd}^3$ = 0.035Weight Water = $0.430 \times 571 = 246$ lbs. per cubic yard Abs. Vol. Water = $246 \div 1.00 \div 62.4 \text{ lbs/ft}^3 \div 27 \text{ ft}^3/\text{yd}^3$ = 0.146Abs. Vol. Air = 0.060Abs. Vol. = 0.3211 - Subtotal = 0.679%Coarse = 0.55×0.679 = 0.373%Fine = 0.45×0.679 = 0.306Fine agg. = $0.306 \times 2.65 \times 62.4 \text{ lbs/ft}^3 \times 27 \text{ ft}^3/\text{yd}^3 = 1366 \text{ lbs. per cubic yard}$

Coarse agg. = $0.373 \times 2.65 \times 62.4 \text{ lbs/ft}^3 \times 27 \text{ ft}^3/\text{yd}^3 = 1665 \text{ lbs. per cubic yard}$

Moisture Corrections

- Must correct SSD batch weights for moisture
- Water in aggregate (or lack thereof)
- · Adjust batch water
- If aggregate has moisture must reduce batch water, in absorption must add water
- Maximum permissible absorption is 0.5%



Wet batch wt. = $\underline{\text{Batch wt., SSD}} \times 100$ (100 - % Moisture)

Example 1 - SSD Batch Weights

Coarse Agg. = 1665 lbs. Fine Agg. = 1366 lbs. Basic Water = 246 lbs.

Assume

Coarse Aggregate Moisture = 0.3% Fine Aggregate Moisture = 3.1%

Wet Batch Wt., Coarse

 $\frac{1665 \text{ lbs.}}{(100 - 0.3)}$ x 100 = 1670 lbs.

Wet Batch Wt., Fine

 $\frac{1366 \text{ lbs.}}{(100 - 3.1)}$ x 100 = 1410 lbs.

Adjust Water

Coarse
Wet Batch Weight – Dry batch weight
1670 – 1665 = 5 lbs.

Fine 1410 – 1366 = 44 lbs.

246 - 5 - 44 = 197 lbs.

Example

Coarse 1.000 $\underline{1665}$ $\underline{-.003}$.997Fine: 1.000 $\underline{1366}$ $\underline{-.031}$.969 .969

Example 2 - SSD Batch Weights

Coarse Agg. = 1665 lbs. Fine Agg. = 1366 lbs. Water = 246 lbs.

Assume

Coarse Aggregate Moisture = -0.5% (Absorption)
Fine Aggregate Moisture = 3.1%

Wet Batch Wt., Coarse

$$\frac{1665 \text{ lbs.}}{(100 - (-0.5))} \times 100 = 1657 \text{ lbs.}$$

Wet Batch Wt., Fine

$$\frac{1366 \text{ lbs.}}{(100 - 3.1)} \times 100 = 1410 \text{ lbs.}$$

Adjust Water

Coarse

Wet Batch Weight – Dry batch weight 1657 – 1665 = -8 lbs.

Fine

1410 - 1366 = 44 lbs.

$$246 - (-8) + 44 = 210$$
 lbs.

Maximum Water

$$= 0.489 \times 571 \text{ lbs./yd}^3 = 279 \text{ lbs./yd}^3$$

Total water allowed including moisture in aggregates

Example		
Coarse	1.000 + .005 1.005	<u>1665</u> 1.005 = 1657
Fine	1.000 031 .969	<u>1366</u> .969 = 1410

PCC Level II Proportions

Alternate Method to Compute Wet Weights

Table T-214A in IM Volume II has reciprocals that can be used to figure moisture and absorption of aggregate. Using the reciprocals with Example 1:

Fine Aggregate:

 $1366 \times 1.0319917 = 1410 \text{ lbs}.$

Coarse Aggregate:

 $1665 \times 1.0030090 = 1670$ lbs.

The results are the same using either method. The first method will be used throughout this course. There is less chance for error using the first method.

Reissued April 18, 2006 Supersedes April 3, 2001

Matls. IM T214A

RECIPROCALS FOR BATCH WEIGHT CALCULATIONS

		worsture	Content (Fe	icentage ba	sed on Wet	vveigiit)	
	0	1.0	2.0	3.0	4.0	5.0	6.0
0.0	1.0000000 .0010010	1.0101010	1.0204082	1.0309278	1.0416667	1.0526316	1.0638298
diff.		.0010213	.0010423	.0010639	.0010862	.0011092	.0011329
0.1	1.0010010	1.0111223	1.0214505	1.0319917	1.0427529	1.0537408	1.0649627
diff.	.0010030	.0010234	.0010444	.0010662	.0010884	.0011115	.0011354
0.2	1.0020040	1.0121457	1.0224949	1.0330579	1.0438413	1.0548523	1.0660981
diff.	.0010050	.0010255	.0010466	.0010683	.0010908	.0011139	.0011378
0.3	1.0030090	1.0131712	1.0235415	1.0341262	1.0449321	1.0559662	1.0672359
diff.	.0010071	.0010276	.0010487	.0010705	.0010930	.0011163	.0011402
0.4	1.0040161	1.0141988	1.0245902	1.0351967	1.0460251	1.0570825	1.0683761
diff.	.0010090	.0010296	.0010508	.0010727	.0010953	.0011186	.0011426
0.5	1.0050251	1.0152284	1.0256410	1.0362694	1.0471204	1.0582011	1.0695187
diff.	.0010111	.0010318	.0010530	.0010750	.0010976	.0011209	.0011451
0.6	1.0060362	1.0162602	1.0266940	1.0373444	1.0482180	1.0593220	1.0706638
diff.	.0010131	.0010338	.0010552	.0010772	.0010999	.0011234	.0011476
0.7	1.0070493	1.0172940	1.0277492	1.0384216	1.0493179	1.0604454	1.0718114
diff.	.0010152	.0010359	.0010574	.0010794	.0011023	.0011257	.0011500
0.8	1.0080645	1.0183299	1.0288066	1.0395010	1.0504202	1.0615711	1.0729614
diff.	.0010172	.0010381	.0010595	.0010817	.0011045	.0011282	.0011525
0.9	1.0090817	1.0193680	1.0298661	1.0405827	1.0515247	1.0626993	1.0741139
diff.	.0010193	.0010402	.0010617	.0010840	.0011069	.0011305	.0011550

RECIPROCALS FOR BATCH WEIGHT CALCULATIONS

0.0 1.00000000 0.99009901 0.98039216 diff. 00099900 00097933 00096023 0.1 0.99900100 0.98911968 0.97943193 diff. 00099701 00097739 00095835 0.2 0.99800399 0.98814229 0.97847358 diff. 00099502 00097546 00095647 0.3 0.99700897 0.98716683 0.97751711 diff. 00099303 00097354 00095461 0.4 0.99601594 0.98619329 0.97656250 diff. 00099106 00097162 00095274 0.5 0.99502488 0.98522167 0.97560976 diff. 00098909 00096970 00095089 0.6 0.99403579 0.98425197 0.97465887 diff. 00098713 00096780 00094904 0.7 0.99304866 0.98328417 0.97370983 diff. 00098517 00096590 00094718 0.8 0.99206349 0.98231827 0.97276265 diff. 0009		0.0	1.0	2.0	3.0
0.1 0.99900100 0.98911968 0.97943193 diff. 00099701 00097739 00095835 0.2 0.99800399 0.98814229 0.97847358 diff. 00099502 00097546 00095647 0.3 0.99700897 0.98716683 0.97751711 diff. 00099303 00097354 00095461 0.4 0.99601594 0.98619329 0.97656250 diff. 00099106 00097162 00095274 0.5 0.99502488 0.98522167 0.97560976 diff. 00098909 00096970 00095089 0.6 0.99403579 0.98425197 0.97465887 diff. 00098713 00096780 00094904 0.7 0.99304866 0.98328417 0.97370983 diff. 00098517 00096590 00094718 0.8 0.99206349 0.98231827 0.97276265	0.0	1.00000000	0.99009901	0.98039216	
diff. 00099701 00097739 00095835 0.2 0.99800399 0.98814229 0.97847358 diff. 00099502 00097546 00095647 0.3 0.99700897 0.98716683 0.97751711 diff. 00099303 00097354 00095461 0.4 0.99601594 0.98619329 0.97656250 diff. 00099106 00097162 00095274 0.5 0.99502488 0.98522167 0.97560976 diff. 00098909 00096970 00095089 0.6 0.99403579 0.98425197 0.97465887 diff. 00098713 00096780 00094904 0.7 0.99304866 0.98328417 0.97370983 diff. 00098517 00096590 00094718 0.8 0.99206349 0.98231827 0.97276265	diff.	00099900	00097933	00096023	
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0.6 0.99403579 0.98425197 0.97465887 diff. 00098713 00096780 00094904 0.7 0.99304866 0.98328417 0.97370983 diff. 00098517 00096590 00094718 0.8 0.99206349 0.98231827 0.97276265	0.5	0.99502488	0.98522167	0.97560976	
diff. 00098713 00096780 00094904 0.7 0.99304866 0.98328417 0.97370983 diff. 00098517 00096590 00094718 0.8 0.99206349 0.98231827 0.97276265	diff.	00098909	00096970	00095089	
0.7 0.99304866 0.98328417 0.97370983 diff. 00098517 00096590 00094718 0.8 0.99206349 0.98231827 0.97276265	0.6	0.99403579	0.98425197	0.97465887	
diff. 00098517 00096590 00094718 0.8 0.99206349 0.98231827 0.97276265	diff.	00098713	00096780	00094904	
0.8 0.99206349 0.98231827 0.97276265	0.7	0.99304866	0.98328417	0.97370983	
	diff.	00098517	00096590	00094718	
diff000983210009640000094535	0.8	0.99206349	0.98231827	0.97276265	
	diff.	00098321	00096400	00094535	
	diff.	00098127	00096211	00094352	



PROBLEM 1

A. Compute the dry batch weights of a cubic yard for a B-4 mix using absolute volumes (IM 529) as the basis for your calculations given the following specific gravities:

Specific Gravity
Cement 3.14
Fine Agg. 2.66
Coarse Agg. 2.68

B. Compute the wet batch weight based on the results form part A and correct the basic water batched by including free water from the aggregate. Convert your answer to gallons. Also, compute the maximum allowable mixing water in gallons given the following free moisture contents.

Assume Fine Aggregate Moisture 3.1% Assume Coarse Aggregate Moisture 0.3%



PROBLEM 2

FIGURE THE DRY BATCH WEIGHTS OF A C-4 C15 MIX USING FORM 820150. THE SOURCES ARE LISTED BELOW.

Continental Cement Co. - Type I

ISG Resources - Louisa Generating Station

Coarse Aggregate - Kuhlman Const. - Gisleson Quarry - Clayton County

Fine Aggregate – Roverud Construction Co. – Bente Pit – Clayton County

FIGURE THE DRY BATCH WEIGHTS OF A C-4 MIX USING FORM 820150.



Project No				County .	
Mix No.:	Pounds 0	Cement:			
1st Adjus	sted lbs. Cement:	Source:		Sp. Gr.:	12.5
I.M. 491.17	Fly Ash:	Source:		Sp. Gr.:	
I.M. 491.14	Slag GGBFS:	Source:		Sp. Gr.:	
2nd Adjus	sted lbs. Cement:				
To	otal Cementitious				
I.M. T-203	Fine Aggregate Source:			Sp. Gr.:	
I.M. T-203				Sp. Gr.:	
I.M. T-203	Coarse Agregate Source:			Sp. Gr.:	
Basic w/c	v	Vater (lbs/cv) = De	esign w/c (wt. cement + wt F	ly Ash +Slag) =	
Max w/c			esign w/c (wt. cement + wt F		
				A-11-4-1-1-1	
Absolute Volumes					
	Cement	(lbs/cy	/) / (Sp. Gr. X 62.4 X 27)	- 10 <u>- 1</u>	
	Fly Ash	(lba/a)	1// C- C- V C2 4 V 27)	14 <u>1</u> 54.4	
	Fly Asn	(IDS/Cy	/) / (Sp. Gr. X 62.4 X 27)		
	Slag	(lbs/cy	y) / (Sp. Gr. X 62.4 X 27)		90
	Water	(lbs/c)	y) / (1.00 X 62.4 X 27)	- <u>-</u>	
	Air				0.060
			Subtotal		
			1.000 - Subtotal		
			Total		1.000
	개연 시간 보다 그 얼마를 받는				
% FA Agg.:		ate (1.000 - Subto			
% In. Agg.: _ % CA Agg.:		gate (1.000 - Subto gate (1.000 - Subto			
76 CA Agg	Coarse Aggre	gate (1.000 - Subt	otal) A 76 III WIIX		
			Aggregate Total		
Aggregate Weights			17.13 de 18.25 - 25.17	_	
	Fine Aggregat	e (abs vol.) X Sp	. Gr. X 62.4 X 27		
	Intermediate Aggr	egate (abs vol.)	X Sp. Gr. X 62.4 X 27		
	Coarse Aggreg	ate (abs vol.) X S	p. Gr. X 62.4 X 27		
		Cement	(lbs/cy)		
Summary			(lbs/cy)		
Summary		Fly Ash			
Summary		Slag	(lbs/cy)		
Summary		Slag	(lbs/cy) (lbs/cy)		
Summary		Slag Water Fine Agg.			
Summary		Slag	(lbs/cy)		

Project No.:				
Mix No.:		Pounds Cement:		
1st Adjus	ted lbs. Cement:	Source:	Sp. Gr.:	1
I.M. 491.17	Fly Ash:	Source:	Sp. Gr.:	
I.M. 491.14	Slag GGBFS:	Source:	Sp. Gr.:	
2nd Adjus	ted lbs. Cement:	프라마이트 그 사람들이 그		
То	otal Cementitious			
I.M. T-203	Fine Aggregate Source:		Sp. Gr.:	
I.M. T-203 I.M. T-203	Interm. Aggregate Source: Coarse Agregate Source:		Sp. Gr.:	1
Basic w/c_		Water (lbs/cy) = Design w/c (wt. cement + wt		
Max w/c_		Max. Water (lbs/cy) = Design w/c (wt. cement + wt	Fly Ash +Slag) =	
osolute Volumes				
	Cement	(lbs/cy) / (Sp. Gr. X 62.4 X 27)	<u> </u>	
	Fly Ash	(lbs/cy) / (Sp. Gr. X 62.4 X 27)	=	
	Slag	(lbs/cy) / (Sp. Gr. X 62.4 X 27)		
		(155/5)// (op. 51/7/52/7/		
	Water		<u> </u>	
	Water			0.06
	Water	(lbs/cy) / (1.00 X 62.4 X 27)		0.06
	Water	(lbs/cy) / (1.00 X 62.4 X 27)		0.06
	Water	(lbs/cy) / (1.00 X 62.4 X 27) Subtotal	-	
% FA Agg.:	Water	(lbs/cy) / (1.00 X 62.4 X 27) Subtotal 1.000 - Subtotal	=	
% In. Agg.:	Water Air Fine	(lbs/cy) / (1.00 X 62.4 X 27) Subtotal 1.000 - Subtotal Total		
_	Water Air Fine	(lbs/cy) / (1.00 X 62.4 X 27) Subtotal 1.000 - Subtotal Total Aggregate (1.000 - Subtotal) X % In Mix	===	
% In. Agg.: _ % CA Agg.: _	Water Air Fine	(lbs/cy) / (1.00 X 62.4 X 27) Subtotal 1.000 - Subtotal Total Aggregate (1.000 - Subtotal) X % In Mix n. Aggregate (1.000 - Subtotal) X % In Mix	=	1.00
% In. Agg.: _ % CA Agg.: _	Water Air Fine Intern Coars	(lbs/cy) / (1.00 X 62.4 X 27) Subtotal 1.000 - Subtotal Total Aggregate (1.000 - Subtotal) X % In Mix a. Aggregate (1.000 - Subtotal) X % In Mix see Aggregate (1.000 - Subtotal) X % In Mix	=	
% In. Agg.: _ % CA Agg.: _	Water Air Fine A	Subtotal 1.000 - Subtotal Total Aggregate (1.000 - Subtotal) X % In Mix a. Aggregate (1.000 - Subtotal) X % In Mix Be Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total	=	
% In. Agg.: _ % CA Agg.: _	Water Air Fine Intermedian	Subtotal 1.000 - Subtotal Total Aggregate (1.000 - Subtotal) X % In Mix a. Aggregate (1.000 - Subtotal) X % In Mix be Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27	=	
% In. Agg.: _ % CA Agg.: _ ggregate Weights	Water Air Fine Intermedian	Subtotal 1.000 - Subtotal Total Aggregate (1.000 - Subtotal) X % In Mix a. Aggregate (1.000 - Subtotal) X % In Mix be Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 iate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 ce Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Cement (lbs/cy)	=	
% In. Agg.: _ % CA Agg.: _ ggregate Weights	Water Air Fine Intermedian	Subtotal 1.000 - Subtotal Total Aggregate (1.000 - Subtotal) X % In Mix a. Aggregate (1.000 - Subtotal) X % In Mix be Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 iate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 ce Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Cement (lbs/cy) Fly Ash (lbs/cy)	=	
% In. Agg.: _ % CA Agg.: _ ggregate Weights	Water Air Fine Intermedian	Subtotal 1.000 - Subtotal Total Aggregate (1.000 - Subtotal) X % In Mix n. Aggregate (1.000 - Subtotal) X % In Mix se Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 ate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Cement Cement (Ibs/cy) Fly Ash (Ibs/cy) Slag (Ibs/cy)	=	
% In. Agg.: _ % CA Agg.: _ ggregate Weights	Water Air Fine Intermedian	Subtotal 1.000 - Subtotal Total Aggregate (1.000 - Subtotal) X % In Mix In. Aggregate (1.000 - Subtotal) X % In Mix See Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate Total Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 See Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 See Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Cement (Ibs/cy) Fly Ash (Ibs/cy) Slag (Ibs/cy) Water (Ibs/cy)	=	
% In. Agg.: _ % CA Agg.: _ ggregate Weights	Water Air Fine Intermedian	Subtotal 1.000 - Subtotal Total Aggregate (1.000 - Subtotal) X % In Mix n. Aggregate (1.000 - Subtotal) X % In Mix se Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate Total Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 iate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 e Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Cement (lbs/cy) Fly Ash (lbs/cy) Slag (lbs/cy) Water (lbs/cy) Fine Agg (lbs/cy)	=	
% In. Agg.:	Water Air Fine Intermedian	Subtotal 1.000 - Subtotal Total Aggregate (1.000 - Subtotal) X % In Mix In. Aggregate (1.000 - Subtotal) X % In Mix See Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate Total Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 See Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 See Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Cement (Ibs/cy) Fly Ash (Ibs/cy) Slag (Ibs/cy) Water (Ibs/cy)	=	

PROPORTION AND PROBLEM SOLVING

PART A:

Compute the dry batch weights of a cubic yard for an A-3 mix using absolute volumes (IM 529) as the basis for your calculations given the following specific gravities.

SPECIFIC GRAVITIES

Cement 3.14

Fine Aggregate 2.66

Coarse Aggregate 2.68

PART B:

Compute the wet batch weights based on the results from Part A and adjust the basic water batched by correcting for free water (excess water) from aggregates. Convert your answer to gallons. Also, compute the maximum allowable mixing water in gallons. Given the following moisture contents.

Assume Fine Aggregate Moisture = 3.4% Assume Coarse Aggregate Moisture = 0.5%

 What is the total maximum water allowed for 5 cubic yards of C-4 mix 	1. \	What is the	total maximum	water allowed for	r 5 cubic	yards of C-4 mix
--	------	-------------	---------------	-------------------	-----------	------------------

3. What is the water/cement ratio (w/c), given the following information?

Cement	603 lb/yd ³
Free Water	5 gal/yd³
Added Water	27 gal/yd³

4. What is the water/cement ratio (w/c), given the following?

Cement	529 lb/yd ³
Fly Ash	95 lb/yd ³
Free Water	50 lb/yd ³
Added Water	30 gal/yd³

5. What is the maximum number of gallons of water that can be added to a 7 cubic yard load of C-4 WR mix at the paver, given the following information?

Cement	593 lb/yd ³
Free Water	48 lb/yd³
Added water	24 gal/yd³



1. What are the dry batch weights and the actual batch weights for an M-4 mix, given the following information?

Fine Aggregate Sp.Gr. = 2.67 Moisture = 2.8%

Coarse Aggregate Sp.Gr. = 2.65 Moisture = 0.6%

2. What is the total water per cubic yard when 30 gallons per cubic yard is added at the plant and 10 gallons are added to the 7 cubic yard load at the grade?

3. What is the water/cement ratio (w/c)?



1. What are the dry batch weights and the actual batch weights for a C-3 WR mix, given the following information?

Fine Aggregate Source A33510 Moisture 3.0%

Coarse Aggregate Source A10010 Moisture 0.5%

2. What is the total water per cubic yard when 23 gallons per cubic yard is added at the plant and 15 gallons are added to a 7 yd³ load at the grade?

3. What is the w/c?

1. Which weight is more, a cubic yard of B-40C15 mix or a cubic yard of D-57-F15 mix?

Given:

Fine Aggregate Sp.Gr. = 2.66

Coarse Aggregate Sp.Gr. = 2.71

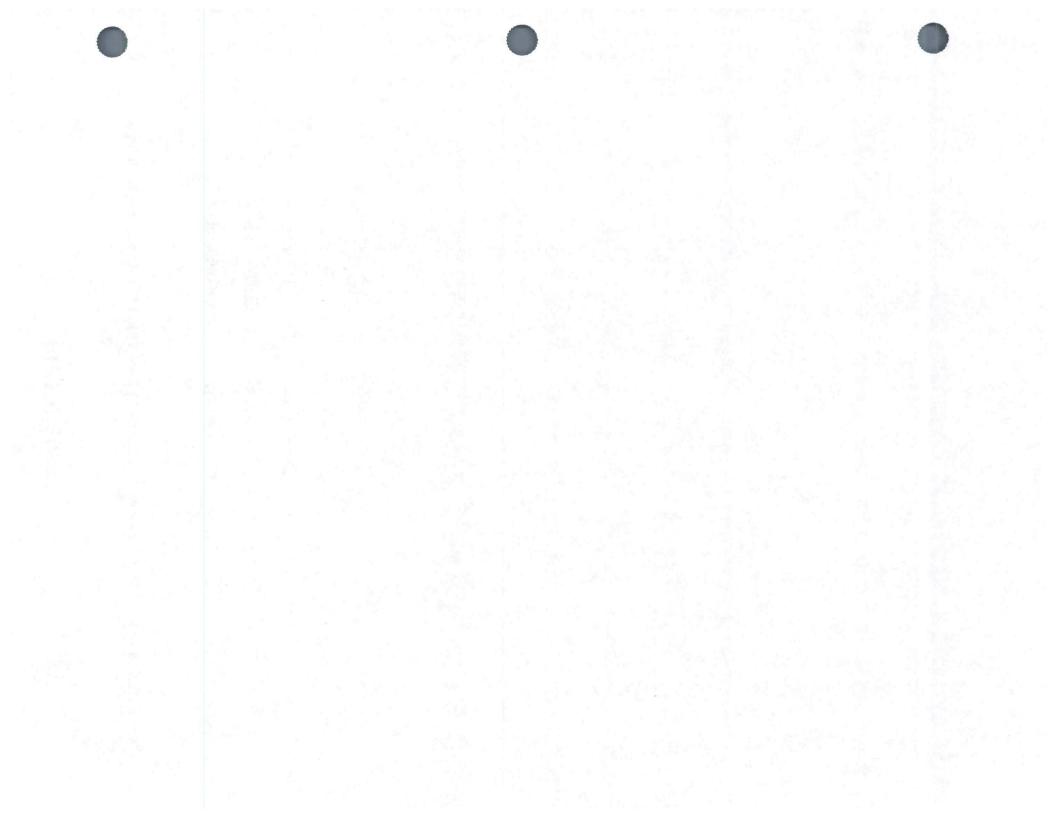
Fly Ash (C) Sp.Gr. = 2.65

Fly Ash (F) Sp.Gr. = 2.60

Cement Sp.Gr. = 3.14

Water Sp.Gr. = 1.00

Note: Assume Sp.Gr. in each mix.



Mix No.:	Pounds Cen	nent:	
1st Adjus	ted lbs. Cement: S	Source:	Sp. Gr.:
I.M. 491.17	Fly Ash: S	Source:	Sp. Gr.:
I.M. 491.14	Slag GGBFS: S	Source:	Sp. Gr.:
2nd Adjus	ted lbs. Cement:		
То	tal Cementitious		
I.M. T-203	Fine Aggregate Source:		Sp. Gr.:
I.M. T-203			Sp. Gr.:
I.M. T-203	Coarse Agregate Source:		Sp. Gr.:
Basic w/c		er (lbs/cy) = Design w/c (wt. cement + wt F	
Max w/c_	Max. Wate	er (lbs/cy) = Design w/c (wt. cement + wt F	ly Ash +Slag) =
Absolute Volumes			
	Cement	(lbs/cy) / (Sp. Gr. X 62.4 X 27)	·
	Fly Ash	(lbs/cy) / (Sp. Gr. X 62.4 X 27)	- <u>- 666</u>
	Slag	(lbs/sy) // Sp. Cr. V 62 4 V 27)	
		(lbs/cy) / (Sp. Gr. X 62.4 X 27)	The state of the s
	Water		
	Water		=
	Water	(lbs/cy) / (1.00 X 62.4 X 27)	=
	Water	(lbs/cy) / (1.00 X 62.4 X 27)	
	Water	(lbs/cy) / (1.00 X 62.4 X 27) Subtotal	=
% FA Agg.:	Water	(lbs/cy) / (1.00 X 62.4 X 27) Subtotal 1.000 - Subtotal Total	=
% FA Agg.: _ % In. Agg.:	WaterAir	Subtotal 1.000 - Subtotal Total (1.000 - Subtotal) X % In Mix	= = = 1.00
% FA Agg.: % In. Agg.: % CA Agg.:	Water Air Fine Aggregate Interm. Aggregate	(lbs/cy) / (1.00 X 62.4 X 27) Subtotal 1.000 - Subtotal Total	= = = 1.00
% In. Agg.: _ % CA Agg.: _	Water Air Fine Aggregate Interm. Aggregate	Subtotal 1.000 - Subtotal Total (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix	= = = 1.00
% In. Agg.: _ % CA Agg.: _	Water	Subtotal 1.000 - Subtotal Total (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix	= = = = =
% In. Agg.: _ % CA Agg.: _	Fine Aggregate Interm. Aggregate Coarse Aggregate	Subtotal 1.000 - Subtotal Total (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix Aggregate Total	= = = = =
% In. Agg.: _ % CA Agg.: _	Fine Aggregate Interm. Aggregate Coarse Aggregate Fine Aggregate Intermediate Aggregate	Subtotal 1.000 - Subtotal Total (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix Aggregate Total (abs vol.) X Sp. Gr. X 62.4 X 27	= = = = =
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Fine Aggregate Interm. Aggregate Coarse Aggregate Intermediate Aggregate Coarse Aggregate	Subtotal 1.000 - Subtotal Total (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix Aggregate Total (abs vol.) X Sp. Gr. X 62.4 X 27	= = = = = = =
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Fine Aggregate Interm. Aggregate Coarse Aggregate Intermediate Aggregate Coarse Aggregate	Subtotal 1.000 - Subtotal Total (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix Aggregate Total (abs vol.) X Sp. Gr. X 62.4 X 27 (abs vol.) X Sp. Gr. X 62.4 X 27	= = = = = = =
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Fine Aggregate Interm. Aggregate Coarse Aggregate Intermediate Aggregate Coarse Aggregate	Subtotal 1.000 - Subtotal Total (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix Aggregate Total (abs vol.) X Sp. Gr. X 62.4 X 27 (abs vol.) X Sp. Gr. X 62.4 X 27 (abs vol.) X Sp. Gr. X 62.4 X 27	= = = = = = =
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Fine Aggregate Interm. Aggregate Coarse Aggregate Intermediate Aggregate Coarse Aggregate	Subtotal 1.000 - Subtotal Total (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix Aggregate Total (abs vol.) X Sp. Gr. X 62.4 X 27 (abs vol.) X Sp. Gr. X 62.4 X 27 (abs vol.) X Sp. Gr. X 62.4 X 27 (abs vol.) X Sp. Gr. X 62.4 X 27 (abs vol.) X Sp. Gr. X 62.4 X 27	= = = = = = =
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Fine Aggregate Interm. Aggregate Coarse Aggregate Intermediate Aggregate Coarse Aggregate	Subtotal 1.000 - Subtotal Total (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix Aggregate Total (abs vol.) X Sp. Gr. X 62.4 X 27 (abs vol.) X Sp. Gr. X 62.4 X 27 (abs vol.) X Sp. Gr. X 62.4 X 27 (abs vol.) X Sp. Gr. X 62.4 X 27 Cement (Ibs/cy) Fly Ash (Ibs/cy) Slag (Ibs/cy) Water (Ibs/cy)	= = = = = = =
% In. Agg.:	Fine Aggregate Interm. Aggregate Coarse Aggregate Intermediate Aggregate Coarse Aggregate	Subtotal 1.000 - Subtotal Total (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix e (1.000 - Subtotal) X % In Mix Aggregate Total (abs vol.) X Sp. Gr. X 62.4 X 27 (abs vol.) X Sp. Gr. X 62.4 X 27 (abs vol.) X Sp. Gr. X 62.4 X 27 (abs vol.) X Sp. Gr. X 62.4 X 27 Cement (Ibs/cy) Fly Ash (Ibs/cy) Slag (Ibs/cy) Water (Ibs/cy)	= = = = = = =

Project No.:				County :	9.5
Mix No.:	Pou	inds Cement:			
1st Adjus	ted lbs. Cement:	Source:	<u> </u>	Sp. Gr.:	
I.M. 491.17	Fly Ash:	Source:	<u> </u>	Sp. Gr.:	
I.M. 491.14	Slag GGBFS:	Source:		Sp. Gr.:	
2nd Adjus	ted lbs. Cement:				
То	tal Cementitious				
I.M. T-203	Fine Aggregate Source:			Sp. Gr.:	1,20
I.M. T-203	Interm. Aggregate Source:			Sp. Gr.:	
I.M. T-203	Coarse Agregate Source:			Sp. Gr.:	4
Basic w/c		Water (lbs/cy) = De	sign w/c (wt. cement + wt F	ly Ash +Slag) =	
Max w/c	N	Max. Water (lbs/cy) = De	esign w/c (wt. cement + wt F	ly Ash +Slag) =	1
Absolute Volumes					
	Cement	(lbs/cy	y) / (Sp. Gr. X 62.4 X 27)	· . =	_
	Fly Ash	(lbs/cy	y) / (Sp. Gr. X 62.4 X 27)		
	Slag	(lbs/cy	r) / (Sp. Gr. X 62.4 X 27)	_	<u>. 1</u>
	Water	(lbs/cy	y) / (1.00 X 62.4 X 27)	- <u> </u>	
	Air				0.060
			Subtotal		
			1.000 - Subtotal		
			Total		1.000
% FA Agg.:		ggregate (1.000 - Subto		= <u>-</u>	
% In. Agg.:		Aggregate (1.000 - Subt		=	19
% CA Agg.:	Coarse /	Aggregate (1.000 - Subt	otal) X % In Mix	- 54	
			Aggregate Total	<u> </u>	
Aggregate Weights	Fine Agg	regate (abs vol.) X Sp	. Gr. X 62.4 X 27		
	Intermediate	Aggregate (abs vol.)	X Sp. Gr. X 62.4 X 27		1.35
	Coarse A	ggregate (abs vol.) X S	p. Gr. X 62.4 X 27		si di
Summary		Cement	(lbs/cy)		
The state of		Fly Ash	(lbs/cy)		
		Slag	(lbs/cy)		
		Water	(lbs/cy)		
		Fine Agg.	(lbs/cy)		
			A CTO AND ADDRESS OF THE ADDRESS OF		
		Interm. Agg Coarse Agg.	(lbs/cy)		



Calculate the batch weights for the following mix using Form 150: C-3WR-C15S35

Given:

Cement - LaFarge

Fly Ash - Louisa Generating

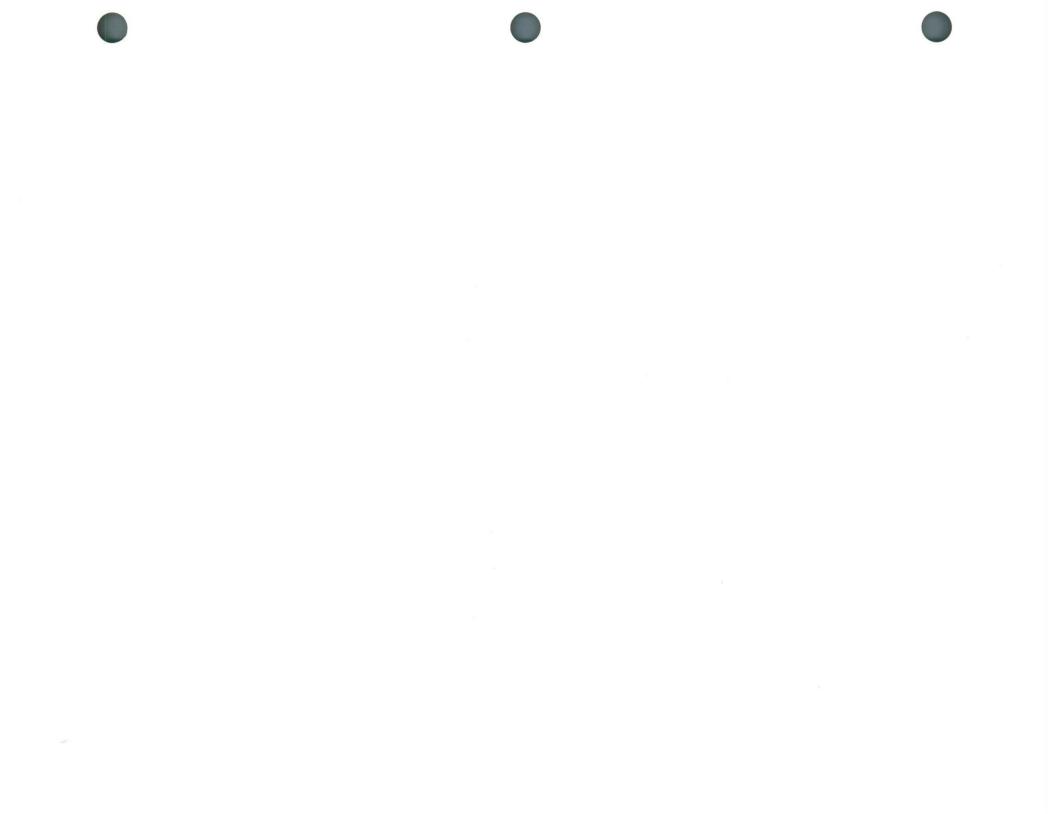
Slag - LaFarge - NewCem

Fine Aggregate – A37514

Coarse Aggregate - A94002

Project No.:				County :	1
Mix No.:	Pounds Cemer	nt:			
1st Adjusted lbs. Cement: Source:			Sp. Gr.:		
I.M. 491.17	Fly Ash: Sou	rce:		Sp. Gr.:	
I.M. 491.14	Slag GGBFS: Sou	rce:		Sp. Gr.:	- 30-7
2nd Adjus	ted lbs. Cement:				
То	tal Cementitious				
I.M. T-203		17 HZ	<u> </u>	Sp. Gr.:	F4 30
I.M. T-203	Interm. Aggregate Source:			Sp. Gr.:	in the
I.M. T-203	Coarse Agregate Source:			Sp. Gr.:	43
Basic w/c	Water	(lbs/ou) = Dos	ign w/c (wt. cement + wt F	ly Ach +Clas) =	
Max w/c			sign w/c (wt. cement + wt F		
Wax W/C_	Wax. Water	(ibs/cy) – bes	iigii w/c (wt. ceilleilt · wt i	ly Asii (Slag) =	
Absolute Volumes					
	Cement	(lbs/cy)	/ (Sp. Gr. X 62.4 X 27)	· • <u>-</u>	Harry.
	Fly Ash	(lbs/cy)	/ (Sp. Gr. X 62.4 X 27)		Pis .
	Slag	(lbs/cy)	/ (Sp. Gr. X 62.4 X 27)	1 - 1	
	Water	(lbs/cy)	/(1.00 X 62.4 X 27)	=	
	Air				0.060
			Subtotal	- <u> </u>	
		1.	.000 - Subtotal	13 (19 = 3)	
			Total		1.000
% FA Agg.:	Fine Aggregate (1	000 - Subtota	al) X % In Mix		
% In. Agg.:	Fine Aggregate (1.000 - Subtotal) X % In Mix Interm. Aggregate (1.000 - Subtotal) X % In Mix			- 1860 (1) - 11 (1)	. 17
% CA Agg.:	Coarse Aggregate (1.000 - Subtotal) X % In Mix				-
A Wainbia		A	ggregate Total		
Aggregate Weights	Fine Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27				48
	Intermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27			<u> </u>	
	Coarse Aggregate (a	abs vol.) X Sp	. Gr. X 62.4 X 27		
Summary	Ce	ment	(lbs/cy)		
		/ Ash	(lbs/cy)		
		Slag	(lbs/cy)		
		Water	(lbs/cy)		
		Agg.	(lbs/cy)		
	Interm.		(lbs/cy)		
	Coarse		(lbs/cy)		







VII.Certified Plant Inspection

IM 527 and Article 2521

A. General

- Certified Plant Inspection will be required for:
 - Primary projects
 - Interstate projects
 - State Park projects
 - Institutional projects
- The Contractor will furnish the Certified Plant Technician for the work specified
- The Plant Technician will be responsible for:
 - Inspection of plant operation
 - Aggregate gradations
 - Identification of materials
 - Testing strength specimens
 - Maintenance of proper reports
 - Other duties as specified in IM 213
 - If test results indicate noncompliance, the Contractor is responsible for deciding corrective action, not the technician



Safety should be uppermost in the minds of those working in concrete plants. The technician should:

- Make certain all contractual safety requirements are met
- Encourage the elimination of hazards
- · Become familiar with hazards
- Wear protective headgear when working around bins and other plant equipment
- Make sure that belt sampling locations are equipped with an On-Off switch

C. Equipment

- Bins (Article 2001.06 and IM 527)
 - The contractor shall maintain any stress carrying-parts of the bin frame
 - Bins must be fully loaded for at least 12 hours before concrete proportioning and the amount of settling determined by the contractor



- If the settlement differential of footings exceeds 1/10 foot (30mm), the District Materials Engineer must be notified
- All other plant machinery shall meet current OSHA standards
- Proportioning Equipment (Article 2001.20 and IM 527)
 - General
 - Proportioning scales and meters shall be test loaded to the maximum load expected during production
 - The DME or a designated staff will witness calibrations before concrete work begins
 - Equipment must be examined at least at 3-hour intervals for correctness of the amount being batched and for damage to the equipment
 - Scale sensitivity shall be checked at least twice a day during a normal working day
 - Cement and Fly Ash Scales
 - Scales must be accurate to within ±0.5% of the load and must operate (delivery tolerance) within ±1% of the required batch amount
 - Cement shipment yield determinations must be made every 10,000 cubic yards (10,000 cubic meters) after the original determination made near the end of the first full day of production
 - Aggregate Scales
 - Must operate within a delivery tolerance of ±1% of the required batch amount
 - Water Measuring Device
 - Water delivered to the batch must be accurate to 2.2 pounds or ±1% of the amount shown by the indicator; whichever is greater

Proportioning equipment must be examined at least at 3-hour intervals for correctness of the amount being batched and for damage of the equipment

Scale Sensitivity shall be checked at least twice during a normal working day

Delivery tolerance shall be checked at least once during a normal working day

Cement shipment yield determinations must be made every 10,000 cubic yards after the original determination made near the end of the first full day of production

- Admixture Dispensing Equipment
 - Equipment for dispensing liquid admixtures must be accurate to ±3% of the quantity required
 - Operation of the dispenser must be observed for uniform delivery at least once during each 3 hours of normal operation
 - The dispensing equipment must be flushed with water at least once a day
- Mixing Equipment (Article 2001.21 and IM 527)
 - Stationary Mixers
 - Mixing time shall be a minimum of 60 seconds and a maximum of 5 minutes
 - Charge time plus discharge time plus minimum mixing time of 60 seconds is the minimum batch cycle time
 - Mixing time must be determined and recorded at least once per dayTruck Mixers
 - Batches must be mixed from 70-90 revolutions at mixing speed
 - Mixing time must be determined and recorded at least once daily
 - Transit mixers must carry a current certification stating that the mixer has been examined in the last 30 days
 - Continuous Mixers
 - Calibration performed by Contactor, witnessed by District Materials
 - Once calibrated in a District, it is not required that it be recalibrated for subsequent projects within that District



Charge time

- + Mixing time (60 sec. Minimum)
- + Discharge time
- = Minimum batch cycle time



- Transportation Vehicles (Article 2301.13 and IM 527)
 - Stationary Mixing
 - Concrete must be placed from non-agitating units within 30 minutes after discharge from mixer. If a retarding admixture is used, this time may be extended an additional 30 minutes
 - Concrete must be placed from agitating units within 90 minutes after the water and cement have made contact with each other
 - Truck Mixing
 - On truck-mounted transits with agitation, concrete must be placed within 90 minutes after the water and cement have made contact with each other. If no agitation is used, the time limit is 30 minutes

D. Material

- Identification
 - Aggregates
 - The plant technician shall verify that all material incorporated in the project is properly certified.
 - Certified aggregate may be incorporated on the basis of the certified truck ticket.
 - Cementitous Material (cement, fly ash, GGBFS)
 - May be incorporated into the project on the basis of the manufacturer's certification.

Determine and record the cement to water contact time at least once each day!



Do not permit any new material to be used or stored with accepted material until satisfied the new material is acceptable.



Water

- Municipal supply systems and potable sources may be used without testing; other sources (lakes, streams, etc.) must be approved by the Central Laboratory.
- Admixtures(Air-Entraining, Retarding and Water-Reducing Admixtures)
 - May be incorporated with no further testing if listed in IM 403. Dosage rates are also included in this IM Any admixture older than 18 months, or suspected of being frozen shall be tested before use.
 - Admixtures shall be mixed once a day to maintain the solids in suspension. Each 100 gallons of solution shall be circulated a minimum of 5 minutes per day.
- · Storage and Handling of Materials
 - Storage and handling of all aggregates must comply with Article 2301.13. The D.M.E. authorizes and is responsible for proper changes.
 - Fine aggregate must be drained at least 24 hours before being used.
 - For both coarse and fine aggregate, moisture content of successive batches must not vary more than 0.5%.
 - Be alert for contamination of aggregate stockpiles.
 - Cementitous materials must be stored in weatherproof enclosures. If lumps develop in cement or fly ash, it must not be used until it has been reprocessed, retested and approved. Cementitous materials, which have been in storage at the project site for more than 60 days or in the producer silo for more than one year, must also be retested and approved.

Admixtures shall be mixed thoroughly **once a day** prior to proportioning.

VI. Concrete Plant Inspection Checklist

I.M. 527

- A. The proportioning equipment must be examined at least at 3-hour intervals for correctness of the amount being delivered and for damage.
- B. The scale sensitivity shall be checked at least twice during a normal working day by placing a mass equal to 1/10 percent of the batch on the fully loaded scales and observing the movement of the indicator.
- C. Check scale operation to determine cement delivery tolerance conformance at least twice during each day of normal operation.
- D. The Standard Specification requires that the cement shipment yield determination must be made at intervals of approximately 10,000 cubic yards (10,000 cubic meters) after the original determination made near the end of the first full day of production.
- E. Check scale operation to determine aggregate delivery tolerance conformance at least once during a normal working day and document.
- F. If water is measured with a scale, the delivery tolerance must be determined at least once for each day of normal operation and document.
- G. Admixture dispensers shall be observed for uniform delivery at least once during each 3 hours of normal operation and document.
- H. Admixture dispensers must be flushed with water at least once daily.
- I. Determine and record the mixing speed and the mixing time at least once daily by using the sweep hand of a watch and counting the drum revolutions in one minute.

- Determine and record the time between batching and placement at least once during each day of normal operation.
- K. Specific Gravity One sample per day for both coarse and fine aggregates for the first three days of normal operation and one for each three days of normal operation for both coarse and fine thereafter, assuming the first three days results are consistent.
- L. Moisture A minimum of one test per each half day of operation.
- M. Gradation (QC) Obtain and test one sample per day. See Construction Department Instruction No. 3.22. Show sample number, name of sampler, and name of tester on lab work sheet.
- If maturity not being used, one 20-in. (508-mm) long beam for each 2000 cu. yd. (1529 cubic meters) of concrete placed. Make flexural tests representing alternating 2000 cu. yd. (1529 cubic meters) placement units at 7 and 14 days.
- O. At the plant, the plant inspector shall remove the specimens, clean the molds, oil and return the molds to the grade at the direction of the paving inspector. The plant inspector shall store the specimens until date of test. The storage space shall be a pit adequate for the project, and for normal projects it should be at least 4 ft. x 6 ft. x 18 in. (1.2 m x 1.8m x .46 m). The specimens shall be wet at all times. If the temperature in the sand filled pit drops below 40°F (4.4°C), remove the speciments and place them under wetted burlap in a heated enclosure or in lime saturated water. See I.M. 328. Note: Lime saturated water is prepared by mixing 1 ounce (30 ml) of hydrated lime with 1 gallon (4 L) of water.

P. When opening is determined by the maturity method, casting beams every 2000 cubic yards (1529 cubic meters) is not required. The plant inspector should ensure curve development is performed according to I.M. 383.

Q. Other duties include:

- Close observation of stockpiling and handling of aggregates. There must be no intermingling of aggregates and no contamination.
- Frequent check on wet batch or dry batch truck cleanliness and degree of discharge.
- Document all the above data in diary.
- Make the following report daily: Plant Reports - Form #800240
- Make the following report as prescribed: Cement Yield Report – Form #820912E
- At the end of the project, make a copy of the plant book for the Engineer.

PCC Level II Structural Plant

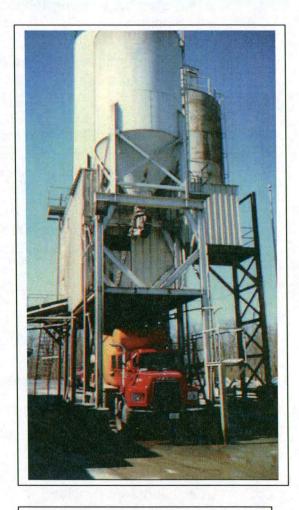
Structural Plant Inspection I.M. 528

Equipment
Elevated, Low-Profile, and Ground Level
Bins

- Tendency for aggregates to be intermingled.
- Intermingled or contaminated materials must not be incorporated.

Proportioning Equipment

- District Materials Engineer approves annually.
- Calibration Report will be posted.
- Vibration and material accumulation cause adjustments to drift
- Small amounts not objectionable.
- Scales not properly sensitized require immediate action
- Plant superintendent or authorized operator representative must make scale and equipment adjustments. Plant inspector not to participate in this activity.
- Plant inspector independently determine if settings or if adjustments are correct and amounts of material in batch are correct.



If material accumulation exceeds one percent of the material batch, it must be removed and readjusted to indicate a zero load within 0.5%.

Scale sensitivity checked at beginning of placement if intermittent or daily if continuous.

1/10 percent of batch on fully loaded scales shall exhibit visible indicator movement.

Strict adherence to plant inspector determine independently to maintain division of authority and to minimize erroneous operations.

PCC Level II Structural Plant

- Suitable wind protection of scales
- Air entraining required for all structural concrete, except Class X.
- Retarding admixture may be required. Water reducer may be used at contractor's option.
- Intermingling of admixtures together may neutralize each other. Introduce separately.

Mixing Equipment

- Truck mounted transit mixers
- Stationary central mixers with in transit agitation
- Stationary mixers located at site
- Concrete mobiles

Sampling and Testing Aggregates

- Specific Gravity
 - 1 per week coarse and fine first two weeks, every other week thereafter.
 - Variations greater than 0.02 from T-203, inform Project Engineer and District Materials Engineer immediately.
- Moisture
 - One sample per lot

Transit mixers must carry current certification signed by responsible company representative - mixer condition examined in last 30 days and free of hardened concrete. It is the responsibility of the CPI to check ready mix trucks for the monthly condition certification.

PCC Level II Structural Plant

- Gradation (QC)
 - One sample per lot.
 - Day's run or 250 yd³
 - Less than 250 yd³ weekly
 - Bridge deck is one lot

Non-Critical Concrete

- The items of work described in IM 528 may be designated as non-critical concrete, when placed at less than 35 cubic yards (30 cubic meters) per week.
- When non-critical concrete is the only concrete produced for the project(s) from a given plant, quality control testing may be reduced to one gradation per two weeks.

Water cement ratio

- Water demand exceeds design w/c ratio and approaches maximum
 notify Project Engineer and District Materials Engineer
- Check aggregate moistures, batch weights, scales, water meter, etc.
- Shall not exceed maximum w/c ratio
- May increase cement content with District Materials Engineer approval

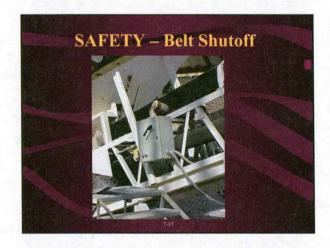
PCC Level II Structural Plant

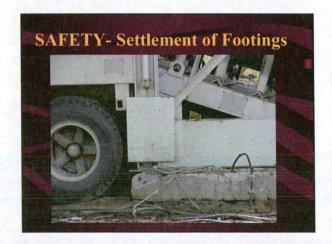
• Strength Tests – IM 316

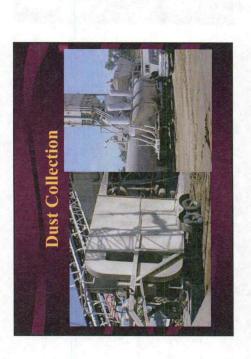
 Required for each section placed or day's placement

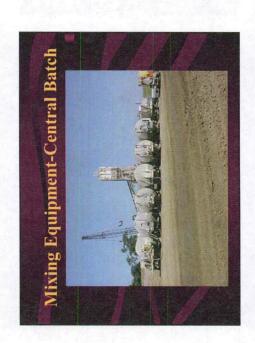
 Abutment walls, pier footings, bridge end posts, and culvert curtain walls not considered critical structural units – strength testing not required.

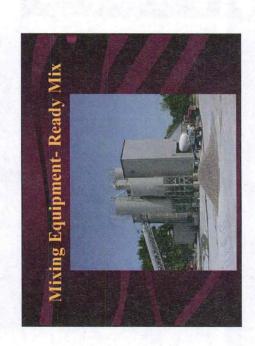


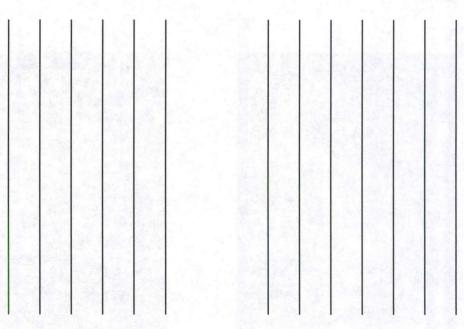


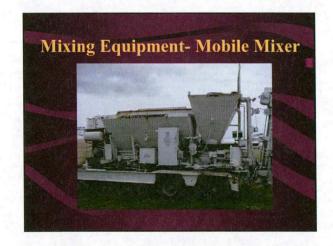


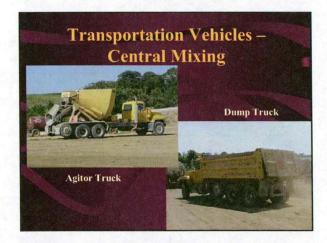


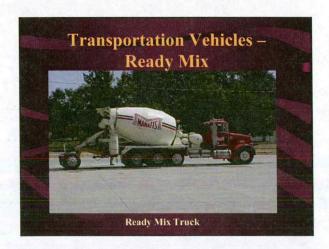


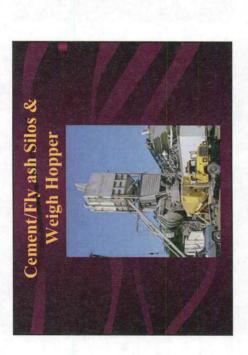


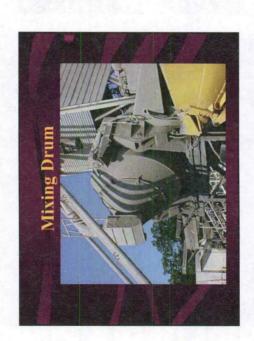


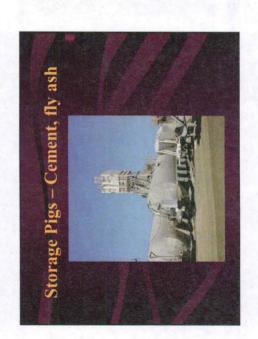


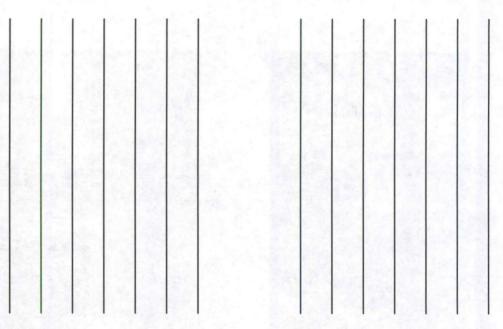


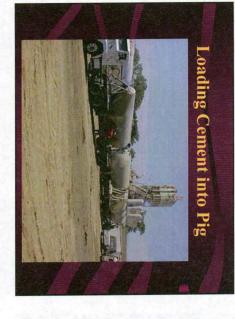








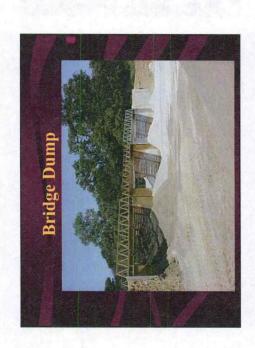


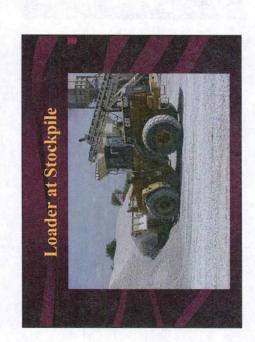


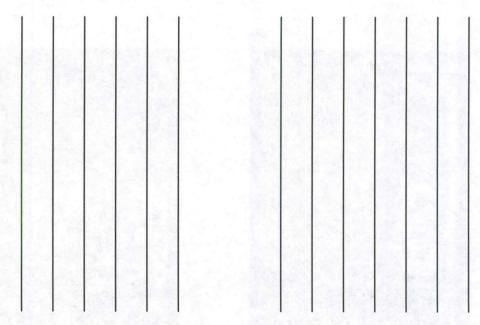


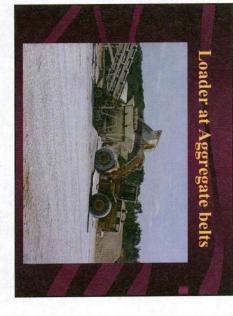
	Admixture Bottles	







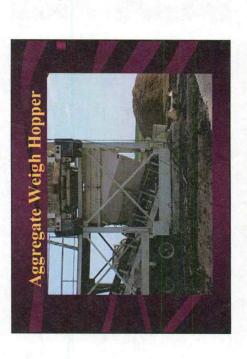


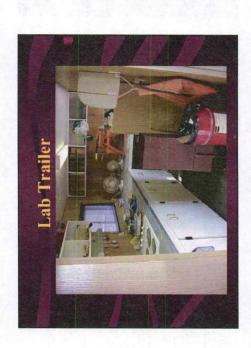


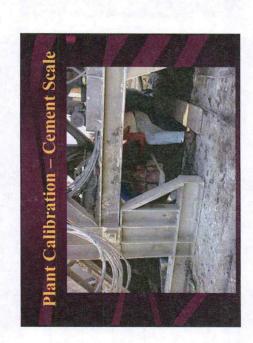


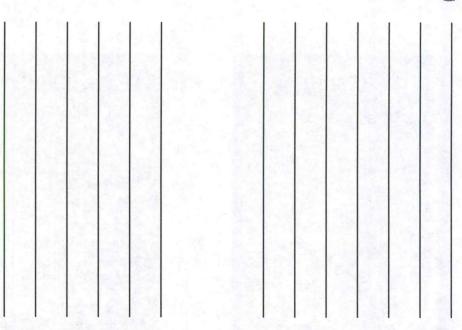
			Aggregate Bins & Weigh Hopper

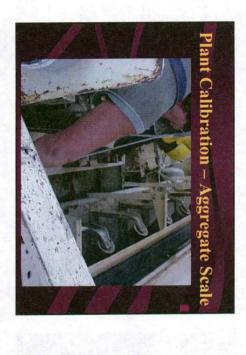
Bins & Weigh Hopper	gregate Belts	

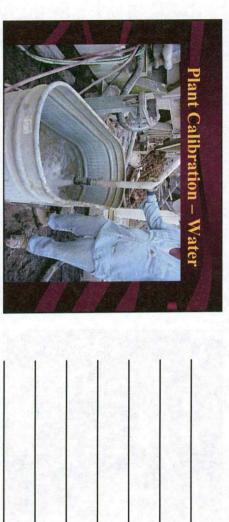












				Plant Calibration – Admix
)	C	ration -
				Admixtu
				ktures
1	ΙI		1	ĭ

alibration – Admixtures		Calibration – Water









PCC Level II References

VIII. References

Instructional Memorandums

- Volume II
- Volume IV

PCC Reference Manual

- IMs and Specifications pertaining to PCC Inspection and Testing
- · Needs Updated Annually

Specifications

- Article 2301 Portland Cement Concrete Pavement
- Article 2403 Structural Concrete
- Article 4100 General Provisions
- Article 2001 General Equipment Requirements

General Supplemental Specifications

GS-01013 - October 2007

Supplemental Specification (SS) or Special Provisions (SP)

· Applied to specific projects, QMC

Construction Manual

- 3.07 Monitoring Program
- 9.00 Portland Cement Concrete Pavement
- 11.50 Concrete

Contract Documents

Proposals

Concrete Specifications Summary (U.S. Units)

CAUTION: CONSULT THE APPLICABLE SPECIFICATIONS FOR REQUIRED AIR CONTENT AND SLUMP BEFORE USING THIS CHART.

January 2008

Concrete Application	Type conc.	Slump- Min.	in. Max.	Target	% Air Co Min.	nten Ma	
Paving	ABC	N/A	N/A	Soc	Specification		2301.04 B&C
Slip Form						_	
Non Slip Form	ABC	1/2	4	7	6	81/2	
Conc. Base (Non Slip Form)	Α	1/2	4	7	6	81/2	2301.04 & 2201
Curb & Gutter	C		3	7	6	81/2	2512.03 & 2301.04
Sidewalk	С		4	7	6	81/2	2511.03 & 2301.04
ntakes & Manholes REPAIR	С	1	3	61/2	51/2	8	2403.03 & 2503.03D
Patches With CaCl	M-4, M-V	1 prior t add. of C		5	3	7	2530.03B & 2529.02B
Patches		Targe	t				
Without CaCI	М	1 to 3 Max, 4		61/2	5	8	2530.03B & 2529.02B
Underseal & Grout	ing, Flowir	ng Mortar		By Flow Cone			2539.03 & 2506.02B
	C-4 WR, C-4 WR-C	11.64	Sam	e as specified	concrete		2310.02
STRUCTURES							
Seal Coat	X	0	8		0	0	2405.05
Sub-Structure Super-Structure	С	1 to 3		61/2	51/2	8	2403.03 A&B 2412.02
Slope Protection	С	1	3	61/2	51/2	81/2	On the Plan Sheet
Piling Encased,		Targe	t				CONTRACTOR OF THE PARTY OF THE
Piling Brg. (Encase	ed) C	1 to 3 Max. 4		61/2	51/2	8	2403-2501.04C-2501.19
		Target 4					
Bridge Deck Overla	ay O	0	1	61/2	51/2	81/2	2413.02A
	HPC	(2-4 min. c					0440.000
Dalaba Dask	HPC	1	4				2413.02B
Bridge Deck	0.000	1	3	61/2	F		2403.03 A&B, 2412
Class B Repair	0 or D	1	3	61/2	51/2	8	(2413.05)
	D	1	3	7	6	0.00	2513.03B
w/Overlay	U	100	3	,	0	61/2	
Barrier Rall			-				2403.03B
Cast in Place	С						2513.03B
Slipform	BR	0	2	7	6	81/2	2414.02
Julyioiiii			-			01/2	In Special Prov.
ightweight Conc.							2403.04
BARRIER RAIL		Target	17			1117	2513.03A
E 44ABCDE, RE 46	BR	1	3	7	6	81/2	2403.03 A&B
		Max. 4					
LIGHTING & HWY. S	IGNING	Target		101			STATE OF THE PARTY
oundation	C	1 to 3		61/2	51/2	8	2403.03 A&B
		Max. 4					
END ANCHORS		Target					
RE 26AB, RE 28	D	1 to 3		61/2	51/2	8	2403.03 A&B
		Max. 4					
- 1985		Target			1 1 1 1		
RE 29A, RE 29B	C	1 to 3			4	7	2403.03 & 2505.04B
RE 33AB, RE 52, RE	53	Max. 4		Little on the			
Shot Crete					6.1		2424.01

Concrete Specifications Summary (Metric Units)

CAUTION: CONSULT THE APPLICABLE SPECIFICATIONS FOR REQUIRED AIR CONTENT AND SLUMP BEFORE USING THIS CHART.

January 2008

Concrete Application	Type Conc.	Slumi Min.	o-mm Max.	Target	% Air C	ontent Ma	
Paving						Die Co	
SIIp Form	ABC	N/A	N/A		Specification		2301.04 B&C
Non-Slip Form	ABC	15	100	7	6	81/2	2301.04 B&C
Conc. Base (Non Slip Form)	Α	15	100	7	6	81/2	2301.04 & 2201
Curb & Gutter	С		75	7	6	81/2	2512.03 & 2301.04
Sidewalk	С	1 10	100	7	6	81/2	2511.03 & 2301.04
ntakes & Manholes REPAIR	С	25	75	61/2	51/2	8	2403.03&2503.03D
Patches With CaCl	M-4, M-V	25 prio add. o		5	3	7	2530.03B& 2529.02B
Patches Without CaCl	М	25 t	get 0 75	61/2	5	8	2530.03B & 2529.02B
Underseal & Grout	ing, Flowl		. 100	By Flow Cone			2539.03 & 2506
OVERLAYS Thin Bond PCC	C-4 WR, C-4 WR-C	4 10	Sam	e as specified	concrete		2310.02
STRUCTURES		•	200	ALICE MADE			0405.05
Seal Coat	X	0	200		0	0	2405.05
Sub-Structure Super-Structure	С	7arget 25 to 75 Max. 100		61/2	51/2	8	2403.03 A&B 2412.02
Slope Protection	C	25	75	61/2	51/2	81/2	On the Plan Sheet
Piling Encased,			get			0112	
Piling Brg. (Encase	ed) C	25 t	0 75	61/2	51/2	8	2403-2501.04C-2501.1
and the state of the state of	12/21/14	Targ	et 20	1 1 24 12 5	- 3	,	The state of the s
Bridge Deck Over	lay O	0	25	61/2	51/2	81/2	2413.02A
	HPC	(2-4 mi) 25	n. delav) 100				2413.02B
Bridge Deck	1		1347 14-17	11/12		-	2403.03 A&B, 2412
Class B Repair	OorD	25	75	61/2	51/2	8	(2413.05)
Barrier Rail							2413.01
w/Overlay	D	25	75	7	6	81/2	2513.03B
			A THE		e Nieuwill		2403.03B
Barrier Rall							2513.03B
Cast in Place	C			350 at 10			2444.02
Slipform	BR	0	50		6	81/2	2414.02
Lightwolaht Con-							In Special Prov.
Lightweight Conc BARRIER RAIL		74	rant				2403.04 2513.03A
RE 44ABCDE, RE 4	5 BR	25	rget 75	7	6	81/2	
RE 44ABODE, RE 4	DK		. 100		0	61/2	2403.03 MaB
LIGHTING & HWY.	SIGNING	Tar			7 ()		THE RESERVE OF THE PERSON NAMED IN
Foundation	C	25 to		61/2	51/2	8	2403.03 A&B
· Januarion		Max.				-	2.55.05 Flat
END ANCHORS		Tar		Tell 1	100		PARTITION OF THE REAL PROPERTY.
RE 26AB, RE 28	D	25 to Max	0 75	61/2	51/2	8	2403.03 A&B
7 E. P. St. 150			get	10 Carlot 1	To Berry		THE PART OF STREET
RE 29A, RE 29B RE 33AB, RE 52, RE	C 53	25 to Max	0 75		4	7	2403.03 & 2505.04B
Shot Crete							2424.01

beams, samples of aggregates or other materials, and the products of project site clearance.

Complete cleanup of the construction area or plant site, including test materials, is the responsibility of the contractor.

3.05 SALVAGED PROJECT MATERIALS REPORTING

Many project plans indicate that some removal items shall be stockpiled or salvaged to a nearby maintenance facility. To accomplish documentation of these items, a "Salvaged Project Materials" form has been developed. Copy the form in *Appendix 3-1* as needed.

The form shall be completely filled out any time project materials are salvaged to a maintenance facility. The form needs the signature and initials of the project inspector and the maintenance employee who received the material.

Distribute a copy of completed form to project engineer, area maintenance manager, Office of Inventory, and project file. The Office of Inventory will add the salvaged items to the 999 series of inventory for the maintenance facility that received these materials. Include copy of completed form in the final payment packet for the project per *Construction Manual 2.45*.

3.06 NOTICE OF SUSPENSION OR RESUMPTION OF WORK

The "Notice of Suspension or Resumption of Work" (Form 810036) shall be used to order a contractor to suspend work because of violation of specifications or a dispute regarding the quality of materials or manner of performing the work, as provided in *Specification 1105.09*. This notice shall include a description of the work to be suspended.

Upon settlement of the question at issue, the "Notice of Suspension or Resumption of Work" (Form 810036) shall be reissued to release the contractor from the work suspension order. Although the work suspension order may be issued by the inspector, the release requires the project engineer's signature.

Copies of the "Notice of Suspension or Resumption of Work" (Form 810036) should be given to the contractor, District Construction Engineer (DCE), and project engineer.

3.07 REQUIREMENTS FOR MONITORING THE CERTIFIED PLANT INSPECTION PROGRAM AND QUALITY MANAGEMENT - ASPHALT (QM-A)

The monitoring requirements listed in the appendices are intended to be the minimum for HMA or PCC plant operation. Field problems may necessitate increased monitoring. For PCC plant inspection, all monitoring requirements, except for plant calibration, will be performed by construction personnel. For HMA projects, monitoring responsibilities are shared between the plant monitor, grade inspector, and materials personnel. Materials personnel will primarily monitor activities involved with HMA materials production process and quality such as plant calibration, QM-A lab operation, contractor field process control, and for QM-A projects, will resolve discrepancies between the District Materials Lab and Contractor Lab results. Construction personnel will be primarily involved in administration and inspection activities. Materials engineers and resident construction engineers may mutually coordinate and shift responsibilities between personnel on an individual project basis to achieve the most efficient use of their respective personnel and minimize unproductive time spent at the contractor's HMA plant. See *Construction Manual 3.20* for responsibilities of project acceptance sampling

and testing.

On certified plant inspection projects, it is a requirement for the plant monitor to be a certified technician for the type of work involved.

QM-A requirements can be considered an expansion of the certified plant program for HMA. In addition to normal certified plant inspection duties, under QM-A the contractor is also required to design and submit their own mix designs for agency approval. At the plant, the contractor is required to analyze and control mix production properties through frequent field testing, based on specified gyratory or Marshall mix design criteria.

For a QM-A project, the plant monitor must be a certified HMA technician. This certification is obtained by attending the Level I HMA course and passing the required examinations.

It is imperative that project engineers maintain an adequate staff of trained, experienced plant monitors. This can be accomplished by having employees participate in the appropriate technician training and certification programs and pass the examinations.

Certified plant inspection will apply to items of work as defined in *Specification 2521.03*. Any items of work excluded from certified plant inspection will be as noted in contract documents. Work excluded from certified plant inspection will also be excluded from QM-A requirements.

In the event the contractor's certified HMA technician is absent, the contractor must contact consultants or other available certified technicians to arrange for inspection.

For duties performed by the certified HMA technician on QM-A projects, the contractor must also contact consultants or other sources for available certified technicians in cases of absenteeism. Because of the laboratory skills necessary to perform this work and the decision making authority as a representative of the contractor, it is not possible or appropriate for the project engineer to provide certified HMA technician services to the contractor in cases of unexpected absences. If the contractor fails to provide certified HMA technicians as required by specification, work covered by QM-A shall be suspended until the project is properly staffed.

Portland Cement Concrete Paving Plant Monitoring

Appendix 3-2 lists the minimum monitoring requirements. A plant monitor will normally be assigned to each project with duties split between plant and grade inspection. Plant monitor should schedule work so the plant can be visited daily during production. The amount of time spent at the plant will depend on the overall quality control at the production plant.

Test beams for determining flexural strengths are to be transported from the grade to the plant site by contracting agency personnel.

Structural Concrete Plant Monitoring

Appendix 3-3 lists the minimum monitoring requirements. The project engineer and contractor should agree in advance whether aggregate gradations, moisture, and specific gravity tests will be waived for concrete which is furnished at a maximum rate of 20 m³ (25 cubic yards) per day. This determination should be in accordance with *Materials I.M.* 528.

Ready mix tickets shall be prepared and signed by the certified plant inspector.

Test beams for determining flexural strengths are to be transported from the grade to the plant site by contracting agency personnel. The certified plant inspector is responsible for curing and storage of the beams. Contracting agency personnel are responsible for testing and reporting results.

Hot Mix Asphalt Paving Plant Monitoring

Appendix 3-4 lists the monitoring requirements. Responsibilities are shared between the plant monitor, grade inspector, and materials personnel. A plant monitor will normally be assigned to each project with duties split between plant and grade inspection, and may also be assigned to multiple projects under construction at the same time. The plant monitor should schedule work so that the plant can be visited daily during production, as required by Appendix 3-4. The amount of time spent at the plant, beyond minimum requirements, will depend on the overall quality control at the production plant. The project inspector will be providing production and placement information to be entered on the daily plant report.

Visits by the project inspector to the plant laboratory for exchange of information and to perform administrative activities will normally be done daily.

The plant monitor will typically be responsible for performing the density testing on HMA core samples.

Plant Reports

The project engineer should make arrangements with the certified technician for timely distribution of plant reports. On QM-A projects, the contractor shall FAX a copy of the daily plant report and QM-A Summary Sheet to the District Materials Engineer on a daily basis. The original and all copies of the plant report shall be kept at the plant until all documentation is completed. Normally, this will be the day following the end of the reporting period. Review and distribution of the reports will be made by the project engineer. This distribution will include a copy to be returned to the certified technician. Prompt consultation with the certified technician and monitor shall follow any significant error or omission.

Documentation

A documentation sample for the plant monitor is contained in *Appendix 3-5*. A separate field book should be set up on each project to document plant inspection. Some flexibility in the suggested format may be necessary depending on project size, type of plant, and if QM-A applies. It is important to document discrepancies and corrective action taken by contractor.

A copy of this documentation must be furnished to the District Materials Engineer (DME) at the time of project acceptance. Also include the certified technician's name, certificate number, and statement from the monitor regarding the work performance of certified technician. It may be necessary to consult with the DME regarding contractor technician performance for Marshall testing duties on a QM-A project. A sample format for providing this documentation is contained in *Appendix 3-6*.

Specification Violations

Failing test results are to be recorded on the daily plant report by the plant inspector.

Verbal notification of such failing results shall precede completion of paperwork to assure timely changes.

Failing test results on QM-A projects related to specified moving averages will be noted on the certified HMA technician data sheets and quality control charts. Special notes on these failures will also be reported in the comment section of the daily plant report. When average points move outside the specification limit, HMA mix production operations shall cease until the contractor proposes meaningful corrective action. The corrective action must be discussed with the DME prior to production start-up.

The plant monitor will convey to the responsible project inspector all specification violations, discrepancies in results with the plant inspector, and improper procedures and equipment used by the plant inspector. The project inspector will issue noncompliance notices for failing test results and inadequate testing procedures or equipment.

In order to use the contractor quality control test results for the acceptance decision, they must be validated by agency verification tests. It is important to notify the contractor and the DME when the results do not compare within the validation criteria in the Materials IM. The lot of material cannot be accepted until the validation issue is resolved by the DME.

All improper procedures, unresolved test discrepancies, or failure to perform inspection duties will be considered by the DME for possible decertification or other appropriate corrective action.

The role of the plant monitor is vital in assuring the DME is aware of any deficient or otherwise unsatisfactory work of the certified technician.

Testing Equipment & Supplies

Certain testing equipment is available for purchase from Department stock. Producers should refer to HMA and PCC Plant Inspection Manuals for specific information and Office of Materials Lab contacts. A list of equipment suppliers is included in the plant manuals.

Necessary plant inspection forms will be furnished to the producer at no cost. The producer can request these through the DME or project engineer. It is a good idea for the plant monitor to carry a supply of forms and make these available to the producers as needed.

The plant monitor can utilize contractor-furnished equipment for testing required at the plant site. HMA core density testing will most likely be done using the same balance, water bath, and thermometer as the contractor. Verification gradation testing should be done at a separate laboratory from the contractor's if possible.

Samples

Verification samples are to be taken by agency personnel or by contractor personnel when directed and witnessed by agency personnel. Materials IM 204 will indicate when contractor sampling assistance is required.

Verification samples that are not tested should be retained until the lot has been

accepted.

If required by contract documents, transportation of secured verification samples to the District Materials Lab shall be performed by the contractor.

CHAPTER 9 PORTLAND CEMENT CONCRETE (PCC) PAVEMENT

9.00 GENERAL

9.01 PRE-CONCRETING CONFERENCE

On all projects involving PCC pavement, the Project Engineer and inspectors should meet with appropriate contractor and supplier personnel to discuss concrete production and pavement placement quality issues before any materials are placed. When ready mix concrete is used, the ready mix producer should also attend.

For the various types of work, the following items should be covered:

- Approvals and required quantities of aggregate and cement, class of mix, time and rate of delivery, percent of air, slump, batch weights, volume per truck, total quantity required, preparation of delivery tickets, testing arrangements, procedures in case of load rejection (can air be increased or a wet load dried by adding cement and aggregate), responsibility for setting batch weights and amount of admixtures, placing, finishing and curing arrangements, and personnel work assignments.
- Settings and condition of paving equipment, dust control, subgrade treatment, procedure for checking steel placement, utility and street return box outs, heading-up equipment, joint sawing and cleaning, joint sealing, rain damage prevention, and cold weather protection.

Only one pre-concreting conference is considered necessary for thoroughly discussing the work, responsibilities, and duties of all involved in the project. On small projects it may be possible to include a pre-concreting conference with the preconstruction conference.

9.02 "PCC PLANT PAGE" (FORMS 800240E and 800240M)

The daily inspection report on paving work is a record of the construction progress, working conditions, weather, etc. during paving and plant operations which may affect pavement quality. This report keeps district and central offices advised on job status and serves as a detailed permanent record of the paving project. At the end of each day on which any pavement was placed, this report is to be completed by field inspection staff for appropriate distribution. Copies of forms are included in *Appendix 9-5*. Refer to *Materials I.M.* 527 for instructions on preparing and distributing this form.

9.03 USE OF COMMERCIAL READY MIX CONCRETE ON PAVING PROJECTS

When the concrete source for a paving project is a commercial ready mix plant, each truck load of concrete must be identified by Form 830212 or an acceptable alternate plant ticket. A current copy of the Form 830212 is included in *Appendix 9-1*.

Required Information:

■ For continuous mainline paving, Form 830212 shall be filled out completely for the first truck. Tickets for subsequent trucks need only to have the Truck No., Ticket No., Conc. This Truck, Time Batched, Water Subtotal, and Maximum Water Allowed portion filled out. When any change in the moisture content, plant adjustments in mixing water, or any other changes to the batching or materials in the concrete are made, a complete ticket must be filled out.

For intermittent production other than mainline paving, such as bridge approaches and street returns, all information on Form 830212 is required for each load because of the greater possibility of need for water adjustment on grade.

Any water added on grade must be documented. Moisture tests must be made frequently to insure uniformity in concrete consistency. Discharge time must be entered on Form 830212 for each load.

9.04 CONCRETE DELIVERY TIMES

To insure that quality concrete is incorporated into pavement, maximum delivery times have been included in *Specification 2301.13D* for both continuous agitation (agitor and ready mix trucks) and non-agitated trucks (dump trucks).

These delivery times should be verified at least once during each day of normal paving. Per *Materials IM 527*, cement to water contact time should be recorded at least daily. These verifications should be recorded in project field books. During hot, dry, windy weather, maximum time limitations listed in specifications are critical limits to insure that quality concrete is being placed and incorporated into project.

included in Appendix 9-6. Project specific circumstances may dictate that repair methods other than those listed in Appendix 9-6 be allowed with approval of the Project Engineer.

D. Shrinkage Cracks

Remove and replace affected areas with new pavement in severe cases.

Minor cracks may be filled with pressure injected epoxy or repaired using Class A bridge floor repair methods.

E. Rough Pavement Sections

Surface variations, which exceed the specification smoothness requirements, require correction by the Contractor. Surface correction shall be accomplished with approved diamond grinding equipment. Use of milling machines, Roto Mill, Galion Scarifier, or other impact devices shall not be permitted.

F. Limitations

Necessary corrective measures on hardened concrete shall only be made after concrete attains age and strength requirements in *Specification 2301.31*.

All required corrective measures shall be completed prior to coring for pavement thickness measurements.

Consultation with the Office of Construction is recommended before placing an HMA or bonded PCC overlay.

9.54 MUD BALL REPAIR

Occasionally mud balls appear in the surface on new concrete pavements. These usually are due to clay balls from a quarry or mud thrown into dump trucks from a portable batch plant located at a wet site, trucks dropping mud from their axles when dumping from a bridge over a dump pit, or end loader operators digging too deep when removing material from a stockpile.

Correction of any discovered mud balls in a pavement surface shall be as follows:

- Any thin concrete skin around the perimeter of the mud ball should be removed so that nearly vertical void walls remain.
- Each void shall be cleaned by a high pressure washer, followed by air blasting to dry the void.
- Voids shall be filled with material meeting Materials I.M. 491.20, Appendix A. This
 material shall be used according to manufacturer's recommendations.
- The surface of filled voids shall be given the same texture as the surrounding pavement.
- A void repair shall be given the proper cure time recommended by the manufacturer prior to opening the roadway to normal traffic.

If a severe problem with mud balls is suspected on a specific project, formal acceptance by the Project Engineer should be delayed until the following spring. This will allow the winter freeze-thaw cycles and snowplowing activities to expose additional mud balls located adjacent to pavement surface. These newly discovered mud ball areas will then also require corrective measures as stated above.

9.55 COLD WEATHER PAVING AND PLANT OPERATIONS

Cold Weather Pavement Protection

During cold weather, *Specification 2301.19.B* requires that newly placed paving, less than 36 hours old, be protected against freezing temperatures. This protection is necessary to allow the hydration process of the curing concrete to continue in cold weather. Adequate protection of concrete allows for paving to be placed later in the season.

The required cold weather protection needed during any given day should be mutually agreed upon between the Contractor and Project Engineer. A daily predetermined weather forecast should be used. For example, the low temperature forecast from the 4:00 pm local radio newscast could be the agreed upon temperature forecast. Once a decision is made as to the appropriate cold weather protection needed, any changes to the amount of protection needed must be agreed between the Contractor and Project Engineer to avoid potential claims.

Below -4° C (25° F), *Specification 2301.19B* requires four layers of burlap between layers of 1.0 x 10⁻⁴ mm (4 mil) plastic or an equivalent commercial insulating material approved by the Project Engineer. Equivalent materials include:

- 3 layers of Burlene
- 1 layer of Fast Track Blankets per Specification 2301.19
- 1 layer of insulating blankets with a minimum R-value of 1.0
- 1 layer of 12 mm (1/2 inch) extruded polystyrene, must be weighted down
- 2 layers of 6 mm (1/4 inch) air celled polyethylene
- 1 layer of 12 mm (1/2 inch) air celled polyethylene

Specification 2301.19B also includes provisions for removal of the cold weather protection. Often a night or two of low temperatures is followed by several days of warmer temperatures. The provisions in 2301.19B provide a means for allowing the removal of cold weather protection when it will no longer be necessary. This is especially important in that it allows the Contractor to reuse covering materials more quickly rather than unnecessarily leaving them on pavement that no longer needs to be covered.

When cold weather protection is required, the Contractor will be reimbursed for extra work per *Specification 2301.35*. The reimbursement amount is the same value regardless of number of layers of protection required.

Cold Weather Plant Operation

Specification 2301.29 states that concrete mixing and placement may be started when the air temperature is at least 1° C (34° F) and rising. In the late fall season before the subgrade begins to freeze and soil temperatures are still relatively warm, it is permissible to allow paving plant operations to begin below1° C (34° F) providing a decent weather forecast is predicted. Paving plant operations basically self regulate during these conditions.

The intent is to maximize the remaining good paving weather still available in the fall. This provision is not intended to make a paving day out of one that is not, but to allow for as much concrete pavement placement as possible during a day forecast for good weather.

After the subgrade begins to freeze, the above provisions should be halted and specifications strictly enforced.

9.56 CURING APPLICATION

The cure shall be applied to the pavement as soon as practical after the finishing operation is complete. This is normally applied with a machine that both applies the curing compound and creates the texture. This is a stop and go operation since curing and texturing can be accomplished faster than the paving operation. Curing shall not be delayed simply because the tines are creating too deep of a texture groove. The goal is a shallow groove and the texture machine can be adjusted in order for the tines to apply less pressure on the surface of the fresh concrete. With a consistent concrete mixture, the downward pressure on the tines can be adjusted in order to allow the tining machine, and thereby the curing process, to be kept right behind the finishers.

The curing shall be applied no later than one half hour after placement. In very hot, dry, windy conditions this is not soon enough. A price adjustment schedule is provided as Table C5 in Appendix 2-34C for areas of pavement where cure is not applied in a timely manner.

9.60 CONCRETE MATERIALS ISSUES

9.61 CONCRETE SAMPLING LOCATIONS

Concrete samples shall be taken as described in *Materials I.M. 327*. The sample location point shall be after plastic concrete has been placed on the grade, either by direct depositing from a batch truck or by use of a placer/spreader machine. On slipform paving projects, the optimum sample location is between placer/spreader and slipform paver machines. For safety considerations, samples may be taken from concrete deposited on the grade in front of the belt placer. Care should be taken to avoid sampling concrete that has been vibrated manually or mechanically. Samples should be taken at locations within the batch that appear to be representative.

9.62 TESTING PROCEDURES

When making test specimens, a sample should consist of about 0.03 cubic meters (one cubic foot) and should be remixed a minimum amount by use of a shovel to ensure uniformity. For routine air and slump tests, smaller samples may be used.

For standard methods of tests, refer to *Materials I.M. 327* (Sampling Freshly Mixed Concrete), *Materials I.M. 316* (Flexure Strength Tests), *Materials I.M. 317* (Slump Test), *Materials I.M. 318* (Air Content Test), and *Materials I.M. 328* (Making, Protecting, and Curing Beams).

9.63 AIR ENTRAINMENT IN PLASTIC CONCRETE

Specification 2301.04.C discusses the required percent of entrained air needed for concrete paving mixes. These percentages have been developed to allow for loss of entrained air as the plastic concrete is placed and consolidated as it goes through the paving operation. The concrete paving mixes have been developed to provide for consolidated concrete containing a 6% air content. To allow for this air loss through the paving operation, tests will be conducted both before and after the paver and a target air content determined. Specification 2301.04.C specifies the procedure that shall be used. The following process will be used in verifying entrained air content in PCC paving mixes:

Control of Air Content

QMC Paving Projects

On the first air test of each day, the contractor and agency shall run side by side tests to ensure air meters are within the tolerance in IM 216. If the air tests are outside the tolerance, the air meters should be calibrated in accordance with IM 318.

The unconsolidated air content limits will be established according to 2301.04C using witnessed contractor quality control test results. The contractor shall notify the engineer whenever an individual quality control test result is outside the tolerance for the target air content.

Non-QMC Paving Projects

The unconsolidated air content limits will be established according to 2301.04C using agency test results. The agency will notify the contractor whenever an individual test result is outside the tolerance for the target air content.

Verification

Lot acceptance shall be based on the agency verification test results on the

unconsolidated mix on the grade. A lot is defined as the amount of a concrete mix placed since the last complying verification air content test.

Air Content Outside Tolerance

When a verification test result is outside the tolerance for the target air content, the contractor will be notified immediately. An air test will then be immediately run behind the paver to aid in identifying the limits of the non-complying air. In addition, the non-complying load will be tested behind the paver to ensure an accurate target air content. If found to be inaccurate, the target air content will be adjusted immediately based upon the air loss and a second lot verification test will be run. If the target air content is found to be accurate, the contractor shall make immediate adjustments to the mix production and placement process to bring the air content back within tolerance. Succeeding loads below the lower target air content tolerance by more than 0.5 % shall not be used. Each subsequent truck will be tested until air content is within tolerance for two consecutive loads. A price adjustment will be applied to all incorporated, non-complying loads that are out of tolerance.

Air Content More Than 0.5% Below Lower Target Content

When the lot verification test result is below the lower target air content by more than 0.5 percent, the contractor may elect to take concrete core samples from the pavement to define the portion of the lot that is non-complying. The lot will be divided into equal 200 square yard (170 square meter) sublots, from the last complying verification test, or witnessed and documented quality control test. A randomly located core will be identified in each sublot. Coring will be at the contractor's expense. The agency will direct and witness the taking of cores. The contractor may either:

- 1) Provide the agency with the cores for testing by Materials Laboratory Test Procedure 407.
- 2) Provide an independent laboratory for testing and a test procedure acceptable to the agency. The agency will take possession and ship the cores at the contractor's expense. Results will be directly reported to the agency and the testing will be at the contractor's expense.

A price adjustment will be applied to sublots represented by cores with an entrained air content below 5.0 percent.

Appendix 2-34(C) is the price adjustment table that lists price adjustments to be applied to concrete in which test results fall outside the specified limits.

Aggregate Correction Factor

Note: Per Materials I.M. 318, an adjustment to the target air content called an aggregate correction factor may be required for some quarries in east central lowa that have highly absorptive aggregates. The aggregate correction factor may be obtained from the District 6 Materials Office. The target air content for PCC mixes utilizing these aggregates would be the specified target for the application plus the aggregate correction factor (see example below). Applying the aggregate correction factor when using aggregates from these quarries helps ensure that proper air content is achieved in the hardened concrete and also reduces excessive bleeding.

Example: For slip form PCC paving utilizing ready mixed concrete, specified air is 7.5% plus 1.5% or minus 1.0% for the first day of paving. For an aggregate correction factor of 1.0%, the target would be 8.5% (8.5% equals the specified target of 7.5% plus the

aggregate correction factor of 1.0%) plus 1.5% or minus 1.0%.

The aggregate correction factor is in addition to any correction added for air content lost through the paver.

9.64 CONCRETE VIBRATION AND CONSOLIDATION

Specification 2301.07.A.6.a requires vibration frequency to be maintained between 4000 and 8000 vibrations per minute for concrete paving finishing machines. To ensure proper consolidation of the plastic concrete, the vibration system used in the finishing machine should provide continuous and full coverage.

The depth of penetration into the concrete of internal vibrators should be set to mid slab height or as deep as possible while passing above any reinforcing steel. An operating position locking device should be provided so that no part of the vibrating unit can be lowered to the extent that it will come in contact with reinforcing steel or tie bars while paving.

Horizontal spacing of vibrators should not exceed the manufacturer's recommendation or 16 inches (410 mm), whichever is less. The Engineer may allow exceptions to this spacing in situations where centerline tie steel placement may be adversely affected or structural elements of the paver make it impractical to maintain exact spacing.

The longitudinal axis of the vibrator body should be mounted approximately parallel to the direction of paving with the exception that the trailing end of each vibrator shall be tilted downward to an approximate slope of 15 degrees below horizontal.

On some large projects, greater than 50,000 square yards (40,000 square meters), an electronic monitoring device, which monitors and records the frequency of each vibrator on the paver, is required. The inspector will periodically check the electronic monitor by use of a manual device. The inspector will periodically check the monitor during the paving day and review, on a spot basis, the daily record of the vibration frequencies. Specification 2301.07, A, 6, a, 2 requires submittal of vibration monitoring data daily for the first three days of paving and weekly thereafter. It is important that these submittals occur because it gives the Engineer the opportunity to review the vibration data to ensure that vibrators are being operated within the allowable frequencies. Upon completion of the project, all vibration monitoring data should be submitted to the Office of Materials.

When a vibrator monitor is not required, vibrator readings should be taken and recorded at the start of concrete placement. Vibrators may be checked in the morning, before paving operation begins. This check can detect malfunctioning or dead vibrators. But, the frequencies will change as the hydraulic oil is heated once paving begins. A check of frequency levels needs to be made after the paver has been operating for some period of time, at least after the first 20 minutes or half hour. Readings should also be taken at least twice daily to check for mechanical failures or problems in the vibration system of the paver. Vibrator readings should be recorded on Form 830213 "Project Information/Paver Inspection." A copy of this form is included in *Appendix 9-3*.

If vibrator frequencies are greater than allowed by the specification, the Contractor should be informed to adjust the paving operations so that future measurements are within required specifications. Excessive vibration frequencies have been known to produce lower entrained air and premature concrete pavement deterioration with shorter

pavement life.

It is also helpful to watch for the presence of vibrator trails in the plastic concrete surface behind the transverse texturing operation (but before the curing compound application). These trails show in the surface of the plastic concrete by a deeper groove in the textured surface. This deeper texture follows the path of the vibrator. Many existing portland cement concrete pavements are showing these "vibrator trails."

9.65 PAVEMENT THICKNESS CORES

Materials I.M. 346 describes procedures for coring PCC pavement for evaluating thickness requirements. The procedures are the basis for acceptance and payment of work. It is intended that the Engineer witness the coring and take possession of the core samples as they are drilled to ensure a proper chain of custody for acceptance. The Engineer will witness the coring and measure the cores immediately on the grade. If cores are not measured on the grade, the Engineer must take immediate possession of the core samples as they are drilled to ensure a proper chain of custody for acceptance. At no time should the contractor have possession of the cores prior to measurement by the Engineer.

9.66 PAVEMENT SMOOTHNESS

Pavement smoothness shall be evaluated in accordance with *Specification 2316* and *Materials I.M. 341*. See *Construction Manual 3.60* for additional information.

9.67 QUALITY MANAGEMENT CONCRETE (QM-C)

QM-C is the design, testing, placement, and monitoring of a Portland cement concrete mixture by a contractor in partnership with the owner for the purpose of making a superior product while promoting innovation and understanding.

The lowa DOT requires QM-C on large paving projects greater than 50,000 square yards (42,000 square meters). It is mainly used on rural type paving projects, without a lot of staging and/or handwork. The mix design is based on an optimized gradation, usually requiring three aggregates of coarse, intermediate, and fine (sand) sizes. QM-C mixes are designed for use in slip-form paving operations only. The optimized gradation allows easier slip-form placement without edge slump, especially on pavements with thicker pavement section (i.e. 12 inch thick interstate pavements). The QM-C mix design is typically coarser than Class C mix design and is not intended for handwork placement. The QM-C supplemental specifications require Class C concrete for handwork. However, in some cases the QM-C mix may be workable enough to be acceptable for handwork. With approval from the Project Engineer, a QM-C mix may be used for handwork.

Since three aggregates are typically required to produce the optimized gradation, QM-C mix designs are better suited on large rural paving projects where batches are proportioned in a central plant. Many ready mix producers do not have the capability to handle more than two aggregates, thus, it is usually not feasible to require QM-C on urban small projects that would typically use ready mixed concrete.

The biggest misconception of using the QM-C specification is that the contracting authority does not have to do testing since the contractor performs testing. IM 530 describes the testing required by the contracting agency. The contracting agency's test results must correlate with the contractor's test results, in accordance with IM 216, in order to allow contractor results to be used as acceptance, be used in the acceptance

decision to comply with the requirement of the Materials Sampling and Testing Program. By not performing any correlation verification testing, the owner may jeopardize federal aid on the project.

Since the contractor incurs additional costs for mix design, grade testing, and increased amount of coarse aggregate in QM-C mixes, Class C concrete may be more economical on smaller projects, urban projects, and projects with extensive staging. Class C concrete will perform equally well as the QM-C mix design and is sometimes better suited for certain placements and field situations.

Measurement and Payment

Measurement and payment can be difficult when using QM-C mixes. Payment for full-depth QM-C pavements is made with two items. The first item is a QM-C cubic yard (cubic meter) item. This item is intended to compensate the contractor for the development of the Concrete Design Mixture (CDM) as well as the testing and process control necessary for production of the mix. The second item is a square yard (square meter) item intended to compensate the contractor for the pavement. An incentive payment is applied to the square yard (square meter) item based upon the aggregate gradation achieved in the CDM throughout the project. However, the incentive only applies to the area of pavement placed using the CDM.

Payment for PCC overlays using QM-C is made with three items. The first item is the QM-C cubic yard (cubic meter) item, and measurement and payment are the same as that used for full-depth pavements. The second item is a QM-C Furnish item. This item is intended to compensate the contractor for the cubic yards (cubic meters) of QM-C mix used on the project. Finally, the third item is a QM-C Placement item. This item is intended to compensate the contractor for placement of the QM-C mix.

NOTE: For overlays, the incentive payment for gradation is applied to both the QM-C Furnish item and the QM-C Placement item.

The square meter (yard) items for QM-C are plan quantity and typically would not need to be measured. However, because the Coarseness/Workability incentive payment only applies to the slip formed portion of the square meter (yard) item, the area of all hand pours must be measured and subtracted from the plan quantity to determine the appropriate Coarseness/Workability incentive payment. This is further complicated by the contractor's option to use the QM-C mix for non-QM-C pavements on a project. See *Appendix 9-7* for guidance on payment for PCC pavements under the QM-C specification.

Materials I.M. 530 requires submittal of all QM-C quality control charts and records to the Project Engineer. The Project Engineer should forward copies of these files to the Office of Materials upon completion of the project.

11.50 CONCRETE (STRUCTURAL, CLASS X, AND FLOWABLE MORTAR)

11.51 PCC PLANT PAGE (FORMS 800240E and 800240M)

The project engineer shall report weekly all concrete placed for each project on "PCC Plant Page" (Form 800240). This form will record concrete placements, all results of sieve analysis tests, and all data on test beams made and tested. The week covered by each report shall begin on Sunday morning and end on Saturday evening. A separate Form 800240 is required for each bridge design, including bridge deck surfacing and resurfacing, and each group of culverts. Refer to *Materials I.M. 527* for instructions on preparing this form.

11.52 USE OF READY MIXED STRUCTURAL CONCRETE Prepour Meeting

It is very important to use the prepour meeting to discuss the specifics of placement, establish communication, and resolve potential "sticky" issues prior to placement. Generally it is recommended to discuss:

- Chain-of-command. Who is in charge for contractor? Who needs to be notified if material tests do not comply with specifications? Establish prior to placement how test results are reported (i.e., does the contractor want to be notified verbally, or in writing each time?).
- Material requirements and admixtures needed for the placement (Examples: Single cement source, concrete temperature and methods used to cool the mix, source and amount of any admixtures, specific mixes required for bridge decks, etc.).

Procedures for introducing admixtures during mixing operations need to be discussed and formalized. For example: How and where will the air entraining agent be introduced? There is a growing concern that placement location of admixtures is causing significant variability in mixes. The plant monitor must watch and document how admixtures are introduced during mixing.

- Method and frequency of acceptance testing during placement. Inform the contractor what is expected if non-acceptable material is found during placement. Recommend to the contractor that they arrange to have a representative from the ready mix plant on site to coordinate concrete delivery, adjustments to concrete mix, and provide direct communication with the ready mix plant during concrete placements.
- Scheduling, truck availability, placement method, and required placement rates.
- Establish an acceptable source of preplacement weather forecasting. Agree on weather parameters which will be used for "go" or "no-go" decisions both "prior to" and "during" the placement activity.
- Review & Discuss items under "Concrete Bridge Floors" in Section 11.62.

Inspector's Checklist

A. Specifications regarding plant inspection, equipment approval, and batching operations should be reviewed for familiarity. In addition to proper plant calibration, the inspector should verify that each truck mixer used on the job has a current

certification as required by *Specification 2001.21*, *Paragraph B* and *Materials I.M.* 528. It is good practice to inspect a random sample of ready mix trucks that will be used on the job, verifying that the certification accurately reflects the truck's condition. Truck certification numbers should be recorded in the inspector's diary and will need to be reverified at least every 30 days. Required information to be recorded on ready mixed concrete truck batch tickets shall be according to Construction Manual Section 9.03.

B. Batching and mixing should be limited to the lead truck until slump and air content have been tested for conformance with specifications. Contractors may make preliminary tests at the plant, but project acceptance is based on job site tests. It is intended that the ready mix plant supply concrete to the construction site that conforms to all applicable specifications at the point where the acceptance sample is taken.

Specification 2403.03, Paragraph A states for Structural Concrete: "Concrete shall be placed with a slump between 25 mm and 75 mm (1 and 3 inches) as a target range, allowing a maximum of 100 mm (4 inches) ..."

Specification 2403.03, Paragraph B states for Structural Concrete:
"... unvibrated structural concrete shall be 6.5 percent, as a target value, with a maximum variation of plus 1.5% or minus 1.0%." Note: As stated in I.M. 318, an adjustment to the target air content called an aggregate correction factor may be required for some aggregates obtained from quarries in east central lowa that have highly absorptive aggregates. The aggregate correction factor may be obtained from the District 6 Materials Office. The target air content for structural concrete utilizing these aggregates would be the specified target for the application plus the aggregate correction factor (see example below). Applying the aggregate correction factor when using aggregates from these quarries helps ensure that proper air content is achieved in the hardened concrete and also reduces excessive bleeding.

Example: For structural concrete specified air content is 6.5% plus 1.5% or minus 1.0%. For an aggregate correction factor of 1.0%, the target would be 7.5% (7.5% equals a specified target of 6.5% plus aggregate correction factor of 1.0%) plus 1.5% or minus 1.0%.

If concrete is being delivered which deviates much from these target values, the contractor is responsible for taking corrective action to bring the mix to within target values. Even if the current mix is within specified limits. The intent of the tolerance is to provide latitude during placement for unforeseen changes in materials, mixes, and placement methods. Placing concrete "consistently" near a tolerance limit is not desirable and warrants additional sampling.

What is important, is the contractor's response to test results approaching tolerance limits. Continually having to add water and/or air agent to each load at the site will not be permitted. If such practice is occurring, the inspector shall notify the contractor (or whomever was designated as "the" responsible individual in charge of the concrete at the site). Ultimately, it is the contractor's responsibility to initiate immediate corrective action.

Non-responsiveness on the contractor's part is reason to initiate sampling and testing of each truck or halt placement. The purpose for additional testing is to

ensure that no noncomplying materials are incorporated into the project.

In some cases admixtures, such as water reducers, are required to be added in split doses or sometimes totally at the site.

C. All Structural Concrete

At the start of each day's placement, no concrete is to be placed in the forms or on the deck until the first truck has been sampled, tested, and approved. Incorporation of materials from this truck will not be permitted unless desired slump and air content are within specified limits. Continuous placement shall not begin until after test results indicate the material meets specified requirements.

If the first load is close to a limit value, it is recommended to sample and test the second load unless site experience indicates it is not necessary.

- Initial start up test results (if taken from the truck chute) must account for method of placement. For example, if placement will be through a pump, air values should be on the high side of target to account for loss during pumping. Again, site/project experience should be factored in this decision.
- Routine acceptance testing will be at a minimum frequency of one sample per 25 cubic meters (30 cubic yards). This frequency may be changed for large, continuous placement where placement rates warrant a lesser frequency. Minimum quantity placed between routine acceptance tests is 25 cubic meters (30 cubic yards). This rate of testing may be increased (made more frequent) if the inspector has a concern that target values are not being met.

NOTE: Only the District Materials Engineer has authority to approve *decreasing* (less frequent) testing frequencies from those listed in *Materials I.M. 204*. PLAN AHEAD and obtain approval for those cases where a variance would be reasonable.

For routine acceptance testing, obtain a representative sample at the last practical point before incorporation, but prior to consolidation. The intent here is to obtain a sample that will most accurately represent the values of slump and air content of the concrete placed. There have been some questions regarding what is considered the last practical point before incorporation. This is an area for good judgement relative to the particular placement. As a guideline, if an inspector has access to the point of discharge of the concrete and will be in this location for other inspection being performed it would seem reasonable that a sample could be obtained for testing. The testing of the sample should be able to be conducted in a reasonably close proximity to the point of sampling.

NOTE:

When concrete is placed by means other than directly from the back of the truck, the sample shall be taken, if possible, after the concrete has passed through the conveyance method being used. (This includes placement by bucket, belt, pumps, power buggies, etc.)

Routine acceptance sampling and testing does not require holding a truck until results are available. However, if there are obvious deficiencies, the inspector has the authority to hold that truck until test results are available.

Inspectors should be alert to obvious visual changes in consistency, with routine acceptance air and slump tests being made as noted above. Any load having questionable consistency should be checked for slump.

- If noncomplying test results are found during routine acceptance sampling, no more material (from that truck or others) shall be incorporated until complying test results are obtained. When test results indicate noncomplying material:
 - 1. The rest of that load shall be rejected and not incorporated, unless adjustments can be made to bring it back into compliance (Specification 1106.04). In an attempt to bring noncomplying concrete into compliance, the supplier may make field adjustments (i.e., add air entraining agent, add portland cement, or rotate the drum). Such "field" adjustments shall be an EXCEPTION and not the general rule and the 90 minute time restriction shall not be waived for any situation.
 - For all noncomplying test results the inspector shall immediately notify the contractor or their representative in charge of the concrete. This notification shall also inform the Contractor if noncomplying materials have been incorporated into the structure.
 - 3. If test results indicated noncomplying materials have been incorporated, the inspector shall make a note in the diary indicating the test results, approximate volume incorporated, location the material was placed, and to whom the notification was given. The inspector should also note a noncomplying event on that particular truck's delivery ticket.
 - At the end of each day or each placement event (whichever is sooner) the inspector shall prepare a Noncompliance Notice (Form 830245) for all noncomplying material incorporated and not removed/replaced during that day or placement event. This notice shall be given to the Contractor yet that day (Materials I.M. 204).
 - 4. When noncomplying materials are found, the inspector will a) hold each truck, and b) initiate sampling and testing of each truck until two consecutive loads meet specifications. At this point, sampling and testing may return to normal project acceptance frequency.
- D. Specifications and Materials I.M.s spell out requirements that materials must meet to be acceptable. Further, Materials I.M. 204 identifies a frequency for sampling/testing and whether the test is an acceptance or assurance test.
 - Authority for initially rejecting noncomplying materials and poor quality work performance is given to the inspector in *Specification 1105.07*. This rejection authority is only superseded by the project engineer. There is an old saying to the effect, "We shall not knowingly incorporate noncomplying material into a project." This means exactly what it says and there is ample support in the specifications for this position.
- E. During placements, the inspector should alternate sampling among the various trucks involved in the operation.

F. If there is a specific truck which is identified as causing a problem with consistency, that truck shall be rejected from further use. (Refer to Specification 2001.21, Paragraph B.)

- G. Transit mixers shall be completely emptied of wash water before reloading. If the truck's top fill hopper is washed after loading, no wash water shall be allowed to enter the mixer.
- H. When it is not practical to sample at the last point prior to incorporation, then a method of correlation between point of placement and the actual point of sampling must be developed. While such cases should be the EXCEPTION and NOT THE GENERAL RULE, one approved method is as outlined below:

When concrete reaches a stable consistency and is within target ranges, correlation tests can be run between the last practical sampling location and the place of deposition. If differences are consistent, then correlated tests can be taken at the last practical sampling location.

The following is a guideline if tests are not consistent:

Test a minimum of three loads of concrete sampled from the "last practical sampling location" and at the point of discharge. Average the difference between the test results. This average (correction factor) is used until another correlation is determined. Correlation tests should be determined, as a minimum, at the beginning, middle, and toward the end of a pour. The inspector needs to factor in situations such as size of pour, changing weather conditions, changes in conveyor length, changes in pumping configuration or pipe angles, and changes in batch proportions when determining frequency of correlation tests.

All subsequent "acceptance" tests are taken at the last practical sampling location and are adjusted using the correlation factor.

All correlation tests and correction factors are to be documented in the field books and noted on the "PCC Plant Page" (Forms 800240E and 800240M) or on a sheet attached to the form. Results reported using correction factors shall be identified with an asterisk (*) or written note.

- I. The inspectors will need to satisfy themselves regarding compliance with the specifications for the number of drum revolutions at mixing speed.
- J. If water, air entrainment, or other admixtures are added at the project site, acceptance testing will not be performed until all additions have been made AND 30 revolutions at mixing speed have been completed following the change.

11.53 ADMIXTURES

Admixtures are those ingredients in concrete other than portland cement, water, and aggregates, that are added to the mixture immediately before or during mixing. Admixtures typically encountered on our jobs can be classified by function as follows:

- Air entraining admixtures
- Water reducing admixtures
- Set retarding admixtures
- Set accelerating admixtures
- Corrosion inhibiting admixtures

■ Finely divided and permeability mineral admixtures (Fly Ash, Ground Granulated Blast Furnace Slag & Silica Fume)

Coloring agents (normally not used for lowa DOT work)

The amount of any admixture used in a mix should be as recommended by the manufacturer and verified through laboratory testing or trial mixes. Effectiveness of an admixture depends upon such factors as type, brand, and amount of cement; water content; aggregate shape; gradation and proportions; mixing time; slump; and temperatures of concrete and air.

Air Entraining Admixtures

Air entraining admixtures are used to purposely entrain microscopic air bubbles in concrete. Air entrainment will dramatically improve the durability of concrete exposed to moisture during cycles of freezing and thawing. Entrained air greatly improves concrete's resistance to surface scaling caused by chemical deicers.

Rules-of-Thumb

- As cement content increases, air agent must increase to maintain equal entrained air.
- As cement fineness increases, the amount of air agent must increase to maintain equal entrained air.
- As coarse aggregate size decreases, the air content increases for a given amount of air agent.
- As fine aggregate volume increases, the air content increases for a given amount of air agent.
- As mixing water increases, the air content increases for a given amount of air agent.
- Air entraining admixtures should be introduced into mix at the plant, but additional may be added at the site to adjust mix for correct air content.
- Air entraining admixtures should (usually) be added to the front of the truck at the plant. If corrosion inhibiting admixture is used, air entraining agents should be added to the back of the truck.

Water Reducing Admixtures - Regular

Water reducing admixtures are used to reduce the quantity of mixing water required to produce concrete of a certain slump or reduce the water-cement ratio. Regular water reducers reduce water content by about 5% to 10%.

Adding a water reducing admixture to a mix without reducing water content can produce a mixture with a much higher slump.

Rules-of-Thumb

- Typically, water reducing admixtures do not reduce the rate of slump loss; in most cases, it is increased. Rapid slump loss results in reduced workability and less time to place concrete at the higher slump.
- Typically, water reducing admixtures have no effect on bleed water.
- Certain types of sulfate starved portland cements may cause false-set with certain brands of water reducers. Typically, water reducers contain lignosulfonates and these sulfates are easily attracted by sulfate starved cements. This action may cause early false-set.
- Despite reduction in water content, water reducing admixtures can cause a significant increase in drying shrinkage.

Water Reducing Admixtures - Super Plasticizers

Super plasticizers are simply "high-range water reducers." They are added to concrete with low-to-normal slump and water content to make high slump "flowable" concrete. Flowable concrete is a highly fluid, but workable concrete that can be placed with little or no vibration and can still be free of excessive bleeding or segregation. Flowable concrete has applications:

- 1. In areas of closely spaced and congested reinforcing steel
- 2. In tremied concrete where "self consolidation" is desirable
- 3. In pumped concrete to reduce pump pressure
- 4. To produce low water-cement ratio high strength concrete. High-range "super plasticizers" can reduce water content by about 12% to 30%.

Rules-of-Thumb

- The effect of most super plasticizers in increasing workability or flowable concrete is short lived. Typically, maximum is 30 to 60 minutes followed by a very rapid loss in workability.
- Typically, super plasticizers are added as split treatments (part at the plant, part at the site). Sometimes the addition is totally at the site.
- Setting time may be affected depending on the brand used, dosage rate, and interaction with other admixtures.
- Excessively high slumps of 250 mm (10 inches) or more may cause segregation.
- High-slump, low water/cement super plasticized concrete has less dry-shrinkage than does high-slump high water/cement conventional concrete.
- Effectiveness of super plasticizer is increased with an increased amount of cement, and/or increased fineness of cement.
- Effectiveness of water reducers on concrete is a function of their chemical composition, cement composition and fineness, cement content, concrete temperature, and other admixtures being used.
- Some water reducing admixtures, such as lignosulfonates, may also entrain some air in the mix.

Retarding Admixtures

Retarding admixtures (retarders) are used to delay the initial set of concrete. High temperatures of fresh concrete 30°C (85°F) and up often cause an increased rate of hardening. Since retarders do not decrease the initial temperature of concrete, other methods of counteracting the effect of temperature must be used.

Rules-of-Thumb

 Retarders are sometimes used to delay initial set of concrete when difficult, long placement times, or unusual placement conditions exist.

NOTE: Retarders are not to be used when the anticipated temperature of the mix is below 13°C (55°F); however, placement requirements must be met within the initial set time indicated for the non-retarded concrete.

Retarding admixtures require a concrete temperature of 13°C (55°F) or greater in order to activate and effectively retard the set of concrete. If the proposed placement cannot be accomplished within the initial set time for non-retarded concrete, the concrete mix temperature will have to be increased through the use of heated materials. When heated materials are used, it is recommended that a concrete mix temperature of 18°C (65°F) be targeted for effective activation of

retarding admixtures.

- Retarders offset the set acceleration effect of hot weather.
- Retarders can be added at the site.
- In general, some reduction in strength at early ages (one to two days) accompanies the use of retarders.
- Use of retarders must be closely monitored, because there is probably no single admixture which has caused more field problems.
- If too much retarder has been used in a mix:
 - 1. Time will usually counter the effects.
 - 2. "Be sure" to maintain the cure during the added time.

Accelerating Admixtures

Accelerating admixtures (accelerators) are used to accelerate the setting time and strength development of concrete at an early age. Strength development can also be accelerated by using:

- Type III "high-early" cement
- Lowering water/cement ratio
- Curing at controlled higher temperatures

Calcium Chloride (CaCl₂) is the material most commonly used in accelerating admixtures. Besides accelerating strength gain, calcium chloride also causes an increase in drying shrinkage, potential reinforcement corrosion, discoloration, and potential scaling.

Rules-of-Thumb

- Always add calcium chloride in solution form as part of the mixing water.
- Calcium chloride is not an antifreeze agent. When used in allowable amounts, it will only reduce the freezing point of concrete by a few degrees.

Corrosion Inhibiting Admixtures

Concrete protects embedded steel from corrosion through its highly alkaline nature (12.5 pH). This causes a passive and non-corroding protective oxide film to form on steel. However, carbonation or the presence of chloride ions from deicers, can destroy or penetrate the protective film. Once this happens, an electronic cell (very small battery) is formed and an electro-chemical process of corrosion begins. This process ultimately forms rust. Rust is expansive (up to 4 times original volume). This induces internal stress and eventually causes spalling to occur.

Corrosion inhibiting admixtures chemically inhibit the corrosion reaction. Calcium nitrite, the most commonly used inhibitor, blocks a corrosion reaction by chemically reinforcing the concrete's passive film.

Rules-of-Thumb

- Corrosion inhibitors should be added at the plant.
- Experience indicates corrosion inhibitors should be placed in the front of the truck (first-in) and air entrainment agent should be placed at the back (last-in).
- Corrosion inhibitors are accelerators and will affect set times. It is recommended to consider adding about a one-half dose of retarder to extend working times.
- Air content of mixes using corrosion inhibitors is often difficult to stabilize. Watch the target air closely.
- A certain amount of calcium nitrite can protect up to a certain threshold level of chloride. Therefore, the amount of corrosion inhibitor added to a mix must be

developed for an assumed maximum level of chloride ingress expected.

Finely Divided Mineral Admixtures

These admixtures are powdered or pulverized materials added to concrete to improve or change the properties (plastic or hardened) of concrete. Based on the mineral's chemical or physical properties, they are classified as: (1) Cementitious, (2) Pozzolans, (3) Pozzolanic and Cementitious, and (4) Nominally inert. Typical PCC mix designs use #3 above.

Pozzolanic Materials

A pozzolan is a siliceous or aluminosiliceous material that in itself possesses little or no cementitious value but will, in finely divided form and in the presence of water, chemically react with the calcium hydroxide released by the hydration of portland cement to form compounds possessing cementitious properties. Pozzolans include fly ash and silica fume.

Fly Ash (Class C & F)

Fly ash is a finely divided residue that results from the combustion of pulverized coal in electric power plants.

Silica Fume

Silica fume, also referred to as micro-silica or condensed silica fume, is another material that is used as a pozzolanic admixture. This light to dark gray powdery product is a result of the reduction of high-purity quartz with coal in an electric arc furnace.

Fly ash and silica fume have a spherical shape. Silica fume has an extremely small particle size (about 100 times smaller than the average cement particle). Although silica fume is normally in powder form, because of its small size and increased ease of handling the product is commonly available in liquid form.

Cementitious Materials

Cementitious materials are substances that alone have hydraulic cementing properties (set and harden in the presense of water). Cementitious materials include ground granulated blast furnace slag.

Ground Granulated Blast Furnace Slag (GGBFS)

GGBFS made from iron blast-furnace slag is a non-metallic product consisting essentially of silicates and aluminosilicates of calcium and other bases developed in a molten condition simultaneously with iron in a blast furnace. The molten slag is rapidly chilled in water to form a glassy sandlike material which is ground to a particle size similar to fly ash. Unlike fly ash and silica fume which have a spherical shape, GGBFS is rough and angular-shaped.

Rules-of-Thumb

- Mixes containing fly ash or GGBFS will generally require less water (about 1% to 10%) for a given slump. Silica fume concrete requires more water for a given slump.
- The amount of air-entraining admixture required to obtain a specified air content is normally greater when fly ash or silica fume is used. Ground slags have variable effects on the required dosage rate of air-entraining admixtures. The amount of air-entraining admixture for a certain air content is a function of the fineness, carbon content, and alkali content.

Fly ash and ground slag will generally improve the workability of concretes of equal slump. However, fly ash in low slump concrete will tend to tear and have reduced workability. Silica fume tends to reduce workability, thus high-range water reducers are usually added to maintain workability.

- Concrete using fly ash or silica fume generally shows less segregation and bleeding than plain concrete. Concrete using some ground slags tend to have slightly higher bleeding than plain concretes, but have no adverse effect on segregation.
- Use of fly ash and ground slag will reduce the amount of heat build-up in concrete. Silica fume most likely will not reduce the heat of hydration, because typically high-range water reducers are used and they increase mass temperatures.
- Use of fly ash and ground slag will tend to generally retard the setting time of concrete. Silica fume alone will accelerate the setting time, however, high-range water reducers tend to offset this.
- Use of fly ash and ground slag generally aids the pumpability of concrete.
- With adequate and correct curing, fly ash and ground slag generally reduces the permeability. Silica fume is especially effective in this regard.

11.54 USE OF INSULATED FORMS FOR PROTECTION

Commercial insulation may be used for protecting concrete during cold weather, or when the contract documents require controlling the heat of hydration. This technique is the contractor's option and could be used in lieu of housing and heating. It will then be the contractor's responsibility to furnish insulation of sufficient quality and thickness to maintain concrete at a temperature of not less than 10°C (50°F) for the first 48 hours after placing, if air temperatures will be less than 5°C (40°F). (Refer to *Specification 2403.08, Paragraph H.*)

Concrete must be between 7°C and 27°C (45°F and 80°F) when placed. To ensure a concrete temperature of at least 10°C (50°F) for 48 hours after placement, the concrete for thin sections such as culvert walls, end posts, piling encasements, etc. should be 18°C (65°F) or higher, since the only additional heat source is the heat of hydration. Concrete for massive sections such as stub abutments, heavy piers, and footings should be in the 13° to 18°C (55° to 65°F) range.

Since only dry insulation is effective, any insulation that has a propensity to adsorb water or become saturated must be protected with a waterproof membrane. The insulation system must provide complete coverage and be secured to provide maximum protection during the full curing period.

For typical protection applications, insulated forms must be left undisturbed for 96 hours before being removed. (Refer to *Specification 2403.11*.)

Checking Temperature of Concrete

For checking compliance with minimum temperature requirements during the 48-hour period after placement, thermometer wells should be cast in the concrete during the pour. The following procedure for checking temperature is suggested:

- 1. Drill an 8 mm (5/16 inch) hole through the form at one or more locations where temperature checks will be made.
- 2. Grease the thermometer probe and insert it through the hole about 100 mm (4 inches) into the plastic concrete.
- 3. Remove probe after the concrete is set and cover hole with insulating material.

4. Further checks can be made by inserting the thermometer through the insulation into the well developed in step 2. Leave thermometer in place if desired, but protect from damage or theft.

NOTE: The thermometer stem should be inserted about 75 mm (3 inches) into the concrete because the sensitive portion of stem is about 70 mm (2 3/4 inches) below the groove.

Record temperature daily for 48 hours following the pour. Temperature readings below 10°C (50°F) during the first 48 hours should be reported to the Office of Construction for evaluation of possible damage or price adjustment.

11.55 DECK PLACEMENT AND HEAT OF HYDRATION

Cracking of concrete in bridge deck placements and large concrete elements (ie: bridge footings, columns, pier caps, etc.) can occur unless the placements are properly controlled. The following provides information on measures that are used in the effort to control cracking of concrete in bridge decks and large concrete element placements.

Deck Placement

Sometime ago the Office of Bridges and Structures, Office of Materials, and Office of Construction began evaluating the phenomena of bridge deck cracking. Measures have been implemented to manage bridge deck placement and prevent cracking through the use of Evaporation Rate Controls.

Research continues in the management of quality bridge deck placements and deck cracking control. To provide needed site specific data for this research, Forms E122, E139, M122 and M139 were developed. These reporting forms were initiated during 1991. Since that time, the information provided from the field has been compiled into a database for evaluation. The evaluation of this data is ongoing and includes review of the effectiveness of Evaporation Rate Controls and possible trends which may lead to a better understanding of crack development.

Forms E122, E139, M122 and M139 are included in *Appendix 11-16*. Since they are not available in Office Supplies, please photocopy as needed. Submit completed forms to the Office of Construction.

Deck Concrete Temperature and Curing

Specification 2412 identifies requirements for placing and curing concrete bridge floors. Of importance for this section are:

- Plastic concrete, when placed, shall not exceed 32°C (90°F).
- Concrete floors will not be placed if the theoretical rate of evaporation exceeds 1 kg/m²/hr (0.2 lbs./sq.ft./hr.).

NOTE: A theoretical evaporation chart is included in *Specification 2412.05*. As an alternative, a computer program has been developed for calculation of theoretical rate of evaporation using Excel. This program incorporates the charts from the specifications in a formula table included on report Forms E122 and M122. The program simplifies the determination of the theoretical rate of evaporation and enables the user to perform trial evaluations for possible changes in air temperature, relative humidity, plastic concrete temperature, and wind velocity. A copy of the Excel program for theoretical rate of evaporation is available at www.dot.state.ia.us/construction/structures.htm.

The curing method requires application of white pigmented curing compound immediately after final finishing, followed by "wet" burlap cure for four (4) days. A sprinkling system is required to keep the burlap wet during this time.

- The curing method requires prewetted burlap to be placed within 10 minutes of final finishing and followed by a "wet" burlap cure for four (4) days. A continuous sprinkling system is required to keep the burlap wet during this time.
- Plastic, in addition to wet burlap, may only be used between October 1 and April 1. The plastic provides a moisture proof barrier above the wet burlap and replaces the sprinkling system after 20 hours of the application of water during cold weather.

The placing of concrete will require close monitoring to comply with the specification. The contractor or ready mix plant should determine temperature of previously placed concrete to project a mix temperature prior to a deck pour. Further, they should obtain a weather report to determine predicted air temperature, wind velocity, and relative humidity for the pour day. Based on this information, you will be able to reasonably predict an evaporation rate.

The above information should be discussed by the inspector, contractor, and ready mix plant operator before a deck pour. The pour should not be attempted if concrete temperature is predicted at 29°C (85°F) or higher and predicted air temperature is above 32°C (90°F). Also, the pour should not be attempted if an evaporation rate would exceed 1 kg/m²/hr. (0.2 lbs./sq.ft./hr.).

District Materials Office has sling psychrometers and wind gauges available for usage the day of the pour. A sling psychrometer is used to determine the relative humidity by finding "wet" and "dry" bulb temperatures. (Refer to Charts in *Appendix 11-17*.) With these values, compute temperature difference and locate the "Difference Between Readings..." column. Then locate the row labeled with appropriate dry bulb temperature. The value at the intersection of "Difference" column and "Dry" bulb temperature is the relative humidity.

EXAMPLE: (English units only)

If the dry bulb temperature is 71°F and the wet bulb temperature is 64°F, the difference is 7°F. At the top of the chart, locate the column headed 7. Follow this column down to the dry bulb temperature row of 71°F. The intersection indicates a relative humidity of 68%.

Placement Considerations

A. If there is any doubt about the concrete temperature exceeding 29°C (85°F), the contractor needs to identify measures which will be implemented to keep mix temperatures within specifications. If the contractor is not prepared to maintain a mix temperature below specifications, the pour should be postponed.

There are several ways concrete temperatures may be kept within specifications. They are:

- Scheduling placements during cooler times of the day
- Wetting the aggregate stockpiles
- Covering/shading the aggregate stockpiles
- Maintaining a supply of portland cement on hand to preclude getting hot material from the supplier
- Chilling the mixing water is one of the most effective ways to lower mix temperatures.

Shaved ice can be used, however, the ready mix operator must submit a proposal for this to the project engineer for review by the Office of Construction.

NOTE:

- 1. No payment will be made for methods taken to keep concrete temperatures and evaporation rates within specifications.
- 2. If pour has to be delayed because of temperature, and pouring is the controlling operation, no working days will be charged.
- B. Location of permissible headers should be discussed with the contractor. If during the pour, it appears:
 - The temperature may exceed 32°C (90°F)
 - And/or the theoretical evaporation rate would exceed 1 kg/m²/hr. (0.2 lbs./sq.ft./hr.)

and these deficiencies cannot be corrected by immediate action, the placement shall be halted at the first permissible joint. On slab bridges, any joint location listed on the plans can be used. For girder beam bridges (steel or concrete), placement may be stopped, in an emergency, at locations as follows:

- Case A. (Continuous or noncontinuous beams, positive section)

 If the positive section has not been completed:

 Complete the positive section and stop at the header location shown on the plans.
- Case B. (Noncontinuous beams, negative section)

 If placement has not proceeded beyond the pier:

 Do not place concrete in the pier diaphragm, and stop just short of the beam end.
- Case C. (Noncontinuous beams, negative section)

 If placement has progressed beyond centerline of the pier:

 Placement must continue through that negative section and stop at the header shown on the plans.
- Case D. (Continuous beams, negative section)

 If problem occurs after starting the negative section:

 Placement must continue through the negative section, and stop at the header shown on the plans.

See Appendix 11-24 for case illustration.

In every case listed above, contact the Office of Construction for curing times and beam break strengths before allowing the contractor to resume deck placement.

Field Documentation

The temperature of concrete should be taken as soon as concrete is placed. It should be taken when the first load is placed and at intervals shown on Forms E122 and M122, Appendix 11-16. Additional checking is warranted if temperature is running at or near maximum. Air temperature should also be taken about the same time as the concrete temperature.

Heat of Hydration

Occasionally, projects will require placement of large volumes of concrete for individual concrete elements (ie: bridge footings, columns, pier caps, etc.). Controlling the temperature of this large volume is important to reduce cracks and potential premature deterioration from thermal cracking that can result from a large temperature difference between the center of the concrete element and its surface. In these cases the contract documents may require monitoring the "heat of hydration." There will also be requirements for the differences between specified monitoring locations. For example: "The temperature difference between the edge of the concrete and the center shall not exceed 10°C (35°F)."

The cooling of large volumes of concrete can take considerable time, and during that time monitoring is required. A form to record these temperatures has been developed. (Refer to "Heat of Hydration" form in *Appendix 11-18*.) Since this form is not included in Office Supplies, please photocopy as needed. Submit completed forms to the Office of Construction.

11.56 PLACEMENT METHODS (PUMPING, BELTING, AND CRANE BUCKET)

Much concern has been expressed about the method of concrete placement because of lost entrained air. Rough handling of plastic concrete during placement has, at times, reduced entrained air to less than 2% not to mention potential segregation problems. While testing at the point of placement "should" identify such problems, varying placement conditions during the pour can affect concrete conditions significantly.

General conditions which must be avoided, or at least severely minimized, are as follows. If one of the following cannot be avoided, at least be aware of the condition, and be sure to conduct additional testing should any of the conditions present themselves.

Crane and Bucket

In the past it was felt the crane and bucket placement method did not adversely affect concrete. This is now in question when viewed from loss of air and potential segregation. Therefore, this method will now also require testing at the placement location, if practical.

Points-to-Watch For

- Free fall of unrestrained concrete shall not exceed 2 m (6 feet) for vertical placement and 1 m (3 feet) for floors and slabs. (Refer to *Specification 2403.08, Paragraph C.*) If the distance is exceeded: (1) reduce the pour depth, (2) remove a section of form work for intermediate placement, (3) or use a tremie.
- Discharge from the bucket must be controllable.
- Cross section of the drop-chute should permit inserting into the form work without interfering with reinforcing steel.

Belt Placement

Belt equipment is typically used to convey concrete to a (1) lower, (2) horizontal, or (3) somewhat higher level.

Points-to-Watch For

- Keep the number and distance of drops between belts to an absolute minimum. Drops tend to encourage segregation and reduce entrained air.
- As belt conveyors are removed from the line (i.e., as on deck pours), recheck the "as placed" air content.

 Be sure all mortar is being removed at the discharge. (No mortar should be on the return belt.)

Check discharge for potential segregation problems.

 In adverse weather (hot and/or windy conditions), long belt runs need to be covered.

Pump Placement

The modern mobile pump with hydraulic placing boom is economical to use in placing both large and small quantities of concrete. These units are used to convey concrete directly from a truck unloading point to the concrete placement area.

Points-to-Watch For

- Typically, pumps are initially flushed with a thin water/cement paste mixture to coat the lines. This slurry must be wasted and the lines charged with the project mix before beginning. Observe, and be sure initial pump charge is thoroughly removed from the pipelines.
- Always pump at a constant rate and keep pipelines full of concrete. High air loss can occur when concrete is allowed to free-fall inside pump lines.
- Avoid, if at all possible, having steep angles in the pump pipelines. Steep angles and slow placement rates are probably the worst conditions for minimizing air loss and segregation. If this condition occurs:
 - 1. Attempt to relocate the pumper, thereby minimizing lift angle.
 - 2. If discharge is not maintaining a constant flow with partial concrete head in the pipe, request pump operator to place a reducer and short section of hose at the discharge end. The purpose is to avoid free falling concrete from impacting the epoxy coated reinforcing steel, deck or forms at high velocity. High velocity impact of concrete aggregate on epoxy coated bars can potentially damage the epoxy coating.
 - 3. If above condition is unavoidable, watch and test the discharge frequently for loss in air and potential segregation.

Rules-of-Thumb for Pumping

- Pump concrete with pipelines as flat as possible (or at least with minimal down angle)
- Minimize (or eliminate) free falling concrete in the pipelines. To do this, maintain some amount of concrete head in the pipelines
- Pump concrete through as few elbows and restrictions as possible
- Pump concrete at "some" constant rate
- Watch for, and test frequently, when situations are not optimized

11.57 FORM REMOVAL

Setting Beams

The following should be used as a guide in conjunction with Specification 2403.19:

A. On diaphragm piers, beams may be set as soon as doing so will not mar or chip the concrete. It is recommended that 24 hours be considered a minimum cure time. (In cooler weather, ambient temperatures below 5°C (40°F), the minimum time indicated should be increased to 48 hours.)

B. No beams may be set on pedestal (T or P10A) piers until the cap concrete is 7 days old and modulus of rupture is at least 3,800 kPa (550 psi) or more. The contractor has the option under *Specifiation 2403.03* to substitute Class M concrete mix for Class C except in bridge floors. When Class M concrete mix is used, beams may be set when the cap concrete is 3 days old and the modulus of rupture is at least 3,800 kPa (550 psi) or more. (Refer to *Specification 2403.19*.) If no test beams are made, the time must be extended to 14 days. (Refer to *Specification 2403.18*.)

There have been special situations where the contractor has been allowed to set beams on piers that have not attained the above strengths. In these cases, the bottom forms have remained in place for an extended period of time. Before approving any variance, contact the Office of Construction for approval.

C. On stub abutments or integral abutments, steel beams and girders may be set as under A above. Concrete beams on stub abutments or integral abutments, same as A above. (Stub abutments are abutments with battered piling, sliding bearings, and the abutment does not move. Integral abutments have vertical piling in prebored holes, beams are rigidly connected to the abutment, and the abutment moves.) On full abutments (solid and continuous from spread footing), same as A above.

11.58 CLASS 3 CONCRETE SURFACE FINISH (RAIL AND BEAMS) Approval of Materials

Materials I.M. 491.10 lists the approved materials and proportions for use in obtaining a Class 3 finish required by Specification 2403.21. Any one of the listed materials may be used. However, for uniformity, only one type should be used on any one structure.

Approvals of this material will be on the basis of legible brand markings on the containers. Periodic sampling and testing will be the responsibility of the Office of Materials. The type used on any structure should be included in the project documentation.

Application of Finish

Surfaces to be given a Class 3 finish must first be given a Class 2 strip down finish immediately after removal of forms. Successful application and adhesion of any type of finish to concrete surfaces is dependent on concrete condition and concrete surface preparation. Factors such as pH of the concrete, concrete moisture content, cleanliness of the concrete surface, and concrete surface profile are all critical to ensuring any coating being applied will securely adhere. For additional information and guidance contact the Office of Construction.

Materials for a special surface finish should be mixed to a uniform condition, preferably with a power mixer. When using a power mixer, add dry ingredients to the liquid. One worker should place the material with a steel trowel, making sure it is pressed firmly into all voids and leveled. When the surface is set so it will not roll or lift, a second worker should smooth the surface uniformly with a rubber float.

Concrete Railings

Surfaces of concrete for barrier rails placed against fixed forms, either on site or in precasting, shall be given a surface finish described for exterior beams in *Specification 2407.14* before application of curing. This should be done as the forms are removed. The contractor may opt to broom (brush) finish the slipform barrier rail.

11.59 FLOWABLE MORTAR

Flowable mortar is being used for four separate purposes according to the current specification:

Backfilling culverts with flowable mortar is specified for the purpose of preventing settlement in the excavation area. Flowable mortar backfill of open trench culverts is typically used when the excavation is in an existing roadway embankment and the excavation area is too small to facilitate normal soil backfill and compaction methods. In this case, flowable mortar fluidity, as discussed in the specifications, is considered non-critical.

- Backfilling culverts constructed under bridges with flowable mortar is specified when existing bridge structures are being converted into roadway embankment sections. This involves constructing a drainage structure under the bridge and converting the existing bridge superstructure into a fully supported roadway section. Flowable mortar backfill is used under the bridge superstructure to fill the embankment area under the bridge up to the bottom of the existing bridge deck. The flowable mortar method is specified since normal soil backfill and compaction methods are not practical and would not achieve the required embankment support for the converted bridge deck. In this case, flowable mortar fluidity is considered non-critical in the area placed below the bridge beams, but would be considered critical between the beams. Flowable mortar for this case is typically specified to be placed in two or more stages.
- Filling void between culvert and culvert liner with flowable mortar is specified to provide support between the culvert liner and existing culvert to prevent future culvert collapse. Flowable mortar is used since normal soil backfilling and compaction methods are not possible. In this case, flowable mortar fluidity is critical and flow distance is limited which may require incremental placement points.
- Plugging culverts with flowable mortar is specified when it is either not possible or practical to remove existing culverts, therefore these culverts are being abandoned in place. In this case, flowable mortar fluidity is critical and flow distance is limited which may require incremental placement points.

Depending on the application, samples of sand, cement, and fly ash may need to be submitted to the Office of Materials for a mix design. (Refer to *Specification 2506.02* for information as to when material will meet the required flow time as measured with a flow cone.) Free water in the sand pile must be considered as mix water because a mix design uses oven dried sand.

Refer to Appendix of Materials I.M. 491.17 for approved fly ash sources and classes.

The success of all flowable mortar projects depends on establishing uniform under-drainage.

Where flowable mortar is to be placed against joints, the joints should be: (1) wrapped with a fabric as per *Specification 4196.01*, *Paragraph B*, or (2) sealed with a gasket, or (3) sealed with roofing cement.

If the contractor uses crushed limestone for granular backfill, it shall meet the requirements for Granular Backfill. (Refer to *Specification 4133.01*.)

Remember flowable mortar is a liquid which has a density of about 2,136 kg/m³ (3,600 lbs./cu yd.) until the water has dissipated. Bulkheads should be strong enough to withstand those pressures.

Under normal conditions, flowable mortar should be set-up sufficiently within 24 to 48 hours for placement of the final lift of either earthfill or special backfill. If "set-up" does not occur or if it seems slow, typically the problem relates directly to drainage of the granular backfill. Often contamination or "dirty" granular backfill is the culprit. Check to be sure it is draining. If not, additional time will help. If time is critical, you may have to physically cut trenches (drainage paths) into the flowable mortar.

Backfilling Culverts - Typical Grading

For backfilling culverts, flowable mortar is used above the granular backfill elevation identified on the plans. There should be a 100 mm (4 inch) subdrain typically located at the culverts flow line elevation. This subdrain is placed to facilitate draining water from the flowable mortar. Therefore, for culverts with buried flow lines, the subdrain will need to be placed in the granular backfill at the lowest elevation possible and yet allow drainage.

Flowable mortar will nominally be placed 0.6 m (2 feet) thick over the entire culvert excavation. Plans, or typicals, define the area used to calculate plan quantities for flowable mortar and granular backfill. (Flowable mortar plan quantities should include 30% additional for anticipated consolidation of the granular backfill and shrink due to loss of water.) If the Contractor opts to excavate a larger area than assumed for plan quantity, additional excavation, backfill, and flowable mortar will not be considered for pay. We will however, require additional excavation to be backfilled in a manner as identified by the plans or typicals.

Placement of flowable mortar shall always be computed from "top down." This means allow for:

- 1. Pavement thickness
- 2. 0.3 m (1 foot) of special backfill, if required
- 3. Variable thickness of earth fill where cover heights are over 2.5 m (8 feet)
- 4. Placement of 0.6 m (2 feet) of flowable mortar

There are two general installation situations.

Situation 1:

Distance between the top of culvert and bottom of pavement is greater than 0.9 m (3 feet), but less than or equal to 2.5 m (8 feet). In this situation, the top of granular backfill will *vary* from 0.6 m (2 feet) below top of culvert to 1.5 m (5 feet) above the culvert top.

Example:

Assume:

- 1. Bottom of slab is elevation 30 m (100 feet) and top of culvert is 28.65 m (94 feet).
- 2. There is 0.3 m (1 foot) of Special Backfill. Elevation 29.7 m (99 feet)
- 3. 0.6 m (2 feet) of flowable mortar is required. Elevation 29.1 m (97 feet)

In this example, cover is less than 2.5 m (8 feet), granular backfill is placed from bottom of excavation up to elevation 29.1 m (97 feet).

Note: There will be consolidation in both the granular backfill and flowable mortar. It is recommended to place:

- Granular backfill to the required calculated elevation
- Flowable mortar to its calculated elevation
- Make up any final elevation difference due to total consolidation by additional thickness of special backfill

Situation 2:

Distance between "top of culvert and bottom of pavement" is greater than 2.5 m (8 feet). In this situation: A) the top of granular backfill will be fixed at the elevation of culvert top, B) 0.6 m (2 feet) of flowable mortar will be placed directly on top of the granular backfill, and C) compacted earthfill will be placed between flowable mortar and special backfill. In this example, the earthfill will have a minimum thickness of 1.5 m (5 feet) and no theoretical maximum thickness.

Example (Using English units only)

Assume:

- 1. Bottom of slab is Elevation 100.
- 2. There is 1 foot of Special Backfill (Elevation 99).
- 3. Earthfill is required, but thickness cannot be calculated yet. (Elevation ???)

At this point you must now calculate from the culvert top, up to the bottom of the earthfill.

- 4. Top of culvert, for this example, is assumed to be Elevation 86.
- 5. Granular backfill is fixed at the culvert top (Elevation 86).
- 6. 2 feet of flowable mortar is required. (Elevation is 86 + 2 = 88.)

In this situation, earthfill is placed from the top of flowable mortar (Elevation 88) to bottom of special backfill (Elevation 99). Specifically, 11 feet of earthfill is required. (Elevation 99 - 88 = 11 feet)

Plugging Culverts

For culverts 20 m (60 feet) or less in length, flowable mortar may be placed into the outlet first, then the inlet. For culverts more than 20 m (60 feet) long, the desirable spacing for placing flowable mortar should be 20 m (60 feet). The optimum travel of flowable mortar is 10 m (30 feet) with approximately 75 mm (3 inches) of fall in the surface. To avoid drilling through pavement, the spacing can be increased to 25 m (80 feet) if necessary.

Backfilling Culverts - Under Bridges

Prior to installing flowable mortar, the culvert must be backfilled with granular backfill to at least 75 mm (3 inches) over the culvert or 1.5 m (5 feet) below the lowest bridge elevation. As this granular backfill is placed, the outside fill should be brought up at the same time with soil.

Flowable mortar used for backfilling culverts under bridges is placed in two stages.

In the first stage, flowable mortar is placed to an elevation about 150 mm (6 inches) below the bottom of bridge deck or the beams whichever is lower. Bridge beams should be fitted with Styrofoam filler to full width of the flanges. Refer to illustration in *Appendix* 11-25. This will prevent adding dead load to the beams with flowable mortar.

In the second stage, flowable mortar is placed through holes drilled in the deck at spacings identified in the plans or specifications. Typically, begin at one abutment and continue longitudinally down the bridge until the other abutment has been reached, filling all holes on one side of the centerline. Then begin on the other side of the bridge and work holes nearest the centerline and proceed to the outside.

After flowable mortar has been placed, the contractor is required to saw a minimum of 75 mm (3 inches) deep cut into the original deck before any sidewalk, curb, or handrail is removed. It is important that this 75 mm (3 inch) saw cut be done prior to any curb removal, thereby preventing damage to the deck.

Placing flowable mortar under a bridge can be accomplished during staged construction. The specification requires a 72-hour delay between stage 1 and stage 2 placement of flowable mortar to allow for settlement of the granular backfill.

Filling Voids Between Culverts

If there is room to place granular backfill between culverts, do so to one-half the new culvert height. In situations such as multiple barrels, or a new pipe inside a box, the granular backfill will adequately maintain pipe location during flowable mortar placement.

If granular backfill cannot be used, culvert(s) should be blocked at 3 m (10 foot) intervals or less and flowable mortar placed as usual. If a pipe inside a culvert has to be blocked in place, the blocking must be situated in a manner to prevent damming and causing voids in the mortar. All blocking placed on the top of the inside culvert must be saddle shaped to fit the culvert. This distributes the buoyant forces over a larger area and reduces chance of pipe buckling. To further reduce buoyant forces:

- Place about one-half of the total flowable mortar
- Delay about four hours before placing the remainder

In all cases, a drainage system must be established on each side of the culvert(s). The drainage system should be a 100 mm (4 inch) slotted drain with a minimum of 150 mm (6 inches) of granular backfill cover. The drainage system reduces buoyancy effects and allows for dewatering of the flowable mortar.

Inspect all pipe joints and lifting holes for looseness and voids. Two approved repair methods are:

- Wrap joints with fabric approved per Specification 4196.01, Paragraph B
- Seal joints with sealant material such as roofing cement or gaskets

ESTIMATING PROPOSAL -- FOR FEDERAL AID CONTRACT PAGE: 1
To be valid for bidding, the Proposal Schedule of Prices form included with this Estimating Proposal or an 'Expedite' generated Schedule of Prices form must be included with a "BIDDING DOCUMENT" issued by the Iowa D.O.T. Office of Contracts.

Bid Order No.: 108

Letting Date: May 15, 2001

9:00 A.M.

Type of Work: PCC PAVEMENT - REPLACE

Primary County: WOODBURY Design: ENGLISH

DBE Goal: 5.0 % 1997 Std Spec

Pre-Qual Group: PCC PAVEMENT - RURAL

* Proposal ID No.: 97-7057-013

* Contracting Authority: CITY OF SIDUX CITY

Proposal Guaranty: \$ 100,000.00

* Tied Proposal Package: None assigned to, or allowed with this Bid Order.

This Proposal Includes The Following Project(s):

Project: STP-U-7057(13)--70-97 County: WOODBURY
Work Type: PCC PAVEMENT - REPLACE Plans: Yes
Route: WESLEY WAY Design: ENGLISH

Location: FROM JUST SOUTH OF I-29/U.S. 77 NORTH TO JUST NORTH OF

SIXTH STREET IN THE CITY OF SIOUX CITY.

Road System: URBAN

Federal Aid - Predetermined Wages Are In Effect

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PROPOSAL SCHEDULE OF PRICES

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Vendor No.: | __._. _ _ | Proposal ID No.: 97-7057-013

Bid Order No.: 108

Letting Date: May 15, 2001

Primary Work Type: PCC PAVEMENT - REPLACE Primary County:

WOODBURY

9:00 A.M.

UNIT	BIDS	MUST	BE	TYPED	OR	SHOWN	IN	INK	OR	THE	BID	WILL	BE	REJECTED.
------	------	------	----	-------	----	-------	----	-----	----	-----	-----	------	----	-----------

Linn	Thom Number	Item	Unit Price	Bid Amount	
No	Item Number Item Description	Quantity and Unit	Dollars Cts	Dollars Cts	
Section	on 0001 RDADWAY ITEMS				
0010	2101-0850002 CLEARING AND GRUBBING	20.000 UNIT			
0020	2102-0425046 SELECTED BACKFILL	100.000 CY			
	2102-2710070 EXCAVATION, CLASS 10, ROADWAY AND BORROW	4,408.000 CY			
0040	2102-2710080 EXCAVATION, CLASS 10, UNSUITABLE OR UNSTABLE MATERIAL	100.000 CY			
	2105-8425005 TOPSOIL, FURNISH AND SPREAD	1,400.000 CY			
0060	2109-8225100 SPECIAL COMPACTION OF SUBGRADE	28.090 STA			
0070	2111-8174100 GRANULAR SUBBASE	19,630.000 SY			
0080	2113-0001100 SUBGRADE STABILIZATION MATERIAL, POLYMER GRID	6,120.000 SY			
0090	2122-5190008 PAVED SHOULDER, P.C. CONCRETE, 8 IN.	258.000 SY			
0100	2123-7450020 SHOULDER FINISHING, EARTH	32.250 STA			

Vendor No.: | __._. __ | Proposal ID No.: 97-7057-013

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Primary Work Type: PCC PAVEMENT - REPLACE

9:00 A.M.

Primary County: WOODBURY

1 /		Item	Unit Price	Bid Amount
Line No		Quantity and Unit	Dollars Cts	Dollars Cts
0110	2301-1033080 STANDARD OR SLIP FORM PORTLAND CEMENT CONCRETE PAVEMENT, CLASS C, CLASS 3 DURABILITY, 8 IN.	11,500.000 SY		
0120	2301-1033100 STANDARD OR SLIP FORM PORTLAND CEMENT CONCRETE PAVEMENT, CLASS C, CLASS 3 DURABILITY, 10 IN.	6,120.000 SY		
0130	2301-4875006 MEDIAN, P.C. CONCRETE, 6 IN.	118.000 SY		
	2301-6911722 PORTLAND CEMENT CONCRETE PAVEMENT SAMPLES	LUMP	LUMP	
	2303-9093000 DRIVEWAY, ASPHALT CEMENT CONCRETE	447.000 SY		
	2315-8275030 SURFACING, DRIVEWAY, CLASS C GRAVEL	10.000 TON		
100	2401-6745760 REMOVAL OF INTAKE	8.000 EACH		
0180	2401-6745830 REMOVAL OF P.C. CONCRETE MEDIAN BARRIER	50.000 LF		
	2401-6745980 REMOVAL OF UTILITY ACCESS	3.000 EACH		
0200	2502-8212034 SUBDRAIN, LONGITUDINAL, (SHOULDER) 4 IN. DIA.	4,157.000 LF		

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PCC PAVEMENT - REPLACE

9:00 A.M.

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1 / 00	Item Number	Item	Unit Price	Bid Amount
Line No		Quantity and Unit	Dollars Cts	Dollars Cts
	2502-8220193 SUBDRAIN DUTLET (RF-19C)	16.000 EACH		
	2503-4360110 INTAKE, MODIFICATION	2.000 EACH	September 1	
	2503-4388014 INTAKE, SPECIAL, AS PER PLAN	7.000 EACH		
	2503-4470480 INTAKE, RA-48	1.000 EACH		
	2503-4470635 INTAKE, RA-63 MODIFIED	3.000 EACH		
	2503-4470685 INTAKE, RA-68 MODIFIED	7.000 EACH		
	2503-4480495 UTILITY ACCESS, RA-49 MODIFIED	1.000 EACH		
0280	2503-4480499 UTILITY ACCESS, RA-49 MODIFIED, TOP ONLY	1.000 EACH		
	2503-7325015 SEWER PIPE, 2000D STORM, 15 IN. DIA.	414.000 LF		
0300	2503-7325018 SEWER PIPE, 2000D STORM, 18 IN. DIA.	337.000 LF		
0310	2503-8462100 UTILITY ACCESS, CONVERT INTAKE TO	1.000 EACH		

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Primary County: WOODBURY

Line	Item Number	I tem Quantity	Unit Price	Bid Amount
No	A CONTRACTOR OF THE PROPERTY O	and Unit	Dollars Cts	Dollars Cts
0320	2504-8462510 SANITARY SEWER UTILITY ACCESS (PRECAST) (RA-51) , MODIFIED	3.000 EACH		
0330	2505-4021331 GUARDRAIL, END ANCHORAGE, BEAM, RE-33A	2.000 EACH		
0340	2505-6300100 POSTS, REMOVE AND REINSTALL	58.000 EACH		
0350	2505-6765007 REMOVAL AND RE-ERECTION OF EXISTING RAIL, AS PER PLAN	LUMP	LUMP	
0360	2510-6745850 REMOVAL OF PAVEMENT	20,260.000 SY		
	2511-6745900 REMOVAL OF SIDEWALK	531.000 SY		
	2511-7526004 SIDEWALK, P.C. CONCRETE, 4 IN.	632.000 SY		
	2512-1725256 CURB AND GUTTER, P.C. CONCRETE, 2.5 FT.	166.000 LF		
0400	2512-1750006 CURB AND GUTTER, P.C. CONCRETE, AS PER PLAN	59.000 LF		
	2513-0471046 CONCRETE BARRIER, APPROACH, RE-46	1.000 EACH		

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Line	Item Number	Item	Unit Price	Bid Amount
Line No		Quantity and Unit	Dollars Cts	Dollars Cts
	2513-0473443 CONCRETE BARRIER, RE-44C	50.000 LF		
	2513-0474990 CONCRETE BARRIER, REINFORCED, AS PER PLAN	1,323.000 LF		
	2515-2475008 DRIVEWAY, P.C. CONCRETE, 8 IN.	929.000 SY		
	2515-6745600 REMOVAL OF PAVED DRIVEWAY	208.000 SY		
	2518-6890032 ROAD CLOSURE (URBAN), PERMANENT, RE-3B	2.000 EACH		
	2518-6910000 SAFETY CLOSURE	7.000 EACH		
	2520-3350010 FIELD LABORATORY	1.000 EACH		
	2523-0000200 ELECTRICAL CIRCUITS	2,130.000 LF		
	2523-0000310 HANDHOLES AND JUNCTION BOXES	18.000 EACH		
0510	2523-0000400 CONTROL CABINET	1.000 EACH		Mark Control
0520	2525-2638030 SILT FENCE	500.000 LF		

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Primary Work Type: PCC PAVEMENT - REPLACE

9:00 A.M.

Primary County: WOODBURY

		Item	Unit Price	Bid Amount
Line No	Item Number Item Description	Quantity and Unit	Dollars Cts	Dollars Cts
0530	2527-9263110 PAINTED PAVEMENT MARKING	108.520 STA		
	2527-926314O PAINTED SYMBOLS AND LEGEND	28.000 EACH		
	2527-926318O PAVEMENT MARKING REMOVED	17.600 STA		
0560	2528-7575000 TRAFFIC CONTROL SIGNALS, FURNISH AND INSTALL	LUMP	LUMP	
	2528-8445110 TRAFFIC CONTROL	LUMP	LUMP	
0580	2528-8445112 FLAGGERS	10.00 DAY	205.00000	2,050.00
	2533-4980005 MOBILIZATION	LUMP	LUMP	
	2598-3778012 GATE VALVE AND VALVE BOX, 12 IN.	1.000 EACH		
	2598-8805612 WATER MAIN, DUCTILE IRON, 12 IN.	240.000 LF		
0620	2598-8810200 WATER MAIN FITTINGS	234.000 LB		
0630	2599-0410116 ATTENUATOR, IMPACT, REMOVE AND REINSTALL	1.000 EACH		

PROPOSAL	SCHEDULE	OF	PRICES

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Primary Work Type: PCC PAVEMENT - REPLACE
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Line	Item Number	Item Quantity	Unit Price	Bid Amount	
No		and Unit	Dollars Cts	Dollars Cts	
0640	2599-9999005 ('EACH' ITEM) LIGHTING POLE, BOLLARD	46:000 EACH			
0650	2599-9999005 ('EACH' ITEM) LIGHTING POLE, PEDESTAL	18.000 EACH			
	2599-9999005 ('EACH' ITEM) PROJECT SIGN	2.000 EACH			
0670	2599-9999005 ('EACH' ITEM) REPLACE UTILITY ACCESS RING AND COVER	21.000 EACH			
0680	2601-2634100 MULCHING	1.000 ACRE			
0690	2601-2636044 SEEDING AND FERTILIZING (URBAN)	1.000 ACRE			
	SECTION OOO1 TOTAL				
	TOTAL BID				

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Letting Date: May 15, 2001

9:00 A.M.

Primary Work Type: PCC PAVEMENT - REPLACE

Primary County: WOODBURY

Note Description

Note Description

DBE--2001 January 26, 2001

STATE OF IOWA 2001 DIRECTORY OF CERTIFIED DISADVANTAGED BUSINESS ENTERPRISES

DBE-010515 May 15, 2001

AMENDMENT TO THE STATE OF IOWA 2001 DIRECTORY OF CERTIFIED DISADVANTAGED BUSINESS ENTERPRISES

(THIS LISTING IS ATTACHED TO THE BIDDING DOCUMENT.)

FHWA-1273.02 March 10, 1994

REQUIRED CONTRACT PROVISIONS - FEDERAL-AID CONSTRUCTION CONTRACTS (EXCLUSIVE OF APPALACHIAN CONTRACTS)

GS-97009 April 03, 2001

GENERAL SUPPLEMENTAL SPECIFICATIONS FOR CONSTRUCTION PROJECTS

IA01-1.1 March 16, 2001

PREDETERMINED WAGE RATE - GENERAL DECISION NUMBER IAOOOOO1
FOR HEAVY AND HIGHWAY CONSTRUCTION -- STATEWIDE (EXCEPT SCOTT COUNTY)

NOTE: THE CONTRACTOR SHALL REVIEW THE CONTRACT DOCUMENTS AND IS RESPONSIBLE FOR IDENTIFYING WHICH ZONE(S), AS DEFINED IN THE PREDETERMINED WAGE RATE SPECIFICATION, APPLY TO THE WORK ON THE CONTRACT.

*** ADDITIONAL REQUIREMENT ***

THE PRIME CONTRACTOR SHALL SUBMIT CERTIFIED PAYROLLS FOR ITSELF AND EACH APPROVED SUBCONTRACTOR WEEKLY TO THE PROJECT ENGINEER. THE CONTRACTOR MAY USE THE IOWA D.O.T. CERTIFIED PAYROLL FORM OR OTHER APPROVED FORM. THE CONTRACTOR SHALL LIST THE CRAFT FOR EACH EMPLOYEE COVERED BY THE PREDETERMINED WAGE RATES. THE PRIME CONTRACTOR SHALL SIGN EACH OF THE SUBCONTRACTOR'S PAYROLLS TO ACKNOWLEDGE THE SUBMITTAL OF THE CERTIFIED PAYROLL.

SP-97569 May 15, 2001 SPECIAL PROVISONS FOR WATER MAIN

*** INTENDED FOR: WOODBURY COUNTY STP-U-7057(13)--70-97 ***

SP-97570 May 15, 2001

SPECIAL PROVISONS FOR TRAFFIC SIGNALIZATION

*** INTENDED FOR: WOODBURY COUNTY STP-U-7057(13)--70-97 ***

SS-97027 July 15, 1997

SUPPLEMENTAL SPECIFICATIONS FOR METRICATION

SS-97029 January 13, 1998

SUPPLEMENTAL SPECIFICATIONS FOR STRUCTURAL STEEL (WELDING)

Page:

Bid Order No.: 108

Proposal ID No.: 97-7057-013

Letting Date: May 15, 2001

Primary Work Type: PCC PAVEMENT - REPLACE

Primary County: WOODBURY

됐다면 어깨워졌다. 스빌 모양.

9:00 A.M.

Note Description

SS-97058 November 14, 2000

SUPPLEMENTAL SPECIFICATIONS FOR EQUAL EMPLOYMENT OPPORTUNITY AND AFFIRMATIVE ACTION REQUIREMENTS

SS-97059 November 14, 2000
SUPPLEMENTAL SPECIFICATIONS FOR SPECIFIC AFFIRMATIVE ACTION
RESPONSIBILITIES (DISADVANTAGED BUSINESS ENTERPRISE) ON FEDERAL AID
PROJECTS

005.02

*** BIDDING PROPOSAL PREPARATION INFORMATION ***

A PROPOSAL MAY CONTAIN MORE THAN ONE PROJECT. SEVERAL FORMS TO BE SUBMITTED WITH THE BIDDING PROPOSAL REQUEST THE BIDDER TO ENTER A "PROJECT NUMBER". THE BIDDER SHOULD ENTER THE "PROPOSAL ID" WHEREVER THE PROJECT NUMBER IS REQUESTED IN THE BIDDING DOCUMENTS.

005.1102

*** ANNUAL BID BOND ALLOWED ***
ADD THE FOLLOWING NEW PARAGRAPH TO THE END OF ARTICLE 1102.12, PROPOSAL

AN 'ANNUAL BID BOND' (FORM 650043) MAY BE USED FOR THE PROPOSAL GUARANTY IN LIEU OF THE OTHER ALTERNATIVES SPECIFIED ABOVE. THE ANNUAL BID BOND WILL BE VALID FOR THE DESIGNATED LIFE OF THE ANNUAL BID BOND FOR USE FOR BIDS SUBMITTED FOR PROPOSALS FOR A LETTING IF RECEIVED AND APPROVED BY THE IOWA DEPARTMENT OF TRANSPORTATION CONTRACTS ENGINEER AT LEAST 5 BUSINESS DAYS PRIOR TO THE LETTING OF FIRST USE. REQUESTS AND INSTRUCTIONS FOR SUBMITTAL OF THE ANNUAL BID BOND ARE TO BE DIRECTED TO IOWA DEPARTMENT OF TRANSPORTATION, OFFICE OF CONTRACTS.

080.01

*** DBE GOAL INFORMATION ***

THE ESTABLISHED DBE GOAL FOR THIS CONTRACT CONCERNING PARTICIPATION BY DISADVANTAGED BUSINESS ENTERPRISES (E.G., SUPPLIERS, AND SUBCONTACTORS) IS SHOWN ON THE FIRST PAGE OF THE 'ESTIMATING PROPOSAL' FORM AND APPLIES TO ALL FEDERAL AID PROJECTS INCLUDED IN THIS PROPOSAL.

REFER TO THE CURRENT "STATE OF IOWA DIRECTORY OF CERTIFIED DISADVANTAGED BUSINESS ENTERPRISES" AND TO THE CURRENT "SUPPLEMENTAL SPECIFICATION FOR SPECIFIC AFFIRMATIVE ACTION RESPONSIBILITES (DISADVANTAGED BUSINESS ENTERPRISES) FEDERAL AID PROJECTS" FOR ADDITIONAL INFORMATION AND INSTRUCTIONS.

IN ADDITION, IF THE WINNING BIDDER ELECTS TO USE DBE SUBCONTRACTORS AND/OR SUPPLIERS, FORM 830231 (SUBCONTRACT REQUEST AND APPROVAL) SHALL BE SUBMITTED TO THE OFFICE OF CONTRACTS WITH THE SIGNED CONTRACT AS PER ARTICLE 1108.01 OF THE STANDARD SPECIFICAITONS.

Page:

Bid Order No.: 108

Letting Date: May 15, 2001 Proposal ID No.: 97-7057-013 9:00 A.M.

Primary Work Type: PCC PAVEMENT - REPLACE

Primary County: WOODBURY

Note Description

500.02

*** WINTER WORK ***

EXCEPT FOR THE EROSION CONTROL WORK REQUIRED FOR THIS PROJECT, THE FREE TIME ALLOWED BETWEEN NOVEMBER 15 AND APRIL 1 WILL NOT BE PERMITTED. THE CONTRACTOR SHALL WORK DURING THE WINTER ON ALL WORKING DAYS AS DEFINED IN 1101.03 'WORKING DAY'.

660.23

*** SPECIALTY ITEM ***

THE ITEM 'SIGNALS, TRAFFIC CONTROL, FURNISH AND INSTALL' IS CONSIDERED A SPECIALTY ITEM FOR THIS PROJECT.

WHEN PERFORMED BY SUBCONTRACT, THE COST OF THIS SPECIALTY ITEM SO PERFORMED BY SUBCONTRACT MAY BE DEDUCTED FROM THE TOTAL COST BEFORE COMPUTING THE AMOUNT OF WORK REQUIRED TO BE PERFORMED BY THE PRIME CONTRACTOR WITH HIS/HER OWN ORGANIZATION. REFER TO ARTICLE 1108.01 OF THE STANDARD SPECIFICATIONS.

670.12

*** SUBLETTING OF CONTRACT ***

REPLACE THE FIRST PARAGRAPH OF STANDARD SPECIFICATIONS ARTICLE 1108.01 WITH THE FOLLOWING:

THE CONTRACTOR SHALL PERFORM AT LEAST 30% OF THE CONTRACT AMOUNT WITH HIS/HER OWN ORGANIZATION. ON THIS PROJECT ONLY, THE CONTRACTOR MAY SUBCONTRACT UP TO 70% OF THE CONTRACT AMOUNT.

THE BIDDERS SHOULD BE AWARE THAT THIS PROJECT REQUIRES SEVERAL TYPES OF WORK. PURCHASING OF MATERIALS FOR SUBCONTRACTORS WILL NOT BE AN ACCEPTABLE METHOD FOR THE PRIME CONTRACTOR TO MEET THE 30% REQUIREMENT.

ITEMS DESIGNATED AS SPECIALTY ITEMS MAY BE PERFORMED BY SUBCONTRACT. AND THE COST OF ANY SPECIALTY ITEMS SO PERFORMED BY SUBCONTRACT MAY BE DEDUCTED FROM THE TOTAL COST BEFORE COMPUTING THE AMOUNT OF WORK REQUIRED TO BE PERFORMED BY THE CONTRACTOR WITH HIS/HER OWN ORGANIZATION.

700.00

*** NO TIES BETWEEN PROPOSALS WILL BE ALLOWED ***

ALL SECTIONS AND ALL ITEMS ON THIS PROPOSAL FORM MUST BE BID WITH THE EXCEPTION OF ALTERNATE ITEMS OR ALTERNATE SETS OF ITEMS. NO OTHER TIES BETWEEN PROPOSALS WILL BE ALLOWED.





PCC Level II

Reports

IX. REPORTS

Paving and Structural Report

- Daily or Weekly
- Form 800240E or 800240M

Portland Cement Shipment Yield

- Every 10,000 cubic yards
- Form 820912

Ready Mix Tickets

Form 830212

Calibration Reports

Form 820917

Transit Mixer Condition

Form 820907

PCC PAVING PLANT BOOK

Plant Information Sheet

Portland Cement Concrete Form

- Batch Weights
- Form 820150E or 820150M

PCC Plant Report

Form 800240E or 800240M

Portland Cement Shipment Yield Report

Form 820912 E

Fly ash Shipments

Form E203 and M203

Aggregate Certifications (Coarse and Fine)

Form E204 and M204

PCC Level II Reports

Specific Gravities

Form E205 and M205

Moistures (Pycnometer)

Form E206 and M206

Daily Plant Checklist

Form E212 and M212

Plant Site Inspection List

Form E210 and M210

Beams Made and Tested

Form E114 and M114

REPORTS AND REPORTING

1. PLANT PAGE - FORM #240

Plant Reports are to be recorded in the computer program or on hand completed forms, both provided by the lowa Department of Transportation. A copy of the completed PCC Plant Page shall be faxed or delivered to the District Materials Engineer on the next working day, within four hours after start-up of the plant. The CPI shall keep a copy of the PCC Plant Page and send the original to the Project Engineer. Copies of the files containing the project information are to be available to the engineer upon request until the project is final.

A separate report is to be made for each day concrete is placed. These reports are to be consecutively numbered for each project. A sample copy and the instructions on completing this report are in **Appendix A**.

When computer forms are used, the following equipment is necessary.

2. PERSONAL COMPUTER

The personal computer shall be capable of running Iowa DOT Programs. The printer shall be capable of producing quality hard copies. That is, original printed output, which is clearly readable and remains readable after being faxed and/or copied.

INSTRUCTIONS FOR COMPLETION OF PCC PAVING & STRUCTURAL REPORTS

The new reporting process does not include Mobile Mixer information. Use the following forms and reports when using a Mobile Mixer:

Form M or E 115	Air & Slump Record
Form M or E 120	Mobile Mixer Data Record
Report #820180	Gradation Test
Report #821297	Nuclear Density of Plastic PC Concrete
Report #820020	Mobile Mixer Calibration

Project No.

Enter the project number listed on the plans.

Plant Name

Enter the name of the ready mix plant and location for structural concrete. Enter the approximate location of a paving plant set up by a contractor.

Example: Croell - Waverly (Ready Mix)
2 miles NW of Waverly (Paving Plant)

Contractor/Sub

A group of people or a company must perform the work being done, either a prime or sub contractor. Enter the name of the contractor performing the work. If it is a subcontractor, list this after the contractor name.

Weather

Enter a brief description of the actual weather conditions at the paving plant. Weather conditions are not required for structural concrete (Ready Mix).

Contract ID

Enter the nine-digit contract number listed at the top of a contract. This is <u>not</u> the five-digit accounting ID number listed with the project number.

County

Enter the county listed on the project plans.

Temperatures, Min. & Max.

An air temperature shall be recorded early in the morning for the minimum and around midafternoon for the maximum. Take the temperatures in a shaded area, otherwise they are meaningless. Temperatures are not required for structural concrete (Ready Mix).

Report No.

Start with the number 1 at the beginning of work for each item on each project. The ending report number shall coincide with the last day each item is completed for paving and the last week for structural. Do not restart the report sequence if the project carries over to the next year.

Example: (Paving) 16 days of 200-mm slip form paving - report 1 through 16.

(Ready Mix) 8 weeks of concrete on Des. 1290 - report 1 through 8.

Date This Report

Enter the date the concrete is placed for each day of paving. Enter the last day of the workweek for structures (normally the Saturday date).

Date of Last Report

Self-explanatory.

Design No.

Enter the design number of the structure where the concrete is being placed on each project. Leave this space blank on paving projects.

Check Mix (Central or Ready)

Place an "X" in the appropriate box provided indicating how the concrete is being produced.

Check Usage (Paving, Structural, Incidental, Patching)

Place an "X" in the appropriate box provided to indicate the type of work where the concrete is used.

Date (Mo./Day)

This column is only used for Ready Mix concrete applications. Enter the month and the date for each day of production during the week.

Example: 5/24, 7/01, 12/03, etc.

Mix Number

Enter the mix number being used that is listed in the proportion tables of IM 529.

Station (Beg./End/Dir)

Enter the beginning and ending station for concrete placed daily by mix. Enter the direction (N, S, E, W) for divided sections or B for 2-lane sections.

Batched

Enter the total cu. yds. (m³) batched for each mix for a paving plant. Enter the total cu. yds. (m³) batched for each unit poured for structures.

% Of Est. Used

Enter the percent of estimated concrete used.

Fine, Intermediate & Coarse Aggregate (Moisture)

Enter the percent moisture once in the morning and once in the afternoon for paving projects. Enter the percent moisture for each unit poured on structures.

Fine, Intermediate & Coarse Aggregate (T203 sp gr)

Enter the specific gravity for each aggregate listed in the T203 source tables.

Fine, Intermediate & Coarse Aggregate (Dry Mass or Wt.)

Enter the weight (mass) of each aggregate calculated by absolute volumes.

Actual Quantities Used Per cu. yds. (m3) in Kilograms (Pounds)

Cement	Enter the pounds (kilograms) of cement calculated by absolute volumes.
Fly Ash	Enter the pounds (kilograms) of fly ash calculated by absolute volumes.
GGBFS	Enter the pounds (kilograms) of ggbfs calculated by absolute volumes.

Fine Enter the actual pounds (kilograms) of fine aggregate adjusted by moisture content.

Enter the actual pounds (kilograms) of intermediate aggregate adjusted by moisture content.

Coarse Enter the actual pounds (kilograms) of coarse aggregate adjusted by moisture content. Enter the calculated difference between the actual weights (masses) and the dry weights

(masses) of both fine and coarse aggregates.

Plant Enter the average pounds (kilograms) of water added at the plant for each cu. yd. (m³). Enter the average pounds (kilograms) of water added on the grade (when permitted by

specification).

Avg. W/C Ratio

Enter the ratio of total water in one cu. yd. (m³) divided by the total sum of cement and fly ash in one cu. yd. (m³), report to three decimal places.

CPI Gradations

This section of the report is for reporting the Certified Plant Inspector gradation test results for the coarse and fine aggregates being used in the mix. If one of the tests fail and backups are tested, record the average in the column provided, which is located just right of the specifications column.

Batched (Today or Week)

Place an "X" under the Today column if the report is being submitted daily (paving). Place an "X" under the Week column if the report is being submitted weekly (structures).

Concrete Batched

Enter the total cu. yd. (m³) of concrete batched under the appropriate column. Paving plant totals are normally under the Today column; structural concrete totals are normally under the Week column.

To Date Total

Enter the running total for both concrete and cement.

Air Entraining (Air Ent.)

Enter the brand name or source, average rate per cu. yd. (m³), and lot number.

Water Reducer (Wat. Red.)

Enter the brand name or source, average dosage rate, and lot number.

Retarder

Enter the brand name or source, average dosage rate, and lot number.

Calcium Chloride (Cal. Chlor.)

Enter the brand name or source, average dosage rate, and lot number only when added at the plant site.

Superplasticizer (Superplas.)

Enter the brand name or source, average dosage rate, and lot number.

Concrete Treatment

Place an "X" directly behind Ice, Heated Water, or Heated Materials, if one or more are used. If ice is used to cool the mix, enter the pounds (kilograms) of ice per cu. yd. (m³).

Cement

Enter the cement type, specific gravity, and source. See IM 401 for the actual source name.

Fly Ash

Enter the type and specific gravity and source. See IM 491.17 for the actual source name.

<u>Example:</u> Chillicothe and ISG Headwaters are <u>not</u> source names.

Ottumwa is the source name.

Rock

Enter the T203 A number, and gradation number.

GGBFS

Enter the grade, specific gravity, and source. See IM 491.14 for the actual source name.

Sand

Enter the T203 A number, and gradation number.

Intermediate

Enter the T203 A number.

Remarks

Enter delays, which may take place. Enter description of noncomplying test results.

CPI

Enter the Certified Plant Inspector name and certification number.

Monitor

Enter the plant monitor name and certification number.

If using the computer spreadsheet, most of this information will be entered on the Project Information and Mix Information sheets and automatically transferred to the Report. For QMC and BR mixes, the combined gradation will be calculated from aggregate percentages entered in the Mix Information Station From and To, Totals to Date Cement and Concrete, and Remarks will be entered directly on the Report.

The next page is an example of a completed Paving Plant Report.

800240E - 04/00 computer

April 19, 2005 Supersedes October 2, 2001

		Loca																	k Mix(x)	Check		SEND
Placeme	1	From	То	7 000	Project No.:	-			_ 0		17-0185-11		6		Report No.:		-	Central	X	Paving	X	(Daily)
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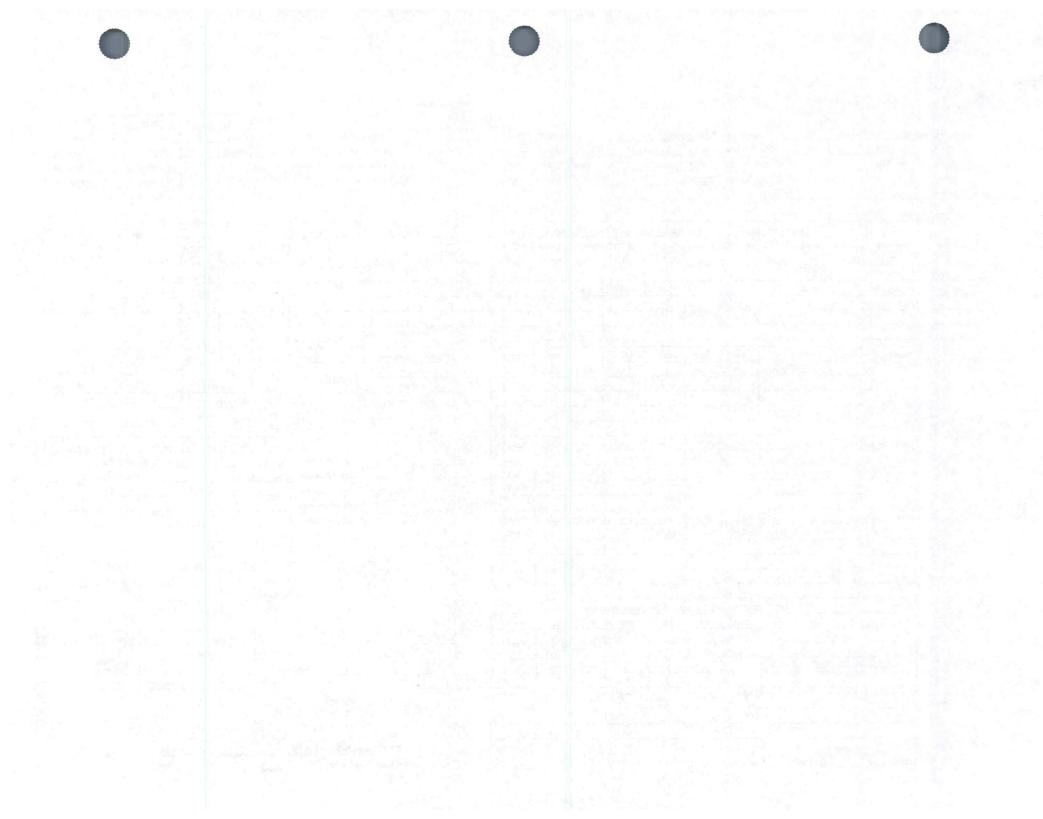
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Mix 4 Mix 5																						
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	(CY)	Used	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	Cement	Fly Ash	GGBFS	Fine	Inter.	Coarse	In Agg.	Plant	Grade	Ratio	Ratio
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				10000					0.0		NA	Q1 / 1/4/5			Water	Reducer:	Plastocre	te 161	T. P. J.		J60011P	
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			7				1000			- 10					Calcium	Chloride:		- 12				
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C.P.I.: John Doe

Monitor: Mike Brown



			County :
Mix No.:	Po	unds Cement:	
1st Adjus	ted lbs. Cement:	Source:	Sp. Gr.:
I.M. 491.17	Fly Ash:	Source:	Sp. Gr.:
I.M. 491.14	Slag GGBFS:	Source:	Sp. Gr.:
2nd Adjus	ted lbs. Cement:		
То	tal Cementitious		
I.M. T-203	Fine Aggregate Source:		Sp. Gr.:
I.M. T-203 I.M. T-203	Interm. Aggregate Source:		Sp. Gr.:
1.W. 1-203	Coarse Agregate Source:		Sp. Gr.:
Basic w/c		Water (lbs/cy) = Design w/c (wt. cement + wt F	Iv Ash +Slag) =
Max w/c	ALCOHOLOGICA CONTRACTOR	Max. Water (lbs/cy) = Design w/c (wt. cement + wt F	
			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Absolute Volumes			
	Cement	(lbs/cy) / (Sp. Gr. X 62.4 X 27)	
	. Na <u>niki ka</u>		
	Fly Ash	(lbs/cy) / (Sp. Gr. X 62.4 X 27)	
	Slag	(lbs/cy) / (Sp. Gr. X 62.4 X 27)	· <u></u>
	Water	(lbs/cy) / (1.00 X 62.4 X 27)	
	Air		0.06
		Subtotal	=
		Subtotal	= <u>-</u>
			= = =1.00
% FA Agg :		1.000 - Subtotal Total	
% FA Agg.: _	Fine A	1.000 - Subtotal Total .ggregate (1.000 - Subtotal) X % In Mix	= = =
% In. Agg.:	Fine A	1.000 - Subtotal Total ggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix	
	Fine A	1.000 - Subtotal Total .ggregate (1.000 - Subtotal) X % In Mix	
% In. Agg.: _ % CA Agg.: _	Fine A	1.000 - Subtotal Total ggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix	
% In. Agg.: _ % CA Agg.: _	Fine A Interm. Coarse	1.000 - Subtotal Total aggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total	<u> </u>
% In. Agg.: _ % CA Agg.: _	Fine A Interm. Coarse	1.000 - Subtotal Total ggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix	<u> </u>
% In. Agg.: _ % CA Agg.: _	Fine A Interm. Coarse	1.000 - Subtotal Total aggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total	
% In. Agg.: _ % CA Agg.: _	Fine A Interm. Coarse Fine Ag	1.000 - Subtotal Total Aggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Gregate (abs vol.) X Sp. Gr. X 62.4 X 27	=
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Fine A Interm. Coarse Fine Ag	1.000 - Subtotal Total aggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total gregate (abs vol.) X Sp. Gr. X 62.4 X 27 aggregate (abs vol.) X Sp. Gr. X 62.4 X 27	=
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Fine A Interm. Coarse Fine Ag	1.000 - Subtotal Total aggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total gregate (abs vol.) X Sp. Gr. X 62.4 X 27 aggregate (abs vol.) X Sp. Gr. X 62.4 X 27	=
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Fine A Interm. Coarse Fine Ag	Total Aggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Gregate (abs vol.) X Sp. Gr. X 62.4 X 27 Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Cement (lbs/cy)	=
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Fine A Interm. Coarse Fine Ag	1.000 - Subtotal Total Aggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total gregate (abs vol.) X Sp. Gr. X 62.4 X 27 a Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Cement Cement [Ibs/cy] [Ibs/cy]	=
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Fine A Interm. Coarse Fine Ag	Total Interpretation of the content	=
% In. Agg.:	Fine A Interm. Coarse Fine Ag	Total Interpretation of the content	=



Distribution: ____ DME ____ Proj. Eng. ____ Plant

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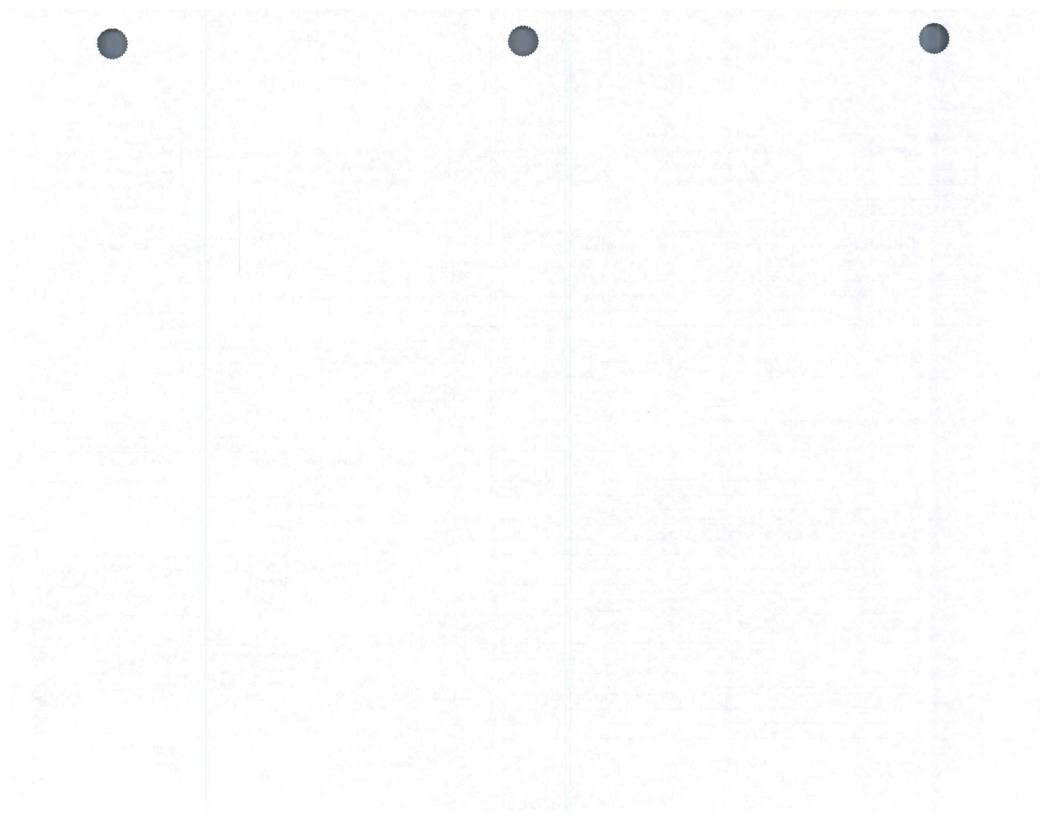
SE000

SE999

E computer	VER 1-06	3										PCC	Plant Report									
		Loca	ation							Problem	#11							Check	Mix(x)	Check	One(x)	SEND
of Placem	nent	From	То	Pr	oject No.:	FN-63-1	(26)38-63	3	Co	ntract ID:	28634	4 7 :		R	eport No.:	4		Central	х	Paving	X	(Daily)
Mix 1	6/18/06		47. 59	Pla	ant Name:	Manatt's	Hwy 146		34 80	County:	Jefferson					06/18/06		Ready		Structure		(Weekly
Mix 2				C	ontractor:	Manatt's	Inc.	MATERIAL SERVICES	Temp.	(°F) Min:	68			Date Of La	st Report:	06/17/06				Incidenta		(Weekly
Mix 3	Tara Maria		A 12		Weather:	Warm-C	loudy		Temp.	(°F) Max:	83			Structures	Des. No:					Patching		(Weekly
Mix 4	2 12 1																					
Mix 5																						
		19.7	Fi	ne Aggre	gate	Intern	nediate A	ggregate	Co	arse Agg	regate	777	Ac	tual Quant	tities Used	Per cy (in)	oounds)		2 1/4	Avg	Max
Mix	Batched	% Of Est.	Moist.	T-203	Wt. SSD		T-203	Wt. SSD	Moist.	T-203	Wt. SSD		- F			1.8 3			Water		w/c	w/c
	(CY)	Used	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	Cement	Fly Ash	GGBFS	Fine	Inter.	Coarse	In Agg.	Plant	Grade	Ratio	Ratio
-4-C20	500.00		2.7	1			146		2.7	THE A	1		6 80	- 1	. 1/1/1 -			33	240.0		- 19	
		ACE		1 1 1 1 1 1	2402-5	B 12	A Port	-27 - 31		9 16 1	-		5.5	100		Tigrati I	ar sk	V 1		-50/N-	6 7 15	
Marie Inc	FIRE I				25 M S	12 7.47			1			ER EF.	19:45	Tipon					11-12-1	CRUST.		
19	ALC:	23975			Wall of		177.3	E 7	4	124		30 T.					11.3		76.1		19.17	13.8
							42 77				- 18 7 M	100				The state of						
	Coarse	THE !	1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply		Conc. Tr	aatmant	(X)	lb / au				Batche		
	Coarse			- 5	3/4		3/6		-					eatment	(*)	lb / cy		. 100				
			100	95-100		25-60		0-10	0-5	0-1.5	Y/N		lce Heated	Water	11/19/19			Chaak	One (X)	Today X	Week	Total
					-Photos								Heated M		Mar o	175				^		To Date
			10 10					E-6 -07	No.				neated iv	lateriais		48		Concrete				1
				100			7.5 1	-		-								Cement	(tons):			10.7
	Intermedia	te	1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply					Г	Bra	nd / Sou	rce	Rate	Lot Nur	nher
	intermedia		1 1/2	La Barri	3/4	1/2	3/0		#0	#200	NA				Air Er	ntraining: D	arex AE			5.0 oz./yd.		libei
	40.55	1500	Acres	17770	1	1.60	100	dames.	Carlot In	Y	NA					Reducer:	UI UX AL		St. a. a. p. of	3.0 02./yu.	333034	
		7	3775				12.00	180 30	7 6	100	NA					Retarder:			7.3			2000
			0.00				1-10	ALLE			INA				Calcium						B (E. 17	
	Fine	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200	Comply					asticizer:			12 1			
	1 1110	1/2	100	90-100	70-100	#10	10-60	#30	#100	0-1.5	Y/N				Superpi	asticizer.	100		- 1			
		- CALLERS !	100	30-100	70-100		10-00		TATE OF	0-1.5	1710											
		500	1		7.77													Туре	Sp. Gr.		Source	
	75 - 75 - 74			P. La	777		p resi				1					C	ement:	1/1			Ash Grove	7
		(MAY S. J.	V 51 35	0.5	3100	200	Was die				171						/ Ash:	C		Lou	uisa Genera	
				Adjuste	d % Passi	ing Calcu	lated Con	nbined Grad	lation		Unit les						BFS:			LO	nsa Genera	atting
	1.5"	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200	Within					- [- [77.5	1.3.1	9/1/29
Target				- Sar	-3.7	1-121-1		a 1/69					Target	E. N. Se				Sou	rce	T-203 A#	Grad. No.	
		58.75		777	W 1914		4.4	27 27 19			725	A COL				C	oarse:	Moscow		A70002	3	3.4
		13.1	N WEST	100	-0.5		, alter	- 1900				WES	- FV - V	100		Interm						
144	Our Re-				J. F.		STANK N	100	170164	F 17. 7	PER PER	Contract of						Hoffman	-	A90504	1	
														ACC ACC.				Tommun		700004		J

C.P.I.: John Doe

Monitor: Mike Brown



Project No.:				County :	
Mix No.:	Pounds Cem	ent:			
1st Adjus	ted lbs. Cement: So	ource:		Sp. Gr.:	4 3
I.M. 491.17	Fly Ash: So	ource:		Sp. Gr.:	
I.M. 491.14	Slag GGBFS: So	ource:		Sp. Gr.:	i vis
2nd Adjus	ted lbs. Cement:				
То	tal Cementitious				
I.M. T-203	Fine Aggregate Source:			Sp. Gr.:	
I.M. T-203	Interm Aggregate Source:			Sp. Gr.:	
I.M. T-203	Coarse Agregate Source:			Sp. Gr.:	21
Basic w/c	Wate	(lbs/cv) = De	sign w/c (wt. cement + wt F	lv Ash +Slag) =	
Max w/c			sign w/c (wt. cement + wt F		1100
bsolute Volumes					
	Cement	(lbs/cy) / (Sp. Gr. X 62.4 X 27)	- <u>-</u>	
	Fly Ash	(lbs/cy) / (Sp. Gr. X 62.4 X 27)	-	
	Slag	(lbs/cy) / (Sp. Gr. X 62.4 X 27)		
	Water	(lbs/cy	y) / (1.00 X 62.4 X 27)		
	Air				0.060
			Subtotal		
			1.000 - Subtotal	242	
			Total		1.000
% FA Agg.:	Fine Aggregate (1 000 Subto	tal \ V % In Mix		
% In. Agg.:	Fine Aggregate (
% CA Agg.:	Interm. Aggregate Coarse Aggregate			1-	7 10 1
			Aggregate Total		
Aggregate Weights			Aggregate Total	- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	
	Fine Aggregate (abs vol.) X Sp	. Gr. X 62.4 X 27	- <u></u>	100
	Intermediate Aggregat	e (abs vol.)	(Sp. Gr. X 62.4 X 27	<u> </u>	
	Coarse Aggregate	(abs vol.) X S	p. Gr. X 62.4 X 27	= <u>_</u>	
Summary		ement	(lbs/cy)		
		ly Ash	(lbs/cy)		
		Slag	(lbs/cy)		
		Water	(lbs/cy)		
	Fir	ne Agg.	(lbs/cy)		
	Interr	n. Agg.	(lbs/cy)		

9-15

Distribution: ___ Materials, ___ TC, ___ Proj. Engr., ___ Contractor



DME _

Distribution:

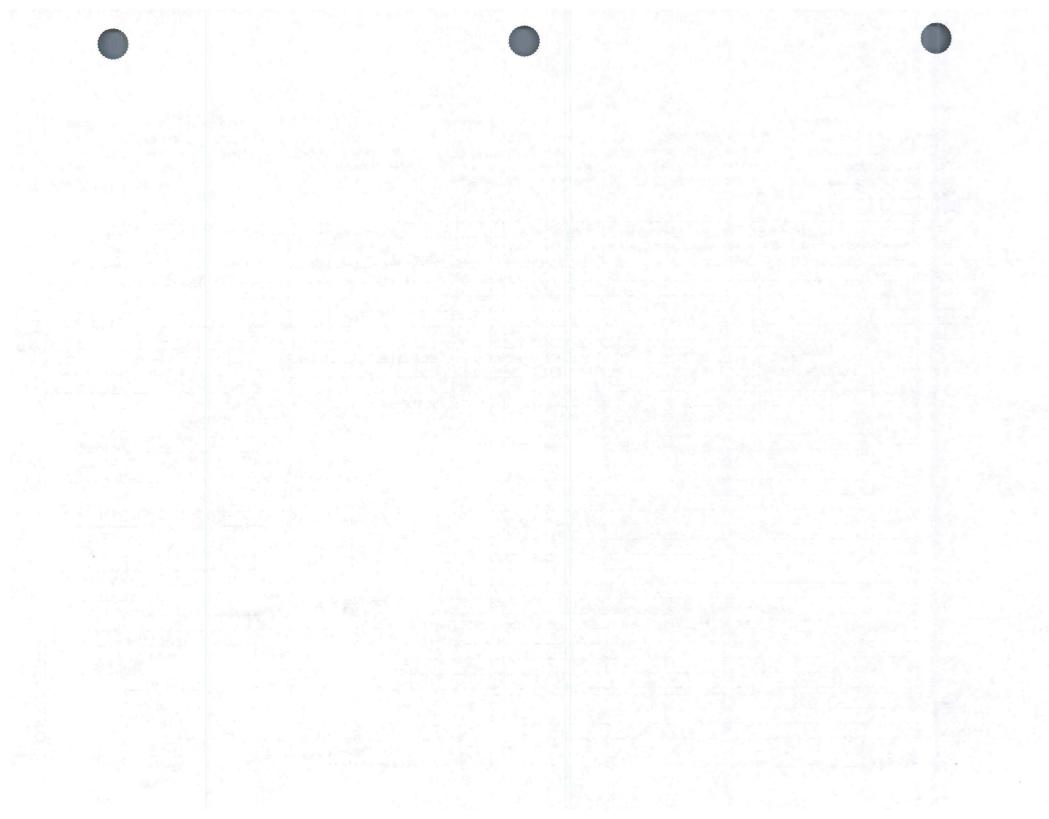
_ Proj. Eng.

Plant

NW999

		Loca	ation									Problem	#12					Check	(Mix(x)	Check	One(x)	SEND
ate of Placem	ent	From	То	Pr	oject No.:	BROS-6	8(22)10		Co	ntract ID:	28634			R	eport No.:	1		Central		Paving		(Daily
Mix 1	8/6/06		6					e - Carroll		County:		13-30				08/06/06	7	Ready		Structure	X	(Weel
Mix 2		112			ontractor:				Temp.	(°F) Min:				Date Of La					2.14	Incidenta		(Weel
Mix 3		fine in		100	Weather:					(°F) Max:				Structures			186			Patching		(Weel
Mix 4	- 1	11/1-11		Town a						(, ,							-			,		
Mix 5		8																				
			Fir	ne Aggre	gate	Intern	nediate A	ggregate	Co	arse Agg	regate		Ac	tual Quant	tities Used	Per cy (i	n pounds)	. F		Avg	М
Mix	Batched	% Of Est.	Moist.	T-203	Wt. SSD		T-203	Wt. SSD	Moist.	T-203	Wt. SSD		9		Part of		1		Water		w/c	w
	(CY)	Used	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	Cement	Fly Ash	GGBFS	Fine	Inter.	Coarse	In Agg.		Grade	Ratio	Ra
-3WR-C20S35		Oscu	3.1	Op. 0.	(150)	(70)	ор. о.	(100)	0.8	ор. о.	(100)	Comone	11971011	000.0	Time	mitor.	Course	m Agg.	180.0	18.0	rtatio	
544K-C20555	77.00		3.1					Table 3	0.0	1			12.44					700	100.0	10.0	y 200 No.	
			3 - 3 -													20013					No.	
											1.79											
	Coarse		1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply	1	Conc. Tr	eatment	(X)	lb / cy	3			Batche		
			100	95-100		25-60		0-10	0-5	0-1.5	Y/N	1	Ice					65		Today	Week	То
			1000						3-11-			17.76	Heated					Check	One (X)		X	To [
						35 100						10,74	Heated M	laterials				Concret	e (CY):			-
										4								Cement	t (tons):			1
	Intermedia	to	1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply						Br	and / Sou	Irco	Rate	Lot Nur	mbor
	intermedia	le	1 1/2	•	3/4	1/2	3/0	#**	#0	#200	NA				Air E	ntraining:	Darex AE		irce	5.0 oz./yd.		libei
					77 77	75.00			0.00			11.								3.0 02./yu.	5577882	
											NA					Reducer:	Plastocre	ete 101			55//662	
											NA					Retarder:						
												100				Chloride:						
	Fine	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200	Comply				Superpl	asticizer:						
			100	90-100	70-100		10-60			0-1.5	Y/N											
			NA.		77.1	- 1 AV	1,11				111							Туре	Sp. Gr.	- 14.31	Source	
									77.6								Cement:	1/11	3.14		Ash Grove	е
						34 1				t jed i i							Fly Ash:		С		Burlington	n
				Adjuste	d % Passi	ing Calcu	lated Con	bined Grad	dation	84.55							GGBFS:			Н	olcim-Gran	cem
	1.5"	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200	Within	4.78			1	Time		X 1 7 7 7		
Target			THE SECOND		900							W. 7.2	Target	100			10.11	Sou	ırce	T-203 A#	Grad. No.	
				100		F 75	. 772			1070							Coarse:			A57018	3	
	1	The state of	4000							7-17-0		100		9.0		Inte	rmediate:					. 4
		0.1915	144					77.00									Fine:			A53508	1	
1					2 1 2			1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1				S. T.	13 July 1	P. P. 18 1				HILL!	11315	4 1 3 2		75
Remarks							400			_												
						212.34																
340			12.7			1 5				G. le	-4											
														C.P.I.:	John Doe					NW000		

Monitor: Mike Brown



Project No.:				County :	340
Mix No.:		Pounds Cement:	<u></u>		
1st Adjus	ted lbs. Cement:	Source:		Sp. Gr.:	(- ks
I.M. 491.17	Fly Ash:	Source:		Sp. Gr.:	
I.M. 491.14	Slag GGBFS:	Source:		Sp. Gr.:	
2nd Adjus	ted lbs. Cement:				
То	tal Cementitious				
I.M. T-203	Fine Aggregate Source:			Sp. Gr.:	5.5
I.M. T-203 I.M. T-203	Interm. Aggregate Source: Coarse Agregate Source:			Sp. Gr.:	
Basic w/c		Water (lbs/cv) = De	esign w/c (wt. cement + wt Fl	v Ash +Slag) =	
Max w/c	The Article of the Control of the Co		esign w/c (wt. cement + wt Fl		C1435
	THE WATER STATE OF	11 11 11		41 (4) 17. 472	440
absolute Volumes	Cement	(lbs/c	y) / (Sp. Gr. X 62.4 X 27)	. =	
	Fly Ash	(lbs/c	y) / (Sp. Gr. X 62.4 X 27)		
	Slag		y) / (Sp. Gr. X 62.4 X 27)		
	Water		y) / (1.00 X 62.4 X 27)	•	ave.
	Air				0.060
			Subtotal		
			1.000 - Subtotal		
			Total		1.000
% FA Agg.:	Fine	Aggregate (1.000 - Subto	otal) X % In Mix		
% In. Agg.:	Interm	n. Aggregate (1.000 - Sub	total) X % In Mix	=	
% CA Agg.: _	Coars	se Aggregate (1.000 - Sub	total) X % In Mix		
			Aggregate Total		
Aggregate Weights	Fine /	Aggregate (abs vol.) X Sp	p. Gr. X 62.4 X 27		
	Intermedi	ate Aggregate (abs vol.)	X Sp. Gr. X 62.4 X 27		
	Coarse	e Aggregate (abs vol.) X S	Sp. Gr. X 62.4 X 27	<u>.</u>	
Summary		Cement	(lbs/cy)		
		Fly Ash	(lbs/cy)		
		Slag	(lbs/cy)		
		Water	(lbs/cy)		
		Fine Agg.	(lbs/cy)		
		Interm. Agg Coarse Agg.	(lbs/cy)		



Remarks

Distribution: _

DME ____

Proj. Eng. _

Plant

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40E computer	VER 1-06												Plant Report							beine.		7
		Loca									Problem #	13							Mix(x)		One(x)	SEND
e of Placem	The second second	From	То	7	oject No.:				7	ntract ID:		and a			eport No.:		- 114	Central	X	Paving	X	(Daily
Mix 1	9/17/06			W. 34			's - Hwy 2'	18 & F62		County:	-				- 10	09/17/06		Ready		Structure		(Wee
Mix 2	9/17/06			Co	ontractor:	Fred Car	rlson Co.			(°F) Min:		de la				09/16/06	1297			Incidental	-	(Wee
Mix 3		The Late		-	Weather:	Sunny-h	ot	COLUMN TO SERVICE SERV	Temp.	(°F) Max:	87			Structures	s Des. No:		-			Patching		(Wee
Mix 4																						
Mix 5		The harden																				
	- Calcin		Fin	e Aggreg	gate	Interm	nediate A	ggregate	Co	arse Agg	regate	New York	Ac	tual Quant	tities Used	d Per cy (i	pounds)			Avg	Ma
Mix	Batched	% Of Est.	Moist.	T-203	Wt. SSD	Moist.	T-203	Wt. SSD	Moist.	T-203	Wt. SSD		1	100					Water	4 (4)	w/c	w/
	(CY)	Used	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	Cement	Fly Ash	GGBFS	Fine	Inter.	Coarse	In Agg.	Plant	Grade	Ratio	Ra
-3WR-C20	1,256.00		3.1	1557.		AND THE	1	12, 110	0.7	1 3 4		Maria		(SIL		A TOTAL			175.0			
-3WR-C20	1,384.00		2.8	DE 18	10 B		- 49 77	-77	0.5	102 14 1		1085	P. FIT	W Ten		THE P		18 91	190.0		79-87	Section 1
	1,00			12 50			ST 7 76		1, 977			9 (3-15)	E-1672	8 7		1 10 30	- 7	13.11				
	100.00	10.		100	20,77			SAN SAL		- X-	J 17	1	PART -		1			7.3		E 50 %		
			-		52 T 37	7 7 7	17745	197100	- NE	THE STATE	THE R						1-0-18				1 474 17	
	7 2 2 2 2												Y ALBERT			- 23	1					
	Coarse		1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply		Conc. Tre	eatment	(X)	lb / cy	1			Batche	d	
		Take W	100	95-100		25-60		0-10	0-5	0-1.5	Y/N	1 1	Ice	7 12-7	Tr. of a					Today	Week	Tot
								2.34		1			Heated	Water				Check	One (X)	X	4 3	To D
									W at			100	Heated M	aterials				Concret	e (CY):			
		No. of the last			HAVE			and the		-	3118							Cement	(tons):	247	N Em	
				P / 1984	1934		10.00	1111111	250		The same							The state of				
	Intermedia	te	1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply						Bra	nd / Sou	rce	Rate	Lot Nun	mber
						18 - 79	5 60 E				NA				Air E	ntraining:	Ad/Aire		Tor	5.0 oz./yd.	233998	
	34 18 1	THE RESERVE	168 -9	The state of					1102		NA	Dr. A			Water	Reducer:	Daratard	17	139 5		5577882	
											NA					Retarder:	1502					
			TONE -		3 (1 1 1 1 1 1 1		37.15		en a			Calcium	Chloride:						1
	Fine	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200	Comply				Superpl	asticizer:		Section 1	100	(705) ·	F-10	7.3
		E LA	100	90-100	70-100	1111	10-60	and L	FF 4.6	0-1.5	Y/N	1						7. 1	8 15.7	Tun T	E C Fre	44.3
	1.75	E-SE			- A- T-	3 5		- 183 PM		- 1.0	V-9.181											
	1000	16.61	-	Jan Aba	Election 1	75 B.	16.5	78° - 17	11	-		mar 1						Туре	Sp. Gr.	W. Walla	Source	
	Str. BY 1	HILL			7 62F.	50 (2)	7. 15.44		BILL	50.7	1-17	Way T					Cement:		SM		LaFarge	75.
			. 107		19.5				44.4	151.		Die Ro					Fly Ash:		0	Ca	uncil Bluff	
	THE STATE OF		William Ta	A	10/ D		l-4-d C	- Line d C	1-41											CO	unch Bluit	5#3
					1.5V		NV	nbined Grad			"400						GGBFS:		- 100			
10.23%	1.5"	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200	Within					172				1
Target					ret line	95.0		3 9 7 1	E 1 1	-1,21			Target					Sou	ırce	T-203 A#	Grad. No.	
Target																	Coarse:			A57004	3	

	Source	T-203 A#	Grad. No.
Coarse:		A57004	3
Intermediate:	A VALL		
Fine:		A58504	1

C.P.I.:	John Doe	SE000
Monitor:	Mike Brown	SE999

		Line of the state		County:	
Mix No.:		Pounds Cement:			
1st Adjus	sted lbs. Cement:	Source:		Sp. Gr.:	HE.
I.M. 491.17	Fly Ash:	Source:	<u> </u>	Sp. Gr.:	
I.M. 491.14	Slag GGBFS:	Source:		Sp. Gr.:	
2nd Adjus	sted lbs. Cement:				
To	otal Cementitious				
I.M. T-203	Fine Aggregate So	ource:		Sp. Gr.:	
I.M. T-203	Interm. Aggregate S	Source:		Sp. Gr.:	
I.M. T-203	Coarse Agregate S	Source:		Sp. Gr.:	
Basic w/c_			cy) = Design w/c (wt. cement + w		
Max w/c_		Max. Water (lbs/	cy) = Design w/c (wt. cement + w	vt Fly Ash +Slag) =	
Absolute Volumes					
	Cement		(lbs/cy) / (Sp. Gr. X 62.4 X 27)		
	Fly Ash		(lbs/cy) / (Sp. Gr. X 62.4 X 27)	¥	7.1
	Slag	***************************************	(lbs/cy) / (Sp. Gr. X 62.4 X 27)		
	Water		(lbs/cy) / (1.00 X 62.4 X 27)	10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
	Air				0.060
			Subtotal	-	
			1000 0 11111		
			1.000 - Subtotal		
			1.000 - Subtotal		1.000
% FA Agg :		Fine Aggregate (1.000	Total		1.000
% FA Agg.:		Fine Aggregate (1.000	Total - Subtotal) X % In Mix	=	1.000
% In. Agg.:		Interm. Aggregate (1.000	Total - Subtotal) X % In Mix 0 - Subtotal) X % In Mix	=	1.000
_			Total - Subtotal) X % In Mix 0 - Subtotal) X % In Mix	=	1.000
% In. Agg.: _ % CA Agg.: _		Interm. Aggregate (1.000	Total - Subtotal) X % In Mix 0 - Subtotal) X % In Mix	=	1.000
% In. Agg.:		Interm. Aggregate (1.000	Total - Subtotal) X % In Mix 0 - Subtotal) X % In Mix 0 - Subtotal) X % In Mix Aggregate Total		1.000
% In. Agg.: _ % CA Agg.: _		Interm. Aggregate (1.000 Coarse Aggregate (1.000 Fine Aggregate (abs vo	Total - Subtotal) X % In Mix 0 - Subtotal) X % In Mix 0 - Subtotal) X % In Mix Aggregate Total		1.000
% In. Agg.: _ % CA Agg.: _		Interm. Aggregate (1.000 Coarse Aggregate (1.000 Fine Aggregate (abs vo	Total - Subtotal) X % In Mix 0 - Subtotal) X % In Mix 0 - Subtotal) X % In Mix Aggregate Total ol.) X Sp. Gr. X 62.4 X 27		1.000
% In. Agg.: _ % CA Agg.: _		Interm. Aggregate (1.000 Coarse Aggregate (1.000 Fine Aggregate (abs vontermediate Aggregate (abs	Total - Subtotal) X % In Mix 0 - Subtotal) X % In Mix 0 - Subtotal) X % In Mix Aggregate Total ol.) X Sp. Gr. X 62.4 X 27 os vol.) X Sp. Gr. X 62.4 X 27		1.000
% In. Agg.: _ % CA Agg.: _ Aggregate Weights		Interm. Aggregate (1.000 Coarse Aggregate (1.000 Fine Aggregate (abs vontermediate Aggregate)	Total - Subtotal) X % In Mix 0 - Subtotal) X % In Mix 0 - Subtotal) X % In Mix Aggregate Total ol.) X Sp. Gr. X 62.4 X 27 os vol.) X Sp. Gr. X 62.4 X 27 ol.) X Sp. Gr. X 62.4 X 27		1.000
% In. Agg.: _ % CA Agg.: _ Aggregate Weights		Interm. Aggregate (1.000 Coarse Aggregate (1.000 Fine Aggregate (abs vontermediate Aggregate (abs Coarse Aggregate (abs Coement	Total - Subtotal) X % In Mix 0 - Subtotal) X % In Mix 0 - Subtotal) X % In Mix Aggregate Total ol.) X Sp. Gr. X 62.4 X 27 os vol.) X Sp. Gr. X 62.4 X 27 total (lbs/cy)		1.000
% In. Agg.: _ % CA Agg.: _ Aggregate Weights		Interm. Aggregate (1.000 Coarse Aggregate (1.000 Fine Aggregate (abs vontermediate Aggregate)	Total - Subtotal) X % In Mix 0 - Subtotal) X % In Mix 0 - Subtotal) X % In Mix Aggregate Total ol.) X Sp. Gr. X 62.4 X 27 os vol.) X Sp. Gr. X 62.4 X 27 total (lbs/cy) (lbs/cy) (lbs/cy)		1.000
% In. Agg.: _ % CA Agg.: _ Aggregate Weights		Interm. Aggregate (1.000 Coarse Aggregate (1.000 Fine Aggregate (abs vontermediate Aggregate	Total - Subtotal) X % In Mix 0 - Subtotal) X % In Mix 0 - Subtotal) X % In Mix Aggregate Total ol.) X Sp. Gr. X 62.4 X 27 os vol.) X Sp. Gr. X 62.4 X 27 t		1.000
% In. Agg.: _ % CA Agg.: _ Aggregate Weights		Interm. Aggregate (1.000 Coarse Aggregate (1.000 Fine Aggregate (abs vontermediate Aggregate	Total - Subtotal) X % In Mix 0 - Subtotal) X % In Mix 0 - Subtotal) X % In Mix Aggregate Total ol.) X Sp. Gr. X 62.4 X 27 os vol.) X Sp. Gr. X 62.4 X 27 t		1.000



PORTLAND CEMENT CONCRETE

				County :	
Mix No.:	Po	ounds Cement:			
1st Adjus	ted lbs. Cement:	Source:		Sp. Gr.:	
I.M. 491.17	Fly Ash:	Source:		Sp. Gr.:	
I.M. 491.14	Slag GGBFS:	Source:		Sp. Gr.:	
2nd Adjus	ted lbs. Cement:				
То	etal Cementitious				
I.M. T-203	Fine Aggregate Source:			Sp. Gr.:	T. T.
I.M. T-203	Interm. Aggregate Source:			Sp. Gr.:	
I.M. T-203	Coarse Agregate Source:			Sp. Gr.:	
Basic w/c		Water (lbs/cv) = D	esign w/c (wt. cement + wt F	lv Ash +Slag) =	
Max w/c			esign w/c (wt. cement + wt F		
					- North
osolute Volumes					
	Cement	(lbs/c	y) / (Sp. Gr. X 62.4 X 27)	- 1 <u>- 1 </u>	1.43
	FLAN	(III-a-I-	-) // C- C- V C2 4 V 27)		
	Fly Ash	(lbs/c	y) / (Sp. Gr. X 62.4 X 27)		
	Slag	(lbs/c	y) / (Sp. Gr. X 62.4 X 27)		
	Water	(lbs/c	ey) / (1.00 X 62.4 X 27)	1 3 4 4 <u>3</u>	
			ey) / (1.00 X 62.4 X 27)	_	0.060
					0.060
					0.060
			Subtotal		1.006
% FA Agg :	Air		Subtotal 1.000 - Subtotal Total	- -	
% FA Agg.: _ % In. Agg.:	Air	Aggregate(1.000 - Subto	Subtotal 1.000 - Subtotal Total otal) X % In Mix	- - -	
% In. Agg.:	AirFine A		Subtotal 1.000 - Subtotal Total otal) X % In Mix stotal) X % In Mix	= = =	
% FA Agg.: _ % In. Agg.: _ % CA Agg.: _	AirFine A	Aggregate (1.000 - Subto Aggregate (1.000 - Sub	Subtotal 1.000 - Subtotal Total otal) X % In Mix stotal) X % In Mix	= = =	
% In. Agg.: _ % CA Agg.: _	AirFine A	Aggregate (1.000 - Subto Aggregate (1.000 - Sub Aggregate (1.000 - Sub	Subtotal 1.000 - Subtotal Total otal) X % In Mix stotal) X % In Mix	= = =	
% In. Agg.: _ % CA Agg.: _	AirFine /	Aggregate (1.000 - Subto Aggregate (1.000 - Sub Aggregate (1.000 - Sub	Subtotal 1.000 - Subtotal Total otal) X % In Mix stotal) X % In Mix stotal) X % In Mix Aggregate Total	= = = =	
% In. Agg.: _ % CA Agg.: _	AirFine A	Aggregate (1.000 - Subto Aggregate (1.000 - Sub Aggregate (1.000 - Sub	Subtotal 1.000 - Subtotal Total otal) X % In Mix stotal) X % In Mix stotal) X % In Mix Aggregate Total p. Gr. X 62.4 X 27	= = = =	
% In. Agg.: _ % CA Agg.: _	Air Fine A	Aggregate (1.000 - Subto Aggregate (1.000 - Sub Aggregate (1.000 - Sub ggregate (abs vol.) X S	Subtotal 1.000 - Subtotal Total otal) X % In Mix stotal) X % In Mix stotal) X % In Mix Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27	=	
% In. Agg.: _ % CA Agg.: _	Air Fine A	Aggregate (1.000 - Subto Aggregate (1.000 - Sub Aggregate (1.000 - Sub ggregate (abs vol.) X S te Aggregate (abs vol.) X S Aggregate (abs vol.) X S	Subtotal Total Total Dotal) X % In Mix stotal) X % In Mix Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27 Sp. Gr. X 62.4 X 27	=	
% In. Agg.: _ % CA Agg.: _ ggregate Weights	Air Fine A	Aggregate (1.000 - Subto Aggregate (1.000 - Sub Aggregate (1.000 - Sub ggregate (abs vol.) X S te Aggregate (abs vol.) Aggregate (abs vol.) X S Cement	Subtotal 1.000 - Subtotal Total otal) X % In Mix ototal) X % In Mix Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27 Sp. Gr. X 62.4 X 27 (lbs/cy)	=	
% In. Agg.: _ % CA Agg.: _ ggregate Weights	Air Fine A	Aggregate (1.000 - Subto Aggregate (1.000 - Sub Aggregate (1.000 - Sub ggregate (abs vol.) X S te Aggregate (abs vol.) Aggregate (abs vol.) X S Cement Fly Ash	Subtotal 1.000 - Subtotal Total otal) X % In Mix ototal) X % In Mix Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27 Sp. Gr. X 62.4 X 27 (lbs/cy) (lbs/cy)	=	
% In. Agg.: _ % CA Agg.: _ ggregate Weights	Air Fine A	Aggregate (1.000 - Subto Aggregate (1.000 - Sub Aggregate (1.000 - Sub ggregate (abs vol.) X So te Aggregate (abs vol.) Aggregate (abs vol.) X So Cement Fly Ash Slag	Subtotal Total Total Dotal) X % In Mix stotal) X % In Mix Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27 Sp. Gr. X 62.4 X 27 (lbs/cy) (lbs/cy) (lbs/cy)	=	
% In. Agg.: _ % CA Agg.: _ ggregate Weights	Air Fine A	Aggregate (1.000 - Subto Aggregate (1.000 - Sub Aggregate (1.000 - Sub ggregate (abs vol.) X So te Aggregate (abs vol.) Aggregate (abs vol.) X So Cement Fly Ash Slag Water	Subtotal Total Total Dotal) X % In Mix stotal) X % In Mix Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27 Sp. Gr. X 62.4 X 27 (lbs/cy) (lbs/cy) (lbs/cy) (lbs/cy)	=	
% In. Agg.:	Air Fine A	Aggregate (1.000 - Subto Aggregate (1.000 - Sub Aggregate (1.000 - Sub ggregate (abs vol.) X So te Aggregate (abs vol.) Aggregate (abs vol.) X So Cement Fly Ash Slag	Subtotal Total Total Dotal) X % In Mix stotal) X % In Mix Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27 Sp. Gr. X 62.4 X 27 (lbs/cy) (lbs/cy) (lbs/cy)	=	



Distribution:

_ DME ____ Proj. Eng.

Plant

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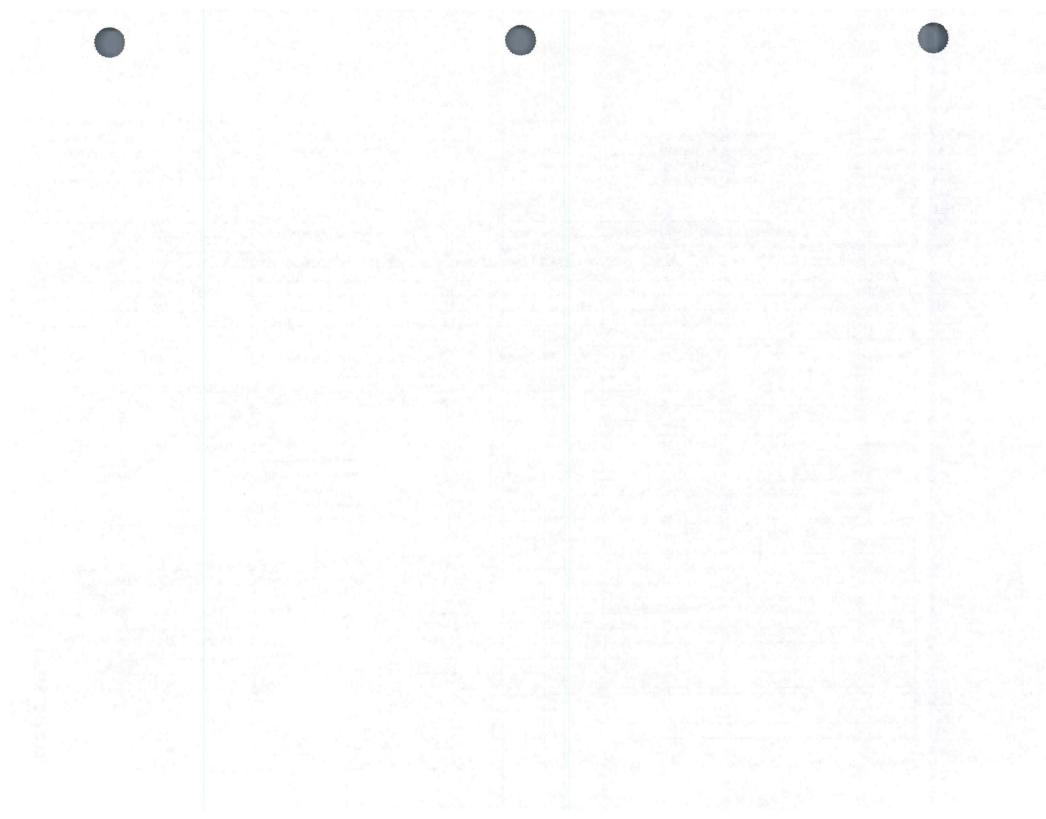
NE000

NE999

40E computer	VER 1-06											PCC	Plant Report									_
		Loca	ition								Problem #	14						Check	Mix(x)	Check	One(x)	SEND
te of Placem	ent	From	То	Pr	oject No.:	STP-53-	4(15)2C-	53	Col	ntract ID:	4920		0.49	R	eport No.:	1	100	Central	3-11-15	Paving	. 25	(Daily
Mix 1	8/6/06			Pla	nt Name:	Kirk Rea	dy Mix			County:	Jones	-1-51		Date Th	is Report:	08/06/06		Ready	X	Structure	X	(Week
Mix 2	8/6/06			Co	ontractor:	Kirk Cor	nst.		Temp.	(°F) Min:	65	1		Date Of La	st Report:					Incidental		(Week
Mix 3	8/6/06				Weather:	Sunny/W	Varm		Temp.	(°F) Max:	85	Mary .		Structures	Des. No:	4920				Patching		(Weel
Mix 4	Bully.																					
Mix 5		1-10-4	74 15																			
	SET		Fir	ne Aggre	gate	Interm	nediate A	ggregate	Co	arse Agg	regate	N. T.	Ac	tual Quant	tities Used	d Per cy (ir	pounds)			Avg	Ma
Mix	Batched	% Of Est.		T-203	Wt. SSD	Moist.	T-203	Wt. SSD	Moist.	T-203	Wt. SSD		FTE	J. 12" 1	8177			33	Water		w/c	w/
	(CY)	Used	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	Cement	Fly Ash	GGBFS	Fine	Inter.	Coarse	In Agg.	Plant	Grade	Ratio	Rat
WR-C15S35	182.00		3.7		V/12	-	7.75	- 376	0.7			178.10	DE FY			1	BILL		175.0	19.0	1 10	
C-4-C15	35.00	13.50	3.4		130	WITTEN	-	100	0.8	17-7	7 7 7		, b				- 1		183.0	25.0	1394	
M-4	14.00		3.4						0.8		71,72	7.31	12-1-12	- 13		111111111111111111111111111111111111111	174.3-5		252.0	14.0	Major	
3-17-74	1	4.4			1,5	163.00		175.175		100	W. 1. 3.	E 18.	7 10		14			13.89				
			8,85					10.4					167-327	41.50	The state of	A JUST				100		
	Coarse		1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply		Conc. Tr	eatment	(X)	lb / cy	1 5	RY AN		Batche	d	
	000.00		100	95-100	Si v	25-60	0.0	0-10	0-5	0-1.5	Y/N		Ice	Catinoni	(24)	12709			7 105	Today	Week	Tot
			100	33-100		25-00	Storing.	0-10	0.0	0-1.5		250	Heated	Water				Check	One (X)	Today	X	To D
	- 130	11111				4, 12					Top of		Heated M		- Wine-	1		Concrete		210		100
		EF T			Grie II	-	18-536	7.4		7 19 19			Treated IV	lateriais				Cement		7		1
		8.41		77.5			100	31907	7.47		1 77 4							Coment	(tono).			1
	Intermediat	te	1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply						Bra	nd / Sour	ce	Rate	Lot Nur	mber
		1,+34,-27	HE I				man.				NA				Air Er	ntraining:	Daravair	1400		3 oz./yd.	AA9912	40.00
	2 3 3 104	Box sec.	1000	3.6			5-1-	25 34	FOL IN		NA				Water	Reducer:	WRDA w	Hycol			AWR99915	5
				1984	16						NA				1	Retarder:						7 4
	5-42	W. Fred													Calcium	Chloride:			7 7 4			. 7
	Fine	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200	Comply				Superpla	asticizer:	- (c - 4)		4 4		5,391	
			100	90-100	70-100		10-60		TE_	0-1.5	Y/N								77	Ar. 1	TYY,	
		Page 1	JOLES!																276			
CARLA		de light	T W														= 100	Туре	Sp. Gr.		Source	
					145	7.73	F- (62)		1100								Cement:	11	1		LaFarge	117
		P TO SERVICE			198					- 0.		e Trial				-	ly Ash:	C			Burlington	1
			1.00	Adjuste	d % Passi	ing Calcu	lated Con	nbined Grad	dation					,			GGBFS:	12)	GE BERTHA	NewCem	6 T .
	1.5"	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200	Within	1. 18								7
Target	1000				9 : 17/1	7-13	7 3 19			2.24			Target	100			1	Sou	rce	T-203 A#	Grad. No.	- 1
												1	W				Coarse:			A53004	3	018
-							1		575					7		Inter	mediate:		100			
The same of		147	B. V. P.	-25		- 801	The state of	ENLEY	0 - 10	18							Fine:		100	A53502	1	

C.P.I.: John Doe

Monitor: Jane Doe



Mix No.:	Project No.:				County:	
1st Adjusted lbs. Cement:	Mix No.:	Poun	ds Cement:			
I.M. 491.17 Fly Ash: Source: Sp. Gr.:		- Tour				
I.M. 491.14 Slag GGBFS: Source: Sp. Gr.:	1st Adjusted	bs. Cement:	Source:		Sp. Gr.:	
2nd Adjusted lbs. Cement:	I.M. 491.17	Fly Ash:	Source:		Sp. Gr.:	1
Total Cementitious	I.M. 491.14	Slag GGBFS:	Source:		Sp. Gr.:	
I.M. T-203	2nd Adjusted	lbs. Cement:				
Interm. Aggregate Source: Sp. Gr.:	Total (Cementitious				
Description Sp. Gr. Sp. Gr.		_			Sp. Gr.:	39.22
Basic w/c		-				
Max w/c	I.M. T-203 C	oarse Agregate Source:			Sp. Gr.:	Libbs.
Max. Water (lbs/cy) = Design w/c (wt. cement + wt Fly Ash +Slag) = Design w/c	Basic w/c		Water (lbs/cy) = De	esign w/c (wt. cement + wt Fl	ly Ash +Slag) =	
Cement	Max w/c	Ma				10.2
Cement	. Volumos					
Slag	e volumes	Cement	(lbs/cy	y) / (Sp. Gr. X 62.4 X 27)	-	
Water		Fly Ash	(lbs/cy	y) / (Sp. Gr. X 62.4 X 27)	<u> </u>	
Subtotal =		Slag	(lbs/cy	y) / (Sp. Gr. X 62.4 X 27)		
Subtotal =		Water	(lbs/c)	y) / (1.00 X 62.4 X 27)	- <u>-</u>	
Total = Total		Air				0.060
Total = % FA Agg.: Fine Aggregate (1.000 - Subtotal) X % In Mix = % In. Agg.: Interm. Aggregate (1.000 - Subtotal) X % In Mix = % CA Agg.: Coarse Aggregate (1.000 - Subtotal) X % In Mix = Aggregate Total = Aggregate Weights Fine Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 = Intermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 =				Subtotal	- <u>-</u>	
% FA Agg.: % In. Agg.: % In. Agg.: % CA Agg.: % CA Agg.: % Carse Aggregate (1.000 - Subtotal) X % In Mix ### Coarse Aggregate (1.000 - Subtotal) X % In Mix ### Aggregate Total ### Aggregate Total ### Entermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 ### Intermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 #### Intermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27				1.000 - Subtotal		
% In. Agg.: % CA Agg.: Coarse Aggregate (1.000 - Subtotal) X % In Mix ### Aggregate Total ### Aggregate Weights Fine Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 #### Intermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 ###################################				Total		1.00
% In. Agg.: % CA Agg.: Coarse Aggregate (1.000 - Subtotal) X % In Mix ### Aggregate Total ### Aggregate Weights Fine Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 #### Intermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 ###################################	0/ 54 4					
% CA Agg.: Coarse Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Fine Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Intermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27						
Aggregate Total = aggregate Weights Fine Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 = Intermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 =						
Intermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 =	70 OX 7199		ig. oguto (moss out)			10.13
Fine Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 = Intermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 =				Aggregate Total	<u> </u>	
그 아내는 사람들은 아내는 내가 되었다면 하는데 되었다면 하는데 되었다.	ate Weights	Fine Aggre	egate (abs vol.) X Sp	o. Gr. X 62.4 X 27	<u> </u>	
전기 하게 하는 것이 없는 이 그는 것이 되고 있어. 아이 가장 사람들이 되고 있었다면 하는 것이 되는 것이다.		Intermediate A	ggregate (abs vol.)	X Sp. Gr. X 62.4 X 27	=_	
Coarse Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27		Coarse Agg	gregate (abs vol.) X S	p. Gr. X 62.4 X 27		
Summary Cement (Ibs/cy)	D/		Cement	(lhs/cv)		
Fly Ash (lbs/cy)			The state of the s			
Slag (lbs/cy)						
Water (lbs/cy)			the state of the s			
Interm. Agg (lbs/cy) Coarse Agg. (lbs/cy)			Intorm Aga			

	입니다 맛있 📤 이번 (10.15)		
	그 보는 바다를 보고 있는데 그리다는		
	그리의 경우의 속성으로 없었습니다.		크림인 나타를 잃었다면서 보였다.
		H. 이렇게 하고 있는 모든 것이다.	

Project No.:	Street day			County :	
Mix No.:		Pounds Cement:			
1st Adjus	ted lbs. Cement:	Source:		Sp. Gr.:	Syr.
I.M. 491.17	Fly Ash:	Source:		Sp. Gr.:	
I.M. 491.14	Slag GGBFS:	Source:		Sp. Gr.:	1. 1.
2nd Adjus	sted lbs. Cement:				
То	otal Cementitious				
I.M. T-203	Fine Aggregate S	Source:		Sp. Gr.:	
I.M. T-203	Interm. Aggregate	Source:		Sp. Gr.:	
I.M. T-203	Coarse Agregate	0		Sp. Gr.:	
Basic w/c		Water (lbs/cy) = D	esign w/c (wt. cement + wt F	ly Ash +Slag) =	
Max w/c		Max. Water (lbs/cy) = D	esign w/c (wt. cement + wt F	ly Ash +Slag) =	Y 1/4
Absolute Volumes					
	Cement	(lbs/c	y) / (Sp. Gr. X 62.4 X 27)	5 W. (<u> </u>	
	Fly Ash	(lbs/c	y) / (Sp. Gr. X 62.4 X 27)		
	Slag	(lbs/c	ey) / (Sp. Gr. X 62.4 X 27)		37.7
	Water	(lbs/c	ey) / (1.00 X 62.4 X 27)		
	Air				0.060
			Subtotal		
			1.000 - Subtotal	-	
			Total		1.000
% FA Agg.:		Fine Aggregate (1.000 - Subto			
% In. Agg.:		Interm. Aggregate (1.000 - Sub	total) X % In Mix	= _	
_			total) X % In Mix	=	
% In. Agg.: _ % CA Agg.: _		Interm. Aggregate (1.000 - Sub Coarse Aggregate (1.000 - Sub	total) X % In Mix	= _	
% In. Agg.:		Interm. Aggregate (1.000 - Sub Coarse Aggregate (1.000 - Sub	ototal) X % In Mix ototal) X % In Mix Aggregate Total	:=	
% In. Agg.: _ % CA Agg.: _		Interm. Aggregate (1.000 - Sub Coarse Aggregate (1.000 - Sub	ototal)X % In Mix ototal)X % In Mix Aggregate Total p. Gr. X 62.4 X 27	:=	
% In. Agg.: _ % CA Agg.: _		Interm. Aggregate (1.000 - Sub Coarse Aggregate (1.000 - Sub Fine Aggregate (abs vol.) X Sp	Atotal) X % In Mix ototal) X % In Mix ototal) X % In Mix Aggregate Total p. Gr. X 62.4 X 27	:=	
% In. Agg.: _ % CA Agg.: _	1	Interm. Aggregate (1.000 - Sub Coarse Aggregate (1.000 - Sub Fine Aggregate (abs vol.) X Sp Intermediate Aggregate (abs vol.)	Atotal) X % In Mix ototal) X % In Mix ototal) X % In Mix Aggregate Total p. Gr. X 62.4 X 27	:=	
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	-	Interm. Aggregate (1.000 - Sub Coarse Aggregate (1.000 - Sub Fine Aggregate (abs vol.) X S Intermediate Aggregate (abs vol.) X S Coarse Aggregate (abs vol.) X S	Atotal) X % In Mix ototal) X % In Mix Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27 Sp. Gr. X 62.4 X 27	:=	
% In. Agg.: _ % CA Agg.: _ Aggregate Weights		Interm. Aggregate (1.000 - Sub Coarse Aggregate (1.000 - Sub Fine Aggregate (abs vol.) X Sontermediate Ag	Atotal) X % In Mix btotal) X % In Mix Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27 Sp. Gr. X 62.4 X 27 [Ibs/cy]	:=	
% In. Agg.: _ % CA Agg.: _ Aggregate Weights		Interm. Aggregate (1.000 - Sub Coarse Aggregate (1.000 - Sub Fine Aggregate (abs vol.) X Sontermediate Ag	Atotal) X % In Mix (atotal)	:=	
% In. Agg.: _ % CA Agg.: _ Aggregate Weights		Interm. Aggregate (1.000 - Sub Coarse Aggregate (1.000 - Sub Fine Aggregate (abs vol.) X Sontermediate Ag	Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27 Sp. Gr. X 62.4 X 27 (lbs/cy) (lbs/cy) (lbs/cy)	:=	
% In. Agg.: _ % CA Agg.: _ Aggregate Weights		Interm. Aggregate (1.000 - Sub Coarse Aggregate (1.000 - Sub Fine Aggregate (abs vol.) X Suntermediate Ag	Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27 Sp. Gr. X 62.4 X 27 (lbs/cy) (lbs/cy) (lbs/cy) (lbs/cy)	:=	



Project No.:		<u></u>		County :	
Mix No.:	F	Pounds Cement:			
1st Adjus	ted lbs. Cement:	Source:		Sp. Gr.:	in the
I.M. 491.17	Fly Ash:	Source:		Sp. Gr.:	
I.M. 491.14	Slag GGBFS:	Source:		Sp. Gr.:	
2nd Adjus	ted lbs. Cement:				
То	etal Cementitious				
I.M. T-203	Fine Aggregate Source:			Sp. Gr.:	
I.M. T-203	Interm. Aggregate Source:			Sp. Gr.:	and the
I.M. T-203	Coarse Agregate Source:			Sp. Gr.:	
Basic w/c		Water (lbs/cy) = D	esign w/c (wt. cement + wt F	Fly Ash +Slag) =	
Max w/c	HISTORIA Y SHIP		esign w/c (wt. cement + wt F		
Absolute Volumes					
	Cement	(lbs/c	y) / (Sp. Gr. X 62.4 X 27)		
	Fly Ash	(lbs/c	y) / (Sp. Gr. X 62.4 X 27)		
			-1// C- C- V CO 4 V CT)	=	
	Slag	(lbs/c	y) / (Sp. Gr. X 62.4 X 27)	A. The second	1
	Water		sy) / (Sp. Gr. X 62.4 X 27)		
	Water	(lbs/c			0.060
	Water	(lbs/c	ey) / (1.00 X 62.4 X 27)		0.060
	Water	(lbs/c	y) / (1.00 X 62.4 X 27)		0.060
	Water	(lbs/c	ey) / (1.00 X 62.4 X 27)		0.060
	Water	(lbs/c	sy) / (1.00 X 62.4 X 27) Subtotal		1.000
% FA Agg.: _	Water Air Fine	Aggregate (1.000 - Subto	Subtotal 1.000 - Subtotal Total	=	
% FA Agg.: _ % In. Agg.: _	Water Air Fine	(lbs/c	Subtotal 1.000 - Subtotal Total	=_ =_ =_ =_	
_	Water Air Fine Interm	Aggregate (1.000 - Subto	Subtotal 1.000 - Subtotal Total otal) X % In Mix total) X % In Mix	=_ =_ =_ =_	
% In. Agg.:	Water Air Fine Interm	Aggregate (1.000 - Subto Aggregate (1.000 - Subto Aggregate (1.000 - Sub e Aggregate (1.000 - Sub	Subtotal 1.000 - Subtotal Total otal) X % In Mix total) X % In Mix	=_	
% In. Agg.:	Water Air Fine Interm	Aggregate (1.000 - Subto Aggregate (1.000 - Subto Aggregate (1.000 - Sub e Aggregate (1.000 - Sub	Subtotal 1.000 - Subtotal Total otal) X % In Mix stotal) X % In Mix stotal) X % In Mix	=_	
% In. Agg.: _ % CA Agg.: _	Water Air Fine Interm Coarse	Aggregate (1.000 - Subto Aggregate (1.000 - Subto Aggregate (1.000 - Sub e Aggregate (1.000 - Sub	Subtotal 1.000 - Subtotal Total otal) X % In Mix total) X % In Mix total) X % In Mix Aggregate Total	=_	
% In. Agg.: _ % CA Agg.: _	Water Air Fine Interm Coarse	Aggregate (1.000 - Subto Aggregate (1.000 - Subto Aggregate (1.000 - Sub Aggregate (1.000 - Sub	Subtotal 1.000 - Subtotal Total otal) X % In Mix total) X % In Mix total) X % In Mix total) X % In Mix	=_	
% In. Agg.: _ % CA Agg.: _	Water Air Fine Intermedia	Aggregate (1.000 - Subton. Aggregate (1.000 - Subton. Aggregate (1.000 - Subton. Aggregate (1.000 - Subton.) X Sparegate (abs vol.) X Sparegate (Subtotal 1.000 - Subtotal Total otal) X % In Mix total) X % In Mix total) X % In Mix total) X % In Mix Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27	=_	
% In. Agg.: _ % CA Agg.: _	Water Air Fine Intermedia	Aggregate (1.000 - Subton. Aggregate (1.000 - Subton. Aggregate (1.000 - Subton. Aggregate (abs vol.) X Spate Aggregate (abs vol.)	Subtotal 1.000 - Subtotal Total otal) X % In Mix total) X % In Mix total) X % In Mix total) X % In Mix Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27	=	
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Water Air Fine Intermedia	Aggregate (1.000 - Subton. Aggregate (1.000 - Subton. Aggregate (1.000 - Subton.) X Sparter Aggregate (abs vol.) X Sparter	Subtotal 1.000 - Subtotal Total otal) X % In Mix total) X % In Mix total) X % In Mix total) X % In Mix Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27 Sp. Gr. X 62.4 X 27	=	
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Water Air Fine Intermedia	Aggregate (1.000 - Subton. Aggregate (1.000 - Subton. Aggregate (1.000 - Subton.) X Spate Aggregate (abs vol.) X Spate Agg	Subtotal 1.000 - Subtotal Total otal) X % In Mix total) X % In Mix total) X % In Mix total) X % In Mix Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27 Sp. Gr. X 62.4 X 27 [lbs/cy]	=	
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Water Air Fine Intermedia	Aggregate (1.000 - Subton. Aggregate (1.000 - Subton. Aggregate (1.000 - Subton.) X Spate Aggregate (abs vol.) X Spate Agg	Subtotal 1.000 - Subtotal Total Total otal) X % In Mix total) X % In Mix total) X % In Mix Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27 Sp. Gr. X 62.4 X 27 (lbs/cy) (lbs/cy) (lbs/cy)	=	
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Water Air Fine Intermedia	Aggregate (1.000 - Subton Aggregate (1.000 - Subton Aggregate (1.000 - Subton Aggregate (abs vol.) X State Aggregate (abs	Subtotal 1.000 - Subtotal Total Total otal) X % In Mix total) X % In Mix total) X % In Mix Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27 Sp. Gr. X 62.4 X 27 (lbs/cy) (lbs/cy) (lbs/cy) (lbs/cy)	=	
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Water Air Fine Intermedia	Aggregate (1.000 - Subton Aggregate (1.000 - S	Subtotal 1.000 - Subtotal Total Total otal) X % In Mix total) X % In Mix total) X % In Mix Aggregate Total p. Gr. X 62.4 X 27 X Sp. Gr. X 62.4 X 27 Sp. Gr. X 62.4 X 27 (lbs/cy) (lbs/cy) (lbs/cy)	=	



PROBLEM 14

Calculate the cement yield

- 4096 lb. cement in scale hopper from last cement yield check.
- 4872 batches at 623 lb./batch
- 615 batches at 604 lb./batch
- 66 batches at 823 lb./batch
- 3000 lb. left in scale hopper

Total weight billed is 3,333,333 lb. (1666.67 Ton)



PROBLEM 15

Calculate the cement yield given the following

- 2600 lb. cement left in scale hopper from last yield check
- 1480 batches at 492 lb./batch
- 500 batches at 571 lb./batch
- 3000 lb. cement left in hopper this check
- Total billed weight is 512.05 Ton
- Show your work in Tons (convert lb. to ton)

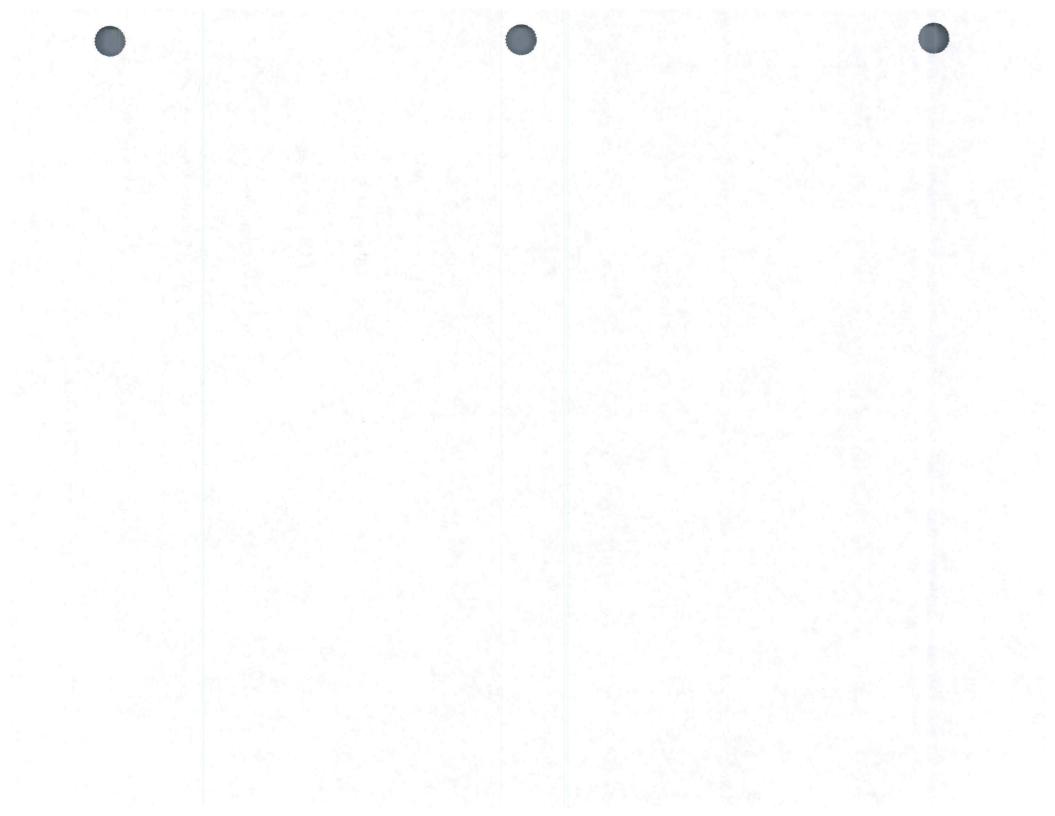
[발명 - 보이트 10 HT - HT	5.552
를 하게 받는 것도 있는데 보고 있다면 하는데 되었다면 보고 있다면 되었다면 되었다면 되었다면 되었다면 보다.	

PROBLEM 16

Cement Yield

- Tons Billed = 902.38
- Number of batches = 3180
- Batch Size = 1 yd³
- 571 lb. cement per yd³

Find cement yield in percent



IDOT CUSTOMER NO.: 1
MASON CITY IA.

JOB NO./ID. 1 #5

TICKET NO.: 34 PLANT ID.: 2495 DATE:11-24-98 TIME-12:46 7.00 CY FORMULA NO.: 1 C-3-WR-C 15% TOLERANCE: 4 QTY ORD'D: 999999.00 QTY DEL'D: 16617.00 LOADS: 2378 REQ SLUMP: 0.00

GAT	E	DESCRIP.	TARGET	ACTUAL	MC	GATE	DESCRIP.	TARGET	ACTUAL	
AGG	2	ROCK	6180	6120 LB	0.5%		/			
AGG	1	SAND	10000	9960 LB	3.2%	WTZ	2 WATER 2	154	154	GL
AGG	3	ROCK	6180	6240 LB	0.5%	AD2	2 ADA	29	29	OZ
						AD4	4 WR	116	117	OZ

CEM 1 CEM. 3290 3275 LB CEM 2 FLY ASH 580 590 LB 590 LB +

TIME-12:47 AGG 0:- 20 20 LB CEM 0: - 15 15 LB WATA: 8 GL

TRUCK NO.: 47 DRIVER NAME: JIM H. DRIVER NUMBER:

IDOT CUSTOMER NO.: 1 MASON CITY IA.

JOB NO. / ID. 1 #5

TICKET NO.: 35 PLANT ID.: 2495 DATE:11-24-98 TIME-12:46 7.00 CY FORMULA NO.: 1 C-3-WR-C 15% TOLERANCE: 4 QTY ORD'D: 999999.00 QTY DEL'D: 16624.00 LOADS: 2379 REQ SLUMP: 0.00

GATE	Ξ	DESCRIP.	TARGET	ACTUAL	MC	GATE	DESCRIP.	TARGET	ACTUAL
AGG	2	ROCK	6180	6320 LB	0.5% +				
AGG	1	SAND	10000	10020 LB	3.2%	WT2	2 WATER 2	154	154 GL
AGG	3	ROCK	6180	6140 LB	0.5%	AD2	2-ADA	29	29 DZ
						AD4	4 WR	116	116 DZ

CEM 1 CEM. 3290 3280 LB CEM 2 FLY ASH 580 580 LB

TIME-12:49 AGG 0:- 20 20 LB CEM 0: - 10 - 10 LB WATA: 13 GL

TRUCK NO.: 48 DRIVER NAME: JON W. DRIVER NUMBER:

TDOT

CUSTOMER NO. : MASON CITY IA.

JOB NO. /ID.

1 #5

1

18 PLANT ID.: 2495 DATE:11-24-98 TIME-11:10 TICKET NO. : 7.00 CY FORMULA NO.: 1 C-3-WR-C 15% TOLERANCE: 4
QTY DRD'D: 999999.00 QTY DEL'D: 16505.00 LOADS: 2362 REQ SLUMP: 0.00

GATE	DESCRIP	. TARGET	ACTUAL		MC	GAT	E	DESCR	IP.	TARGET	ACTUAL	
AGG 8	ROCK	6160	6200	LB	0.3%							
AGG :	SAND	10020	9980	LB	3.4%	WTZ	2	WATER	5	154	154	GL
AGG :	ROCK	6160	6120	LB	0.3%	ADS	2	ADA		. 29	29	OZ
						AD4	4	WR		116	117	OZ

CEM 1 CEM. 3290 3295 LB CEM 2 FLY ASH 580 580 LB

TIME-11:11 AGG 0:- 20 20 LB CEM 0: - 5 5 LB

WATA: 0 GL

TRUCK NO.: 48 DRIVER NAME: JON W. DRIVER NUMBER:

IDOT

1 CUSTOMER NO. : MASON CITY IA.

JOB NO. /ID.

1 #5

TICKET NO. : 19 PLANT ID.: 2495 DATE:11-24-98 TIME-11:13 7.00 CY FORMULA NO.: 1 C-3-WR-C 15% TOLERANCE: 4 QTY DRD'D: 999999.00 QTY DEL'D: 16512.00 LOADS: 2363 REQ SLUMP: 0.00

GATE	DESCRIP.	TARGET	ACTUAL		MC	GAT	E	DESCRIP.	TARGET	ACTUAL	
AGG 2	BUCK	6160	6100	1 B	0 74						
	SAND	10020			3.4%	ыта	2	WATER 2	154	154	COL
AGG 3		6160	6140	-		ADS			29		OZ
						AD4	4	WR	116	115	OZ

CEM 1 CEM. 3290 3295 LB 580 LB CEM 2 FLY ASH 580

00 LB CEM 0: 5 TIME-11:14 AGG 0: 00 @ LB

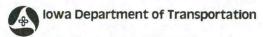
WATA: 2 GL

TRUCK NO. : 44 DRIVER NAME: POOR BOY DRIVER NUMBER: Form 830212 10-95

READY MIX CONCRETE

		Plant
Truck No.	Ticket No	
Date	Des. No	
Proj. No.		
Mix No	_ Retarder/Water Reducer? Yes	□ No
Conc. This Truck		_ C.Y./m ³
Air agent added this truck .		oz./mL
Time Batched	Discharged	120
Rev. Mixed (Plant)	Grade	
Water (gal./L or lbs./kg Th	nis Truck) 8.33lbs./gal.	
	gal./L	_lbs./kg
	gal./L	_
Subtotal	gal./L	_lbs./kg
Added Grade	gal./L	_lbs./kg
TOTAL WATER	gal./L	_ lbs./kg
	gal./L lbs./cy	
Air	Slump	
Plant Insp		
Receiving Insp.		t with the

Form 820917 11-94



Office of Materials PLANT CALIBRATION REPORT

Shaded area to be completed for paving plants and when application Contractor/Producer	County	its.	
Plant Location	Project		
Class of Concrete	Mix No.(s)		
Design W/C Ratio(s)	Max W/C Ratio(s)		
MATERIAL SOURCE Producer Name &		SPECIFIC GRAVITY	DRY BATCH
Aggregate (Coarse)			
Aggregate (Find)		THE PARTY	
Cement			
Fly Ash			Sealer I
Water		sic sirin fi	4/18/18/
Air Entraining Agent			A LIVE
Curing Compound			
Water Reducing Agent			
Retarding Admixture			
alibrated by:	Fitle:	Date Date Date Date Date Date Date Date	e:
oarse Aggregate Sampling Point:			2 17.5
emarks:			
lote: Circulation of air entraining, water reducing, and retarding	admixtures is required prior to us	e.	
his above data is furnished by the Contractor/Producer as so orth in the Standard Specifications for plant operations. The contracting Authority makes no representations as to accuracy	e	730	96 34 7
ither express or implied, which are to be construed to relieve the ontractor from the responsibility to comply with the specification:	e Title	ent operatives	NAME OF THE OWNER, OWNE

Distribution: White Copy - Plant Inspector; Canary Copy - Contractor/Producer; Pink Copy - Transportation Center Materials Engineer; Goldenrod Copy - Resident Engineer Send copy to Central Materials on city and county projects. (PCCP Only)

Matls. IM 527 Appendix D

PORTLAND CEMENT & READY MIX PLANT CALIBRATION CHECKLIST

References: IM 527, 528 and noted Specifications

STORAGE & HANDLING OF MATERIALS

Aggregates: 2301.13

- Certified compliance
- Separation of materials
- Storage area floor shall be a minimum of 18" of similar material
- Fine aggregates shall drain a minimum of 24 hours on new bridge deck floors-2412.02

Cementitious Material: 2301.13

- Approved certified sources
- No intermingling of products or sources
- Stored in suitable weather proof enclosures

WATER

Sample when required

ADMIXTURES

- Verify acceptance of lot
- Circulate 5 min. per 100 gal. of solution
- Proper storage to prevent freezing

PLANT REQUIREMENTS

Safety:

- · Guards, ladders, railings and walkways
- Sampling location
- Proper template if belt sample
- Safety switches and belt lockouts in place
- Bins are structurally safe: 2001.06
- Settlement of footings is uniform
- Suitable wind protection for scale operation
- Automatic interlocks for projects over 6000 sq. yds: 2001.20 & 2301.13
- Weight indicator or digital readouts are in full view of the plant operator.

Scale Calibration: 2001.20

Calibration of batch plant scales as required by the specifications is performed by incrementally loading the scales with standard test weights and partial batches through the operating range of the scales. As each increment of load is applied, the actual observed weight and the required weight are compared. The differences plus or minus, are determined and converted to percentages of the required weight. If the percentage deviations are less than the tolerance allowed by the specifications and the scales are sensitive to the test loads, the scales will be considered in calibration. If the scales do not meet the various requirements, the contractor should be notified immediately and required to make the necessary repairs or adjustments. The engineer may order recalibration if the scale equipment malfunctions, material quantities do not agree with actual material quantities, or any repairs or replacement of equipment occurs.

- Calibrate scales to include the maximum weight for projected batches
- Commercially manufactured weights that have the weight stamped on the exterior and appear to be unaltered and in good condition may be assumed to meet the requirements of ASTM E617.
- Non-commercially manufactured test weights may be used in providing accumulating weight for loading the scales, if validated against commercially manufactured test weights.
- Accumulate calibration error at each increment that material replaces known weight.

Matls. IM 527 Appendix D

NOTE: Example uses 2000 lbs. of known weights applied at 1000 lb. increments. Accumulated error applies only when exchanging known weight with material.

Applied Wt.	Scale Reading	Error	Accum. _Error_	Wt. Replaced By Material
1000	995	-5		
2000	1995	-5	-5*	yes
3000	2990	-10	-15	<
4000	3995	-5	-10*	yes
5000	5000	0	-10	<
6000	6005	+5	-5*	yes
7000	7010	+10	+5	<

NOTE: *Accumulated error is from last known error prior to material replacement.

< Intermediate errors are measured to determine specification compliance, but are not part of the accumulated result.

As a guide, a working form to help record field calibration measurements is on page 4.

Water Calibration: 2001.20B

- Equipment shall be such that accuracy will not be affected by variations in pressure of the water supply.
- Weighing equipment to verify water calibration shall meet specification
- Repairs or adjustments will require equipment to be recalibrated.

Equipment for Dispensing Liquid Admixtures: 2001.20C

- Calibrate per Specification
- Measuring container of digital readout shall be on view of plant operator.

Truck Mixer & Agitator: 2001.21B

- Meet the requirements of specification
- Truck mixer certification (Form #820907) kept in truck and is up to date.

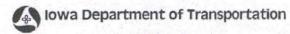
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	E	The Alex	. 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	4 5 5 7			
LOC	CATION			승기 본지	READ	Y MIX PLA	NT
	CEMEN	T SCALE -	- ACCURATI	E TO 0.5% C	F BATCH W	EIGHT	
SENS	SITIVITY - E	MPTY	F	ULL	LBS. @		_LBS.
TOLE	ERANCE – 0	.1% OF BA	TCH WEIGH	IT OR 2 LBS	s., WHICHEV	ER IS GRE	ATER
pplied	scale	3.1	accum.	applied	scale		accum
veight	reading	error	error	weight	reading	error	error
	7 15 1 1						- Articles
200							
## J. J. J.	2 10 20 41	WILL ST	(1 1 th 2 th				
					OF BATCH		
SENS	SITIVITY - E	MPTY	TCH WEIGH	ULL	LBS. @	ED IS GDE	_ LBS.

applied weight	scale reading	error	accum. error	applied weight	scale reading	error	accum. error
- 8-17-2							
1000	1				1 475.6		
	1 ME 1 ME 1	- A					
							7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
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						Acres de Maria	Date and
		U- 74		Sale North Control			1.7.1.000,18

WATER-ACCURATE TO +/-1.0% OR 2 LBS., **ADMIXTURES**-ACCURATE TO +/-3.0% OF QUANTITY REQUIRED

met	ered	scale		ar meter	ea meas.		reducer meas.	Reta meter	arder meas
gal.	lbs.	reading	error	OZ.	OZ.	OZ.	OZ.	OZ.	OZ.
		Carlotte (T	Carlo de la companya	A 18 CUC	ation of the				
				BITC	19.19	20.3			2
100									Pa y
North.							DOM:		
1,000		11 - 11 - 1							

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	1/1/31	44.15.11	Portland (Cement Sh	ipment Yield	Report			0.00	Date Su	The second secon	01/02/04		Property.
ontract ID:	29999	. 00									Ash Grove			
	FM-85(25)55	-85			Plant Loc	nation:	NW Corr E29			Contractor:	Manatt's			
County:	Story				Flant Luc	Jation.	NWV COII E25				75		10.7	100
	Invoice	Billed				Invoice	Billed				Invoice	Billed		
Date	Number	Tons	Туре		Date	Number	Tons	Туре		Date	Number	Tons	Туре	100
06/02/03	107312	28.19	I/II		06/04/03	107352	27.86	1/11		0	0	0.00	I/II	
06/02/03	107313	28.14	1/11		06/04/03	107353	27.57	1/11		0	0	0.00	1/11	
06/02/03	107314 107315	27.85 27.81	1/11		06/04/03	107354 107355	28.14 27.99	I/II		0	0	0.00	1/11	
06/02/03	107315	27.92	I/II		06/04/03	107356	28.10	I/II		0	0	0.00	I/II	PC To
06/02/03	107317	28.21	1/11		06/04/03	107357	27.79	I/II		0	0	0.00	1/11	
06/02/03	107318	25.49	1/11		06/04/03	107358	26.99	1/11		0	0	0.00	I/II	
06/02/03	107319	26.57	I/II		06/04/03	107359	27.85	I/II		0	0	0.00	1/11	
06/02/03	107320	28.06	1/11		06/04/03	107360	28.00	I/II		0	0	0.00	1/11	
06/02/03	107321	28.02	1/11		06/04/03	107361	27.94	I/II		0	0	0.00	1/11	
06/02/03	107322	28.15 28.36	1/11		06/04/03	107362 107363	27.30 28.28	1/11		0	0	0.00	1/11	-
06/03/03	107323 107324	28.36	1/11		06/04/03	107363	28.28	1/11		0	0	0.00	1/11	
06/03/03	107324	27.73	1/11		06/04/03	107364	28.50	1/11		0	0	0.00	1/11	
06/03/03	107326	28.26	1/11		06/04/03	107366	28.00	1/11		0	0	0.00	1/11	
06/03/03	107327	25.55	1/11		06/04/03	107367	27.99	1/11		0	0	0.00	1/11	
06/03/03	107328	28.19	1/11		0	0	0.00	I/II		0	0	0.00	1/11	
06/03/03	107329	27.61	1/11		0	0	0.00	1/11		0	0	0.00	1/11	
06/03/03	107330	28.18	1/11		0	0	0.00	1/11		0	0	0.00	1/11	-
06/03/03	107331 107332	28.37 28.24	1/11		0	0	0.00	1/11		0	0	0.00	I/II	-
06/03/03	107332	28.20	1/11		0	0	0.00	1/11		0	0	0.00	1/11	
06/03/03	107333	28.03	1/11		0	0	0.00	1/11		0	0	0.00	1/11	179
06/03/03	107335	28.18	1/11		0	0	0.00	1/1		0	0	0.00	I/II	
06/03/03	107336	28.03	1/11		0	0	0.00	1/11		0	0	0.00	I/II	100
06/03/03	107337	21.00	1/11		0	0	0.00	I/II		0	0	0.00	I/II	
06/04/03	107338	27.78	1/11		0	0	0.00	I/II		0	0	0.00	I/II	1
06/04/03	107339	28.15	1/11		0	0	0.00	1/11		0	0	0.00	1/11	
06/04/03	107340 107341	28.25 28.32	1/11		0	0	0.00	I/II		0	0	0.00	1/11	+
06/04/03	107341	27.89	1/11		0	0	0.00	1/11		0	0	0.00	I/II	
06/04/03	107343	27.96	1/11		0	0	0.00	I/II		0	0	0.00	1/11	
06/04/03	107344	28.50	I/II		0	0	0.00	1/11		0	0	0.00	1/11	
06/04/03	107345	28.28	1/11		0	0	0.00	I/II	0.00	0	0	0.00	1/11	
06/04/03	107346	27.27	1/11		0	0	0.00	I/II		0	0	0.00	I/II	1
06/04/03	107347	27.91	1/11		0	0	0.00	1/11		0	0	0.00	1/11	1
06/04/03	107348 107349	28.34 27.88	I/II		0	0	0.00	I/II		0	0	0.00	1/11	+
06/04/03	107349	28.34	1/11		0	0	0.00	1/11		0	0	0.00	1/11	
06/04/03	107351	28.35	1/11		0	0	0.00	1/11		0	0	0.00	1/11	
						M. Jan								
	Cement				Cement									
Monte	Per CY	Batched			Batched									
Mix No. C-4WR-C15	(lbs) 5 503	(CY) 5,782.00	ALUM L		(Tons) 1,454.17					-				
M-4	825	168.00			69.30					Total Billed	Weight (Tons)	1.555 84		
C-4WR	593	147.00			43.59	7 3 3 5	Section 1					. 10.00.01		100
0	0	0.00			0.00	100				1				
0	0	0.00			0.00					Yield =	100.7	%		
Left In			his Check (+)	- 52	1.53			1.8						
Scale (Tons		Previous Yie	* /		1.68			C.F	P.L:		1000			100
		Total Weighed	(Batch Scale)		1,566.91				No. of the last		Signature			



TRANSIT MIXER CONDITION CERTIFICATION

In accordance with requirements of Iowa Department of Transportation Standard Specifications Section 2001.21B this certifies the herein described transit mixer was examined on the date shown and was found to be in proper working condition, the fins and blades were not damaged or worn excessively, and the drum interior was free of hardened concrete buildup.

Home Base	
Owner	
Mixer Manufacturer	
Serial Number	
MMB Rating (Mixing, Cu. Yd.)	Year New
Truck Manufacturer	
Year	Color
Date	Signature

English Ready Mix Plant Book Index

Index - b

Form Description	Form #	Page
Plant Information Sheet	Plantinf	
Portland Cement Concrete Form	E820150	
PCC Plant Report	E800240	
Cement Shipments	E202	等 医(病)
Fly Ash Shipments	E203	
Aggregate Certifications (Coarse)	E204	
Aggregate Certifications (Fine)	E204	
Specific Gravities	E205	
Moistures (Pycnometer)	E206	
Mixer Data	E208	
Ready Mix Check List	E209	
Plant Site Inspection List (PCC)	E210	
Beams Made & Tested (If Applicable)	E114	
Daily Diary	Daily 3 or 4	
열레 교민하다 중 합니다. 이 경우 하다 그 이 경우		
		Property and
		ta Mari



Plant Information Sheet

Project No.:	Contract ID.:	
Prime Contractor:		7.90
Plant Type:		
Plant Location:		
Pollution Control:		
Storm Water Permit No.:		
Date Calibrate:	<u> 200</u> 40 100 100 200 200 200 200 200 200 200 20	
Ву:		
	Material Sources	
	Phone No.	Fax No.
Plant Superintendent:	<u> </u>	
Certified Plant Inspector:		
Certification No.:		
Certified Plant Inspector:		
Certification No.:		
Certified QMA Inspector:		
Certification No.:	<u> </u>	
Certified Plant Monitor:		
Certification No.:		
Certified Plant Monitor:		
Certification No.:		
Project Engineer:		
Project Manager:	I The State of the second control of the sec	
Project Inspector:		
Materials Inspector:		AND THE
Resident Auditor:	TC Aug	ditor:



Iowa Department Of Transportation Office Of Materials PORTLAND CEMENT CONCRETE

Project No.:		 	County:	
Mix No.:	P	Pounds Cement:		
1st Adjus	sted lbs. Cement:	Source:	Sp. Gr.:	
I.M. 491.17	Fly Ash:	Source:	Sp. Gr.:	
I.M. 491.14	Slag GGBFS:	Source:	Sp. Gr.:	
2nd Adjus	sted lbs. Cement:			
To	otal Cementitious			
I.M. T-203	Fine Aggregate Source:		Sp. Gr.:	
I.M. T-203	Interm. Aggregate Source:		Sp. Gr.:	
I.M. T-203	Coarse Agregate Source:		Sp. Gr.:	
Basic w/c		Water (lbs/cy) = Design w/c (wt. cement + wt	Fly Ash +Slag) =	
Max w/c		Max. Water (lbs/cy) = Design w/c (wt. cement + wt	Fly Ash +Slag) =	
Absolute Volumes				
	Cement	(lbs/cy) / (Sp. Gr. X 62.4 X 27)		-
	Fly Ash	(lbs/cy) / (Sp. Gr. X 62.4 X 27)		
	Slag	(lbs/cy) / (Sp. Gr. X 62.4 X 27)	_	2.37
	Water	(lbs/cy) / (1.00 X 62.4 X 27)	<u> </u>	
	Air			0.060
		Subtotal		
		1.000 - Subtotal	- <u>- </u>	
		Total		1.000
% FA Agg.:	Fine	Total Aggregate (1.000 - Subtotal) X % In Mix		1.000
% FA Agg.: _ % In. Agg.:				1.00
	Interm	Aggregate (1.000 - Subtotal) X % In Mix		1.000
% In. Agg.: _ % CA Agg.: _	Interm	Aggregate (1.000 - Subtotal) X % In Mix n. Aggregate (1.000 - Subtotal) X % In Mix		1.000
% In. Agg.:	Interm Coarse	Aggregate (1.000 - Subtotal) X % In Mix n. Aggregate (1.000 - Subtotal) X % In Mix e Aggregate (1.000 - Subtotal) X % In Mix		1.000
% In. Agg.: _ % CA Agg.: _	Interm Coars	Aggregate (1.000 - Subtotal) X % In Mix a. Aggregate (1.000 - Subtotal) X % In Mix e Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total	==	1.000
% In. Agg.: _ % CA Agg.: _	Fine A	Aggregate (1.000 - Subtotal) X % In Mix a. Aggregate (1.000 - Subtotal) X % In Mix e Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27	==	1.000
% In. Agg.: _ % CA Agg.: _	Fine A	Aggregate (1.000 - Subtotal) X % In Mix a. Aggregate (1.000 - Subtotal) X % In Mix e Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 ate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27	==	1.000
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Fine A	Aggregate (1.000 - Subtotal) X % In Mix a. Aggregate (1.000 - Subtotal) X % In Mix e Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 ate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27	==	1.000
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Fine A	Aggregate (1.000 - Subtotal) X % In Mix a. Aggregate (1.000 - Subtotal) X % In Mix e Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 ate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 e Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Cement (Ibs/cy) Fly Ash (Ibs/cy)	==	1.000
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Fine A	Aggregate (1.000 - Subtotal) X % In Mix a. Aggregate (1.000 - Subtotal) X % In Mix e Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 ate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 e Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Cement (Ibs/cy) Fly Ash (Ibs/cy) Slag (Ibs/cy)	==	1.000
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Fine A	Aggregate (1.000 - Subtotal) X % In Mix a. Aggregate (1.000 - Subtotal) X % In Mix e Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 ate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 e Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Cement (Ibs/cy) Fly Ash (Ibs/cy) Slag (Ibs/cy) Water (Ibs/cy)	==	1.00
% In. Agg.: _ % CA Agg.: _ Aggregate Weights	Fine A	Aggregate (1.000 - Subtotal) X % In Mix a. Aggregate (1.000 - Subtotal) X % In Mix e Aggregate (1.000 - Subtotal) X % In Mix Aggregate Total Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 ate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 e Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Cement (Ibs/cy) Fly Ash (Ibs/cy) Slag (Ibs/cy)	==	1.000

Distribution: ___ Materials, ___ TC, ___ Proj. Engr., ___ Contractor



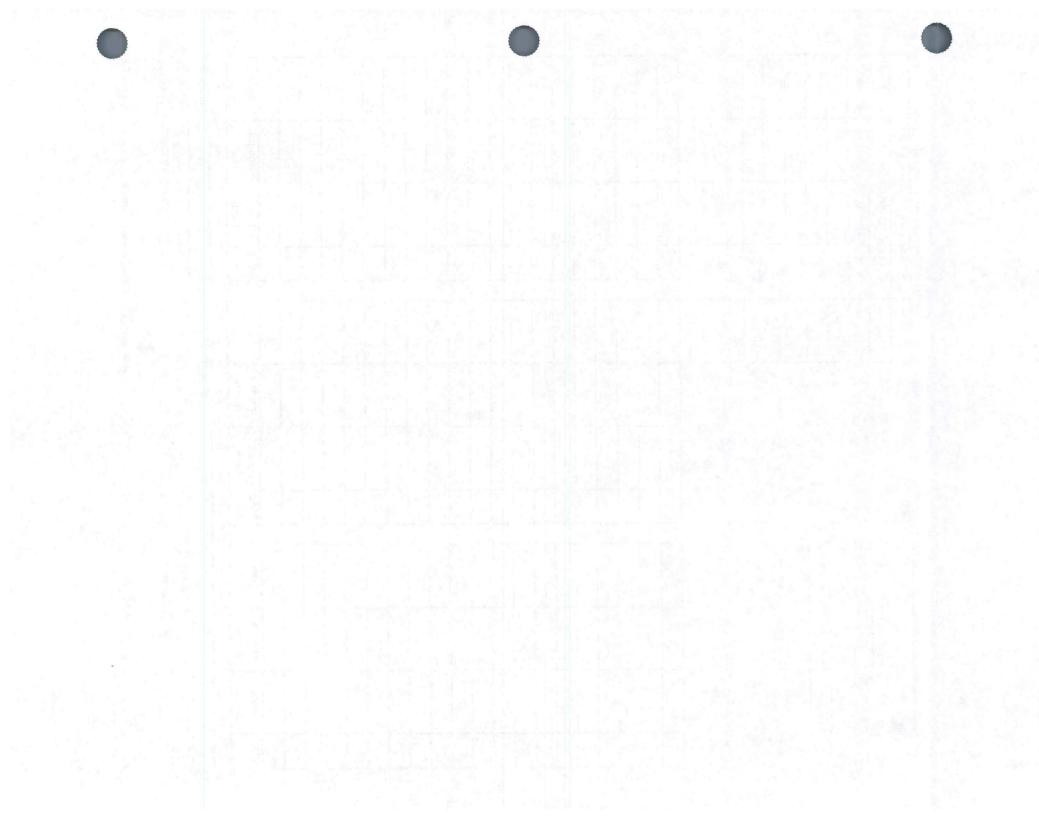
12/95 Form E820912

									Page:		
									Report No.;		
	Po	rtland Ceme	nt Shipmer	nt Yield Repo	rt			Date Su	1 14 1	11 11 11 11	
								0			
								Contractor:		1000	
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	Invoice	Billed			Invoice	Billed		F 165 187	Invoice	Billed	120
Date	Number	Tons	Туре	Date	Number	Tons	Туре	Date	Number	Tons	Туре
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	Charles and the second										
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			1	0.00							
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Left In		This Che	eck (+)	0.00				Yield =	0.00	%	
	Dravie							1 lolu =	0.00		
Scale (Tons		ished (Patch		0.00			CDI				
	I otal We	ighed (Batch	Scale)	0.00			C.P.I.:				

Contractor

TCME

Central Materials



Fly Ash Shipments

Spec. Grav.:	Page No.:
Source:	Туре:
Project No.:	Contract ID.:

.702.538	Ticket	Certified	To Date	Used	To Date		
Date	No.	(Tons)	(Tons)	(Tons)	(Tons)	Remarks	Ву
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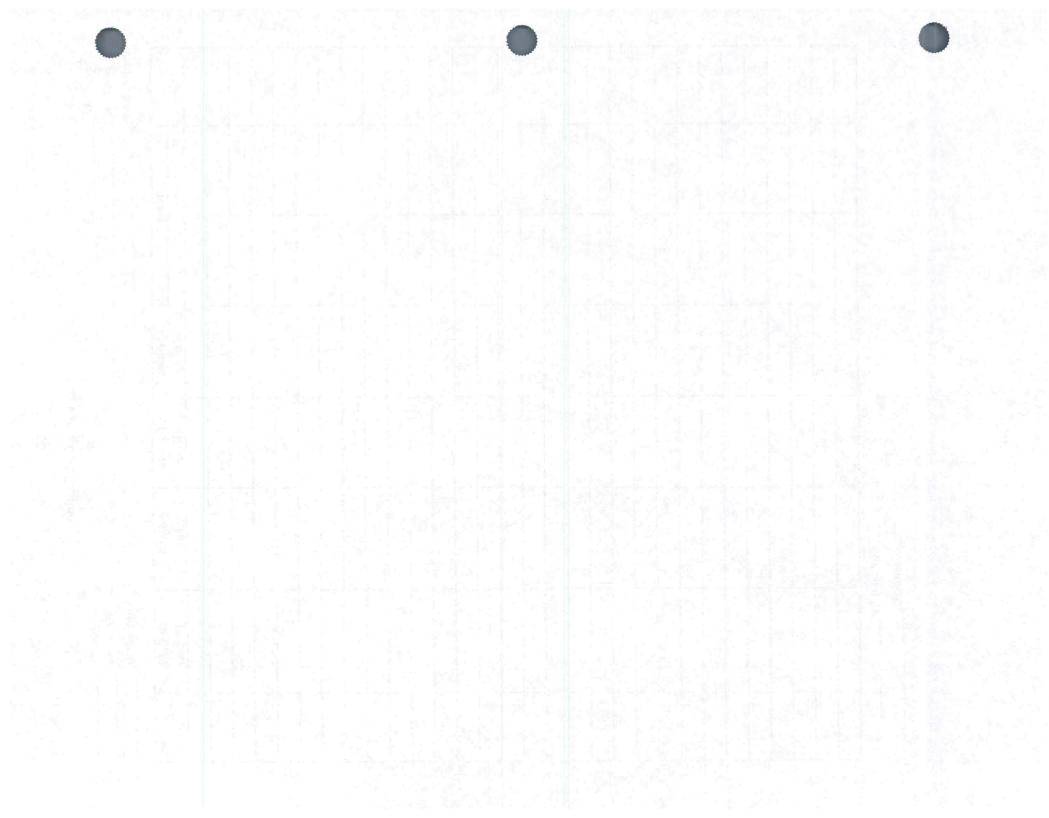
Checked By:	A THE PERSON NAMED IN
Audited By:	

Aggregate Certification

00 0	
Page No.:	
Grad. No.:	<u> </u>
Contract ID.:	
	Page No.: Grad. No.:

	Ticket	#	Certified	To Date	Used	To Date	
Date	From	То	(Tons)	(Tons)	(Tons)	(Tons)	Ву
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Checked By:	
Audited By:	



	Page No.:
Project No.:	Contract ID.:

Date	Aggregate Type	S (Grams)	P (Grams)	S+P (Grams)	W (Grams)	Actual Sp. Gr.	T-203 Sp. Gr.	D.
Date	Type	(Grams)	(Grams)	(Grams)	(Grains)	эр. Gг.	эр. Gг.	Ву
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Audited By:	

Specific Gravity=S \ (S+P-W)

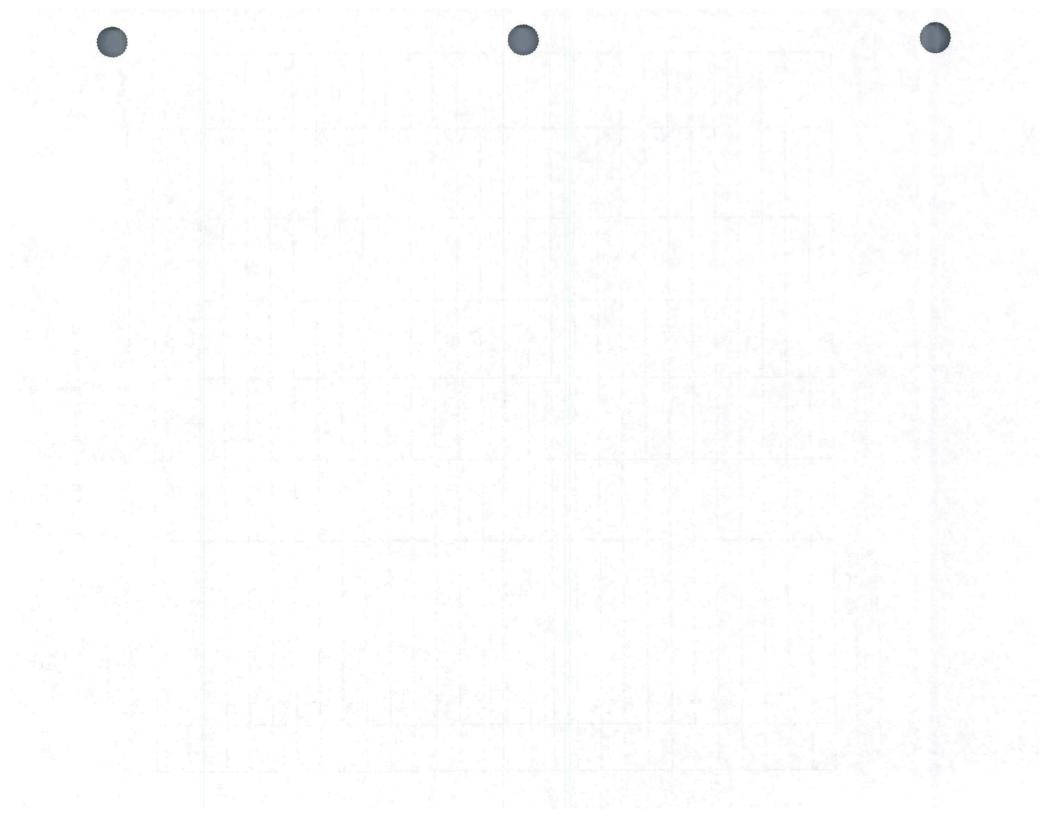


Moistures by Pycnometer (IM 308)

		Page No.:
Project No.:	<u>. 4</u>	Contract ID.:

	Aggregate	W	W1	Diff.	Moisture		
Date	Туре	(Grams)	(Grams)	(Grams)	(%)	Remarks	Ву
9 13	4 F J 19 18 17		FIRE A	Yan A			
	FT TELES		19 No. 20 T. 19 No.	SERVE T	ROLL TO		5.715.70
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April 19	Marie Carlo	1991. 8	44194.53	9 48 300			F 7 7 2 3
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17-16-7			53.57.78				
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		APPLY		The total			Se la se
1				3-45-93	1. The A. 10 T.		
							7

Checked By:	1
Audited By:	



Daily Plant Check List

	Page No.:
Project No.:	Contract ID.:

	Stock	Scale	ale Mixing Mixir		Placed	Cem De	elivery	Fly Ash	Delivery	Agg. D	elivery	Plant	Admix.	
Date	Piles	Sens.	Speed	Time	Time	AM	РМ	AM	PM	AM	PM	Site	Dispens.	В
refugi			356.50	C. P.		Walth	W. T.		2		186-19		- 35	
	0.4				Don	130					18			
A TO														1
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	75				E MIT	1.5	FIFE			100	1.47	HE EVE	1757.3	T

Com	p	lies	= Y

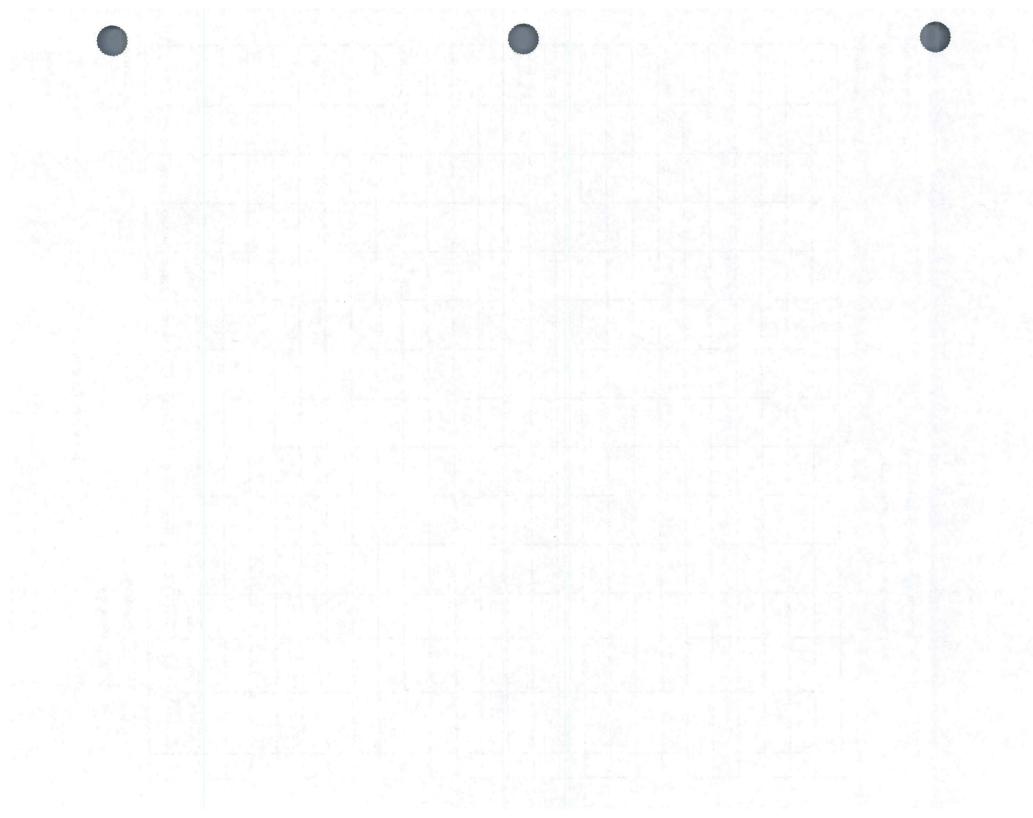
Discrepancy = D

Not Applicable = NA

Record Actual Mixing Time & Placed Time

Form E212

Refer to Daily Diary For Discrepancies

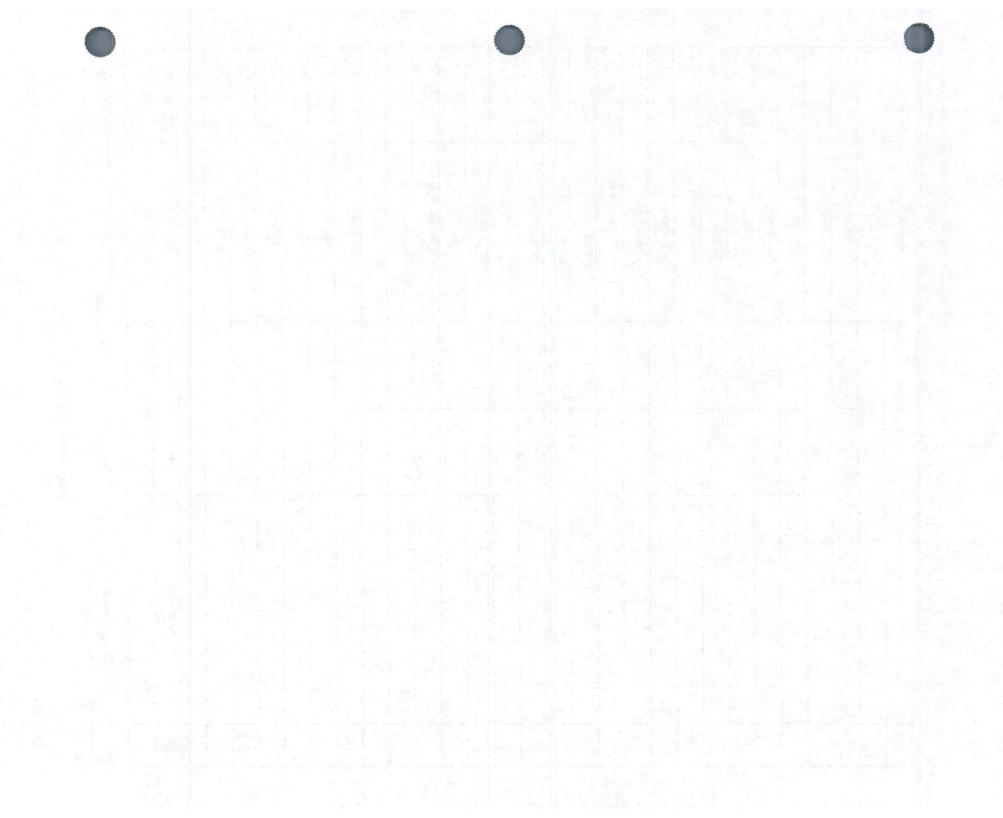


Plant Site Inspection List (PCC)

	Page No.:
roject No.:	Contract ID.:

Date		Com	plies		
Checked	Item	Yes	No	Remarks	Ву
	Bins				
2 2 7 24	Bin Dividers				The state of the s
	Bin Supports				
	Screens				
	Guards				
	Ladders				
	Railings				100
	Belt Lockouts				
	Sampling Location				
	Aggregate Scales				
	Cement Scales				
	Fly Ash Scales				
	Admixture Dispensers				
	Water Meter				
	Cement Storage				
	Fly Ash Storage				
	Mixing Equipment				
	Lab Location				
	Lab Condition				
	Lab Equipment				
	Air Condition				1.0
	Heating	1.70			
	Telephone		5		
	Water				
	Exhaust Fan				
15 20	Restroom				
	Fax Machine				40
	Computer		THE PERSON NAMED IN		

If an item does not apply to the project, write (not applicable) in the remarks column.







Line No.:	
Item Code:	Page No.:
Description:	Category No.:
Project No.:	Contract ID:

Beams Made Information						Beam Break Information								3		
Date Made	Mix Number	Beam No.	Time	Air %	Slump (in)	W/C Ratio	Age (Days)	Loc.	Depth (in)	Width (in)	Indicated Load (lbs)	Actual Load (lbs)	Comp. Factor	Mod. Of Rupture (psi)	Spec.	В
						728						1	0.000000	0		
										1 1 1 1			0.000000	0	7	
			HY Ch						4				0.000000	0		4
									5224				0.000000	0		
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9-63					330								0.000000	0		
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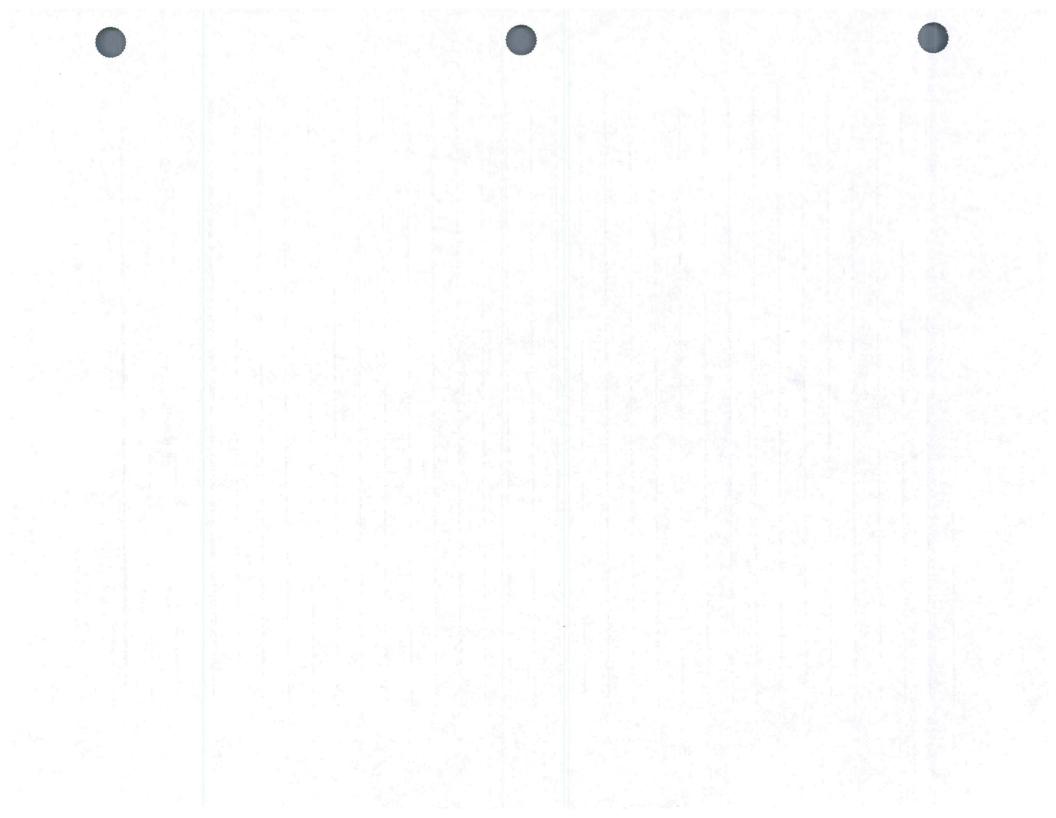
Checked	By:			



Rev 1/97 Daily3

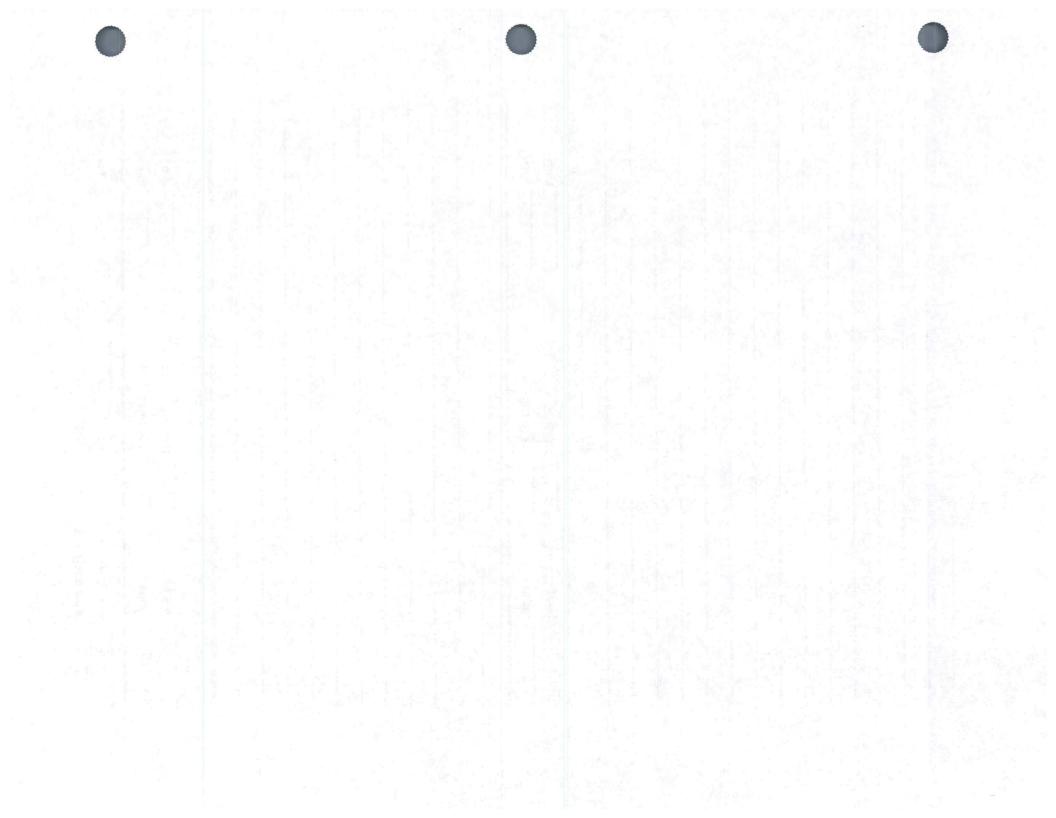
Page No.:

Project No.:		Contract ID:
Date:	Sunrise:	High:
Day:	Sunset:	
Weather:		
		The second second
37.9 S 34 W		
	By:	



Rev 1/97 Diary 4

roject No.:		Contract ID:
Date: Day: Weather:	Sunrise: Sunset:	
		By:
Date:	Sunrise:	
Weather:		
	Ву	



English PCC Paving Plant book Index

Item Description	Form #	Page
Plant Information Sheet	Plantinf	
Portland Cement Concrete Form	E820150	
PCC Plant Report	E800240	
Portland Cement Shipment Yield Report	E820912	
Fly Ash Shipments	E203	
Aggregate Certifications (Coarse)	E204	
Aggregate Certifications (Fine)	E204	
Specific Gravities	E205	
Moistures (Pycnometer)	E206	
Daily Plant Check List	E212	
Plant Site Inspection List (PCC)	E210	
Beams Made & Tested	E114	
Daily Diary	Daily 3 or 4	

Plant Information Sheet

Project No.:	Contract ID.:	
Prime Contractor:		
Plant Type:		
Plant Location:		
Pollution Control:		
Storm Water Permit No.:		
Date Calibrate:		
Ву:		
	Material Sources	
	<u> 1812</u> 현실은 전기를 되었다. 12 시간 12 12 12 12 12 12 12 12 12 12 12 12 12	
시간 생물이 가장한 사람이 되고 있었다. 경기를 받았다.		
	Phone No.	Fax No.
Plant Superintendent:		
certified Plant Inspector:		
Certification No.:		
Certified Plant Inspector:		
Certification No.:		
Certified QMA Inspector:		
Certification No.:		
Certified Plant Monitor:		
Certification No.:		
Certified Plant Monitor:	<u> </u>	
Certification No.:		A THOUGH A SECTION
Project Engineer:		
Project Manager:		
Materials Inspector:		
Resident Auditor:	TC Audito	or:



Iowa Department Of Transportation Office Of Materials PORTLAND CEMENT CONCRETE

1st Adjusted lbs. Ce I.M. 491.17 Fly I.M. 491.14 Slag Go 2nd Adjusted lbs. Ce Total Cement I.M. T-203 Fine Ag I.M. T-203 Interm. A I.M. T-203 Coarse Basic w/c Max w/c Absolute Volumes	Ash: Source: GBFS: Source: ement: ggregate Source: Aggregate Source: Aggregate Source: Water (lbs/cy) Max. Water (lbs/cy) ement	= Design w/c (wt. cement + wt Fi = Design w/c (wt. cement + wt Fi bs/cy) / (Sp. Gr. X 62.4 X 27) bs/cy) / (Sp. Gr. X 62.4 X 27) bs/cy) / (Sp. Gr. X 62.4 X 27)		
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C	ily Ash(Il	bs/cy) / (Sp. Gr. X 62.4 X 27)		
F			• _	
	Slag(I	bs/cy) / (Sp. Gr. X 62.4 X 27)		
			7. F	
	Water (I	bs/cy) / (1.00 X 62.4 X 27)	<u> </u>	
	Air			0.060
		Subtotal	- <u> </u>	5 7 7
		1.000 - Subtotal	:20 ± <u>20</u>	
		Total	=	1.000
% FA Agg.:	Fine Aggregate (1.000 - S	Subtotal) X % In Mix		
% In. Agg.:	Interm. Aggregate (1.000 -			
% CA Agg.:	Coarse Aggregate (1.000 -			
aggregate Weights		Aggregate Total	<u></u>	
ggregate weights	Fine Aggregate (abs vol.)	X Sp. Gr. X 62.4 X 27	• <u> </u>	
	Intermediate Aggregate (abs	vol.) X Sp. Gr. X 62.4 X 27		11 4
	Coarse Aggregate (abs vol.	.) X Sp. Gr. X 62.4 X 27	<u></u>	
Summary	Cement _	(lbs/cy)		
	Fly Ash	(lbs/cy)		
	Slag_ Water	(lbs/cy)		
	Water _ Fine Agg.	(lbs/cy)		
		(lbs/cy)		
	Interm. Agg Coarse Agg.	(lbs/cy) (lbs/cy)		

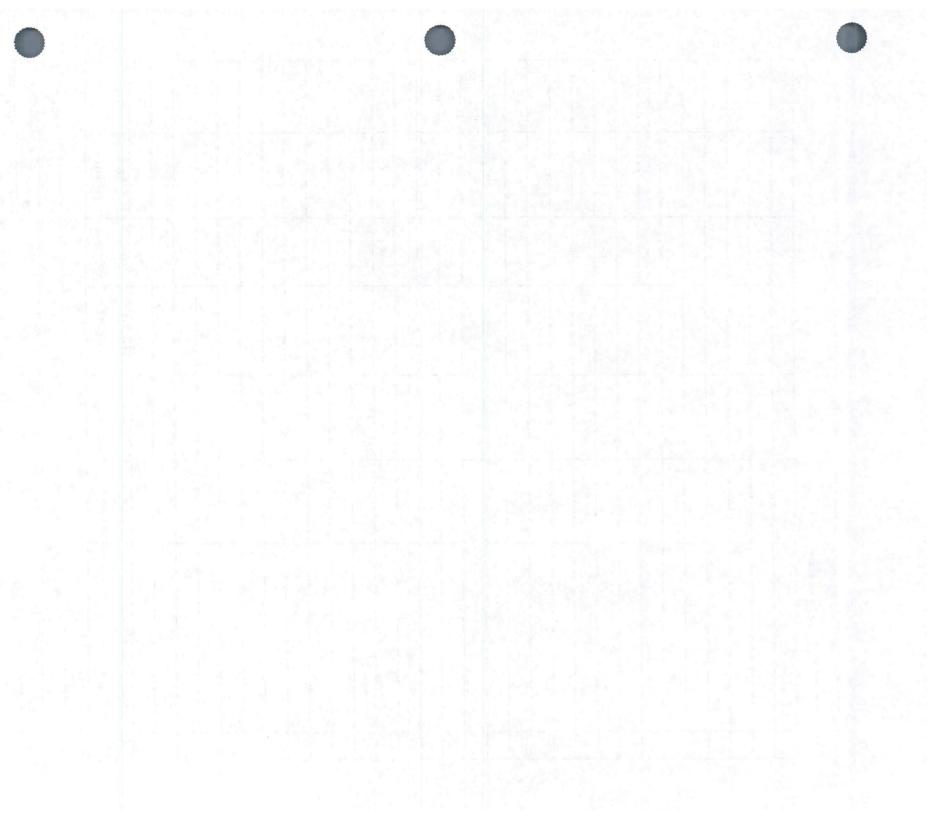


Cement Shipments

Spec. Grav.:	Page No.:
Source:	Туре:
Project No.:	Contract ID.:

Date	Ticket No.	Certified (Tons)	To Date (Tons)	Used (Tons)	To Date (Tons)	Remarks	Ву
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Audited By:	

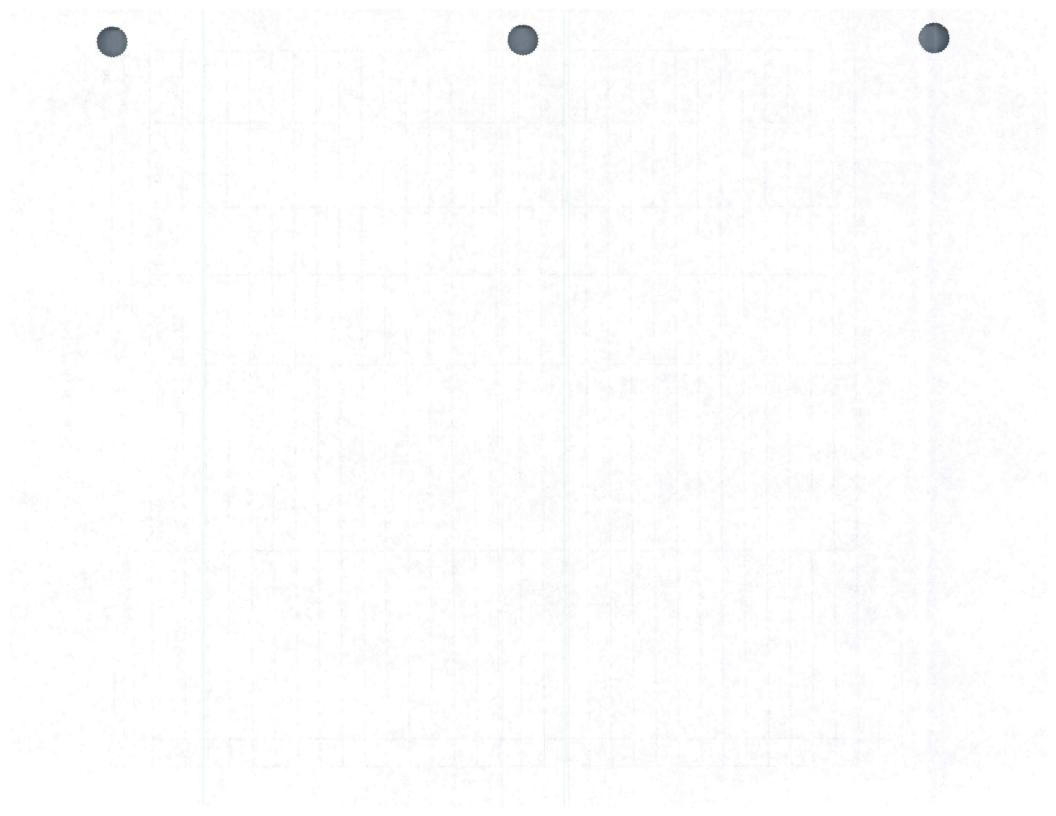


Fly Ash Shipments

Spec. Grav.:	Page No.:
Source:	Type:
Project No.:	Contract ID.:

	Ticket	Certified	To Date	Used	To Date		
Date	No.	(Tons)	(Tons)	(Tons)	(Tons)	Remarks	В
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Audited By:	



Aggregate Certification

Spec. Grav.:		Page No.:	1407
Source:		Grad. No.:	E.
Project No.:	<u> </u>	Contract ID.:	200

	Ticket	t #	Certified	To Date	Used	To Date	
Date	From	То	(Tons)	(Tons)	(Tons)	(Tons)	Ву
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Checked By:	
Audited By:	



Page No.:

-3-6	Aggregate	S	Р	S+P	W	Actual	T-203	
Date	Туре	(Grams)	(Grams)	(Grams)	(Grams)	Sp. Gr.	Sp. Gr.	Ву
32.10					Marie San	100	in the said	
			7 7 4					
Charles III						<u> </u>		
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								13.15
								100
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						Checked By	/:	Val.



Moistures by Pycnometer (IM 308)

	Page No.:
Project No.:	Contract ID.:

Date	Aggregate Type	W (Grams)	W1 (Grams)	Diff. (Grams)	Moisture (%)	Remarks	Ву
							11 15.5
					Carlo State		3
			Be Tale				
							AND S
							10
		U ST SWA STORE					4
		761					200
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					W. 10.13		
			1 10 10 10				4 127
17/14			-117	139			
							3 75 74
		of Tyle					
		AND THE RESERVE		W. Divine			
		34 15	E/Carrie	A THE RE			

Checked By:	
Audited By:	

Rev 01/98 Form E208

Mixer Data

	Page No.:
roject No.:	Contract ID.:

Truck		Date	Mixer	Mixing Capacity	Mixing	g Speed	Agit.	Rev. Counter	
Date No.	Certified	Brand	(CY)	Rated	Actual	Speed	(man/auto)	Ву	
	THUR L								
K-1 14									
			AR SUMMER						
		E partie to		100			N C		
1 499 - 59									
									-
							5-07		
							Section 2		
	Ballion II						No.		199
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1.50	April 1	West N				100			
	A PLAN		C. S. F.						
			P. 20. 3						
						Property of			
	95,7340	-							
	Carrier Service		2000						
ASSET SERVICE					Side No.		Contract.	EL CALLED	
	300							100	
	2000		A TOTAL		196, 136				1



Rev 01/98

Ready Mix Check List

Form E209

	Page No.:
Project No.:	Contract ID.:

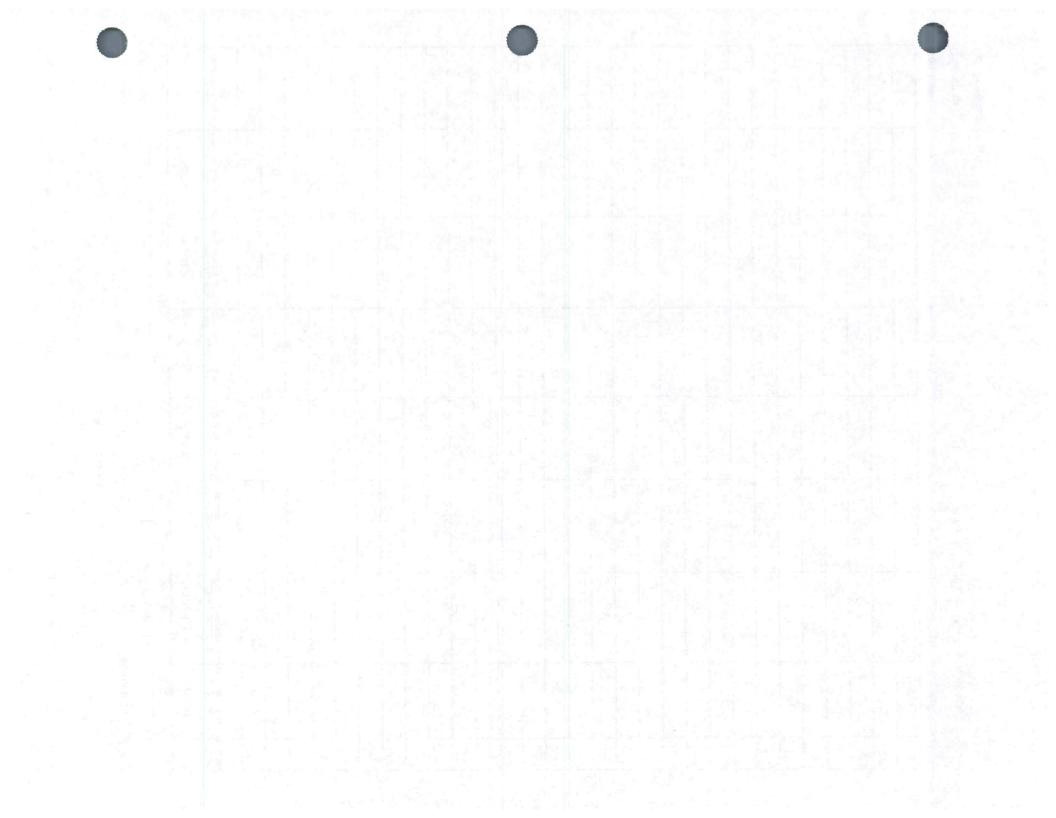
Date	Scale Sensitivity	Scale Operations	Mixing Revolutions	Mixing Time	Stockpiles	Admixture Dispensers	Plant Site	Pv
Date	Sensitivity	Operations	Revolutions	Tille	Otockpiles	Dispensers	Site	Ву
						2.3-2.4		
							M (1997)	
					F1390			13.1
						A45.50		- 10
						No. 1	Se mari	
								See See
						DESTRUCTION ROLL		
								13.7
	1						35734) AT
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			945 10 10 10					
Mark the					Per Tales		E DEVIN	
20114				76.5K			1.00	
								-
STATE OF STREET								
								No.

complies = Y

Discrepancy = D

Not Applicable = NA

Refer to Daily Diary for Discrepancies



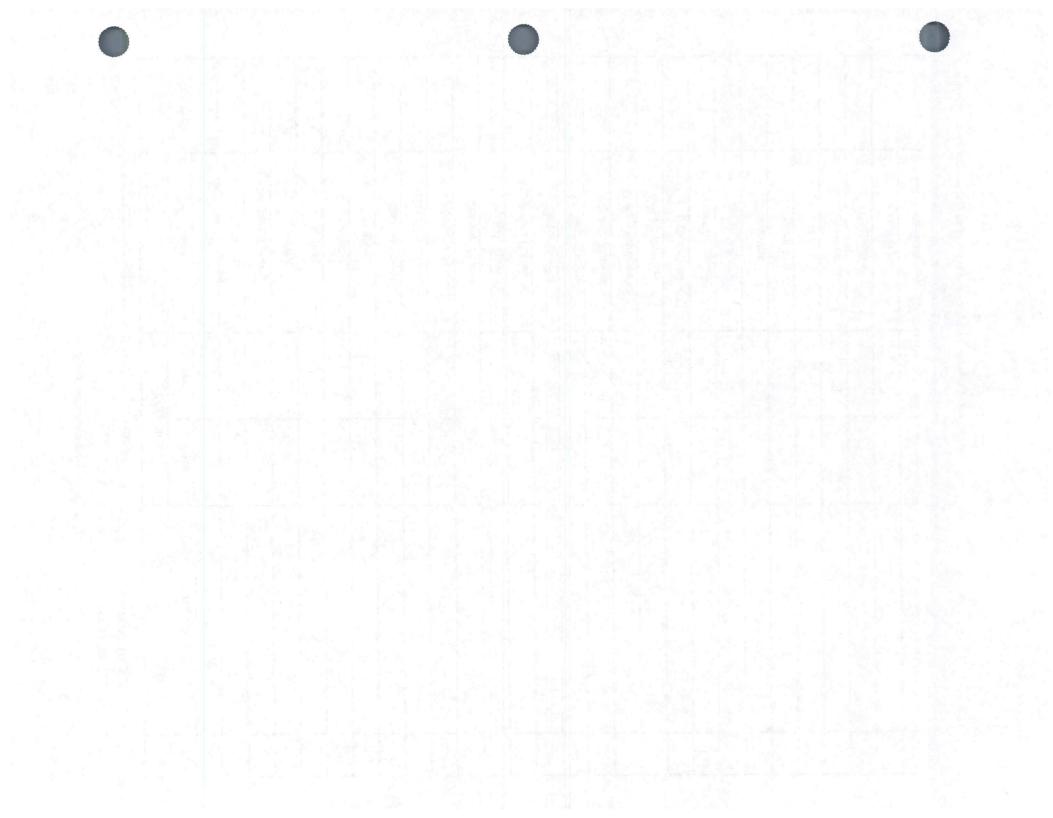
Project No.:_

Plant Site Inspection List (PCC)

	Page No.:
<u> - 이 시간 중요하다 이 바</u> 라면서 하는 것은	Contract ID.:

Date		Com	plies		1
Checked	Item	Yes	No	Remarks	Ву
	Bins				
	Bin Dividers				
	Bin Supports				
	Screens	Part and a			
	Guards				
	Ladders				
	Railings				
	Belt Lockouts				. A 18 11
	Sampling Location				
	Aggregate Scales				
	Cement Scales				114 3
	Fly Ash Scales		May 1		
	Admixture Dispensers				
	Water Meter				
	Cement Storage				
5.75	Fly Ash Storage				
	Mixing Equipment				
	Lab Location				
	Lab Condition				
	Lab Equipment				
	Air Condition				
	Heating				
	Telephone				
	Water				
	Exhaust Fan				
	Restroom	and the second		e A to the state of	
Sec.	Fax Machine	La A A N	Carrier Services		
	Computer				

If an item does not apply to the project, write (not applicable) in the remarks column.



Rev 09/01

PC Concrete Beam Record

Form	F 4	4

Line No.:	
Item Code:	Page No.:
Description:	Category No.:
Project No.:	Contract ID:

Beams Made Information						Beam Break Information								10, 1		
Date Made	Mix Number	Beam No.	Time	Air %	Slump (in)	W/C Ratio	Age (Days)	Loc. (in)	Depth (in)	Width (in)	Indicated Load (lbs)	Actual Load (lbs)	Comp. Factor	Mod. Of Rupture (psi)		Ву
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							in man			1782			0.000000	0		100
													0.000000	0		
				34.3			W 49						0.000000	0		
			The state of										0.000000	0		
											A1.3.79		0.000000	0		
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Checked By:	
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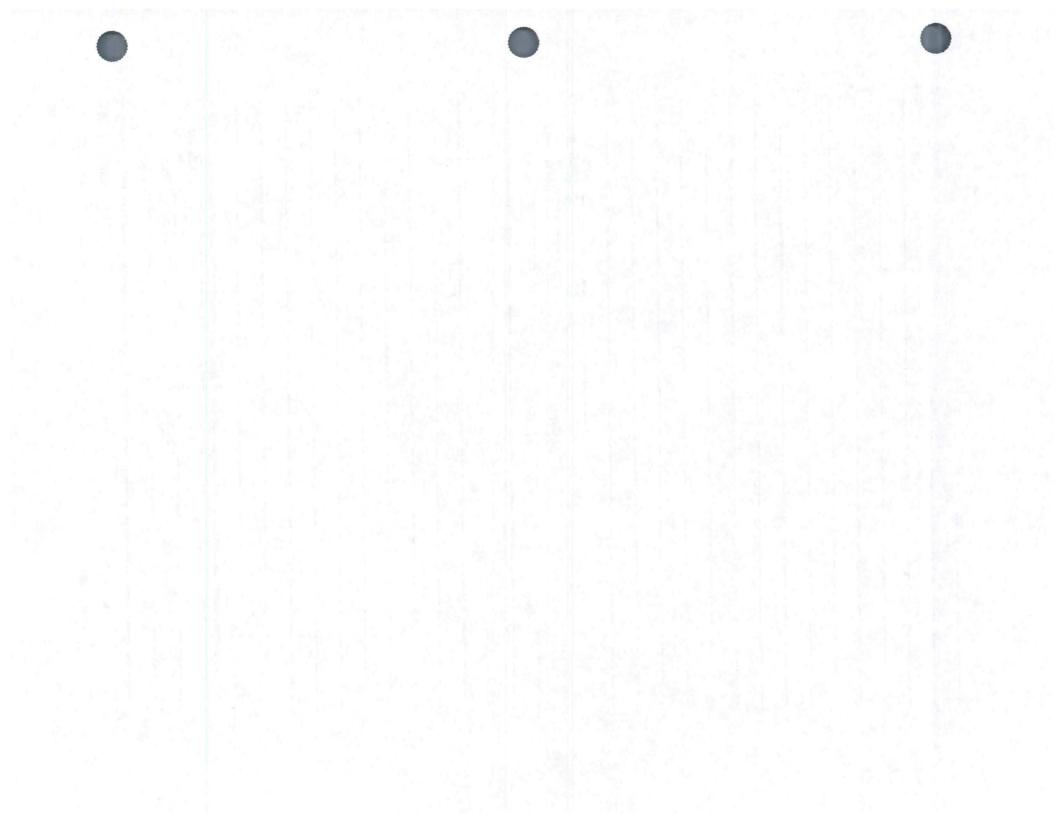
Rev 1/97 Daily3

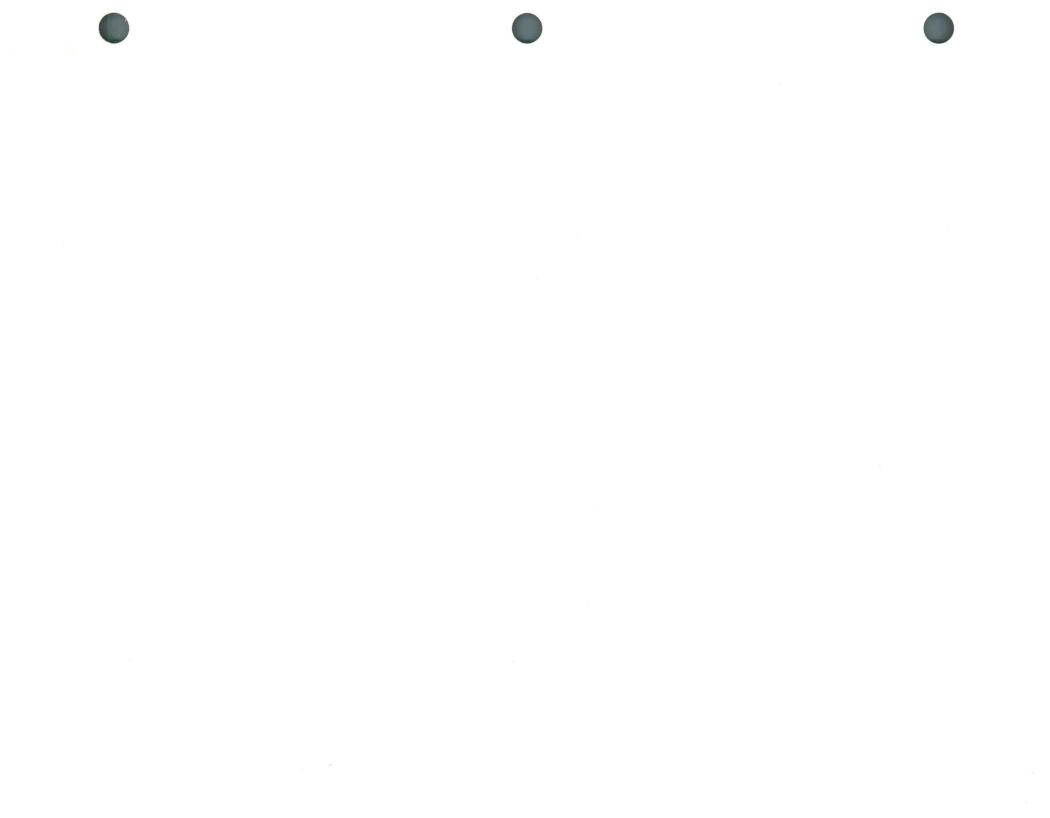
		Page No.:
Project No.:		Contract ID:
Date:	Sunrise:	High:
Day:	Sunset:	Low:
Weather:		
	A CONTRACTOR	
		Control Victoria (1980)
		211

Rev 1/97

Page No.:

roject No.:		Contract ID:			
Date:	Sunrise:	High:			
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Weather:					
		Ву:			
Date:	Sunrise:	High:			
Day:	Sunset:				
Weather:					
	By:	A TORRING TO SE			







PART A

 Absolute Volume
 Dry Batch Masses

 Cement
 0.093 yd^3 x
 $27 \text{ ft}^3/\text{yd}^3$ x
 3.14 x $62.4 \text{ lb/ft}^3 = 492 \text{ lb}$

 Fine Agg.
 0.345 yd^3 x
 $27 \text{ ft}^3/\text{yd}^3$ x
 2.66 x $62.4 \text{ lb/ft}^3 = 1546 \text{ lb SSD}$

 Coarse Agg.
 0.345 yd^3 x
 $27 \text{ ft}^3/\text{yd}^3$ x
 2.68 x $62.4 \text{ lb/ft}^3 = 1558 \text{ lb SSD}$

 Water
 0.157 yd^3 x
 $27 \text{ ft}^3/\text{yd}^3$ x
 1.00 x $62.4 \text{ lb/ft}^3 = 265 \text{ lb}$

PART B

Fine Aggregate Moisture

1.000 1546 lb = 1595 lb

<u>- 0.031</u> 0.969

0.969

1595 lb - 1546 lb = **49 lb excess water**

Coarse Aggregate Moisture

1.000 1558 lb = 1563 lb

-0.003 0.997

0.997

1563 lb - 1558 lb = 5 lb excess water

Total Free Water = 54 lb

Correct basic water to be batched or added as mixing water.

As before, total free water contributed by aggregate is

49 lb water
$$+$$
 5 lb water $=$ 54 lb

Conversion to gallons

$$211 \text{ lb/yd}^3 / 8.33 \text{ lb/gal} = 25 \text{ gal/yd}^3 \text{ of mix water}$$

Maximum water that can be added to the batch

From I.M. 529

w/c = 0.600 lb/lb

Cement
$$x = 0.600 = water$$

492 lb
$$\times$$
 0.600 = 295 lb maximum water per yd³

241 lb /
$$8.33 \text{ lb/gal} = 29 \text{ gal/yd}^3$$

Maximum allowable water that may be added as mixing water.

Solution #2

Form E820150E

Iowa Department Of Transportation Office Of Materials PORTLAND CEMENT CONCRETE

Project No.: 5	STP 27-3980-31	25.48				County : C	Clayton
Mix No.:	C-4-C15	P	ounds Cement:	624			
1st Adju	sted lbs. Cement:	530	Source:	Continental 1		Sp. Gr.:	3.14
IM 491.17	Fly Ash:	94	Source:	Louisa Gene	rating	Sp. Gr.:	2.68
IM 491.14	Slag GGBFS:		Source:			Sp. Gr.:	354
2nd Adju	sted lbs. Cement:	530					
Т	otal Cementitious	624					
IM T203	Fine Aggregate	Source:	Roverud			Sp. Gr.:	2.66
IM T203	Interm. Aggregate	Source:			1 7 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Sp. Gr.:	
IM T203	Coarse Agregate	Source:	Gisleson Quarr	у		Sp. Gr.:	2.66
Basic w/c	0.430		Water (lbs	/cy) = Design	w/c (wt. cement + wt	Fly Ash +Slag) =	268
Max w/c	0.488		Max. Water (lbs	/cy) = Design	w/c (wt. cement + wt	Fly Ash +Slag) = _	305
Absolute Volumes	Cement			(lbs/cy) / (Sp	o. Gr. X 62.4 X 27)	-	0.100
	Fly Ash			(lbs/cy) / (Sp	o. Gr. X 62.4 X 27)	= -	0.021
	Slag			(lbs/cy) / (Sp	p. Gr. X 62.4 X 27)		
	Water			(lbs/cy) / (1.	00 X 62.4 X 27)	=	0.159
	Air						0.060
					Subtotal	_	0.340
				Life y Sales	1.000 - Subtotal		0.660
					Total		1.000
% FA Agg.:	50	Fine	Aggregate (1.000	- Subtotal) X	% In Mix		0.330
% In. Agg.:			Aggregate (1.00			•	1000
% CA Agg.:	50		Aggregate (1.00			=	0.330
					gate Total		0.660
Aggregate Weights		Fine A	ggregate (abs vo	ol.) X Sp. Gr. X	62.4 X 27	=.	1479
		Intermedia	te Aggregate (ab	s vol.) X Sp. G	Gr. X 62.4 X 27	•	Protein.
		Coarse	Aggregate (abs v	ol.) X Sp. Gr.	X 62.4 X 27		1479
Summary			Cemen	t 530	(lbs/cy)		
			Fly Ash		(lbs/cy)		
			Sla		(lbs/cy)		
			Water		(lbs/cy)		
			Fine Agg		(lbs/cy)		
					/		
			Interm. Agg Coarse Agg 10-3		(lbs/cy)		

Iowa Department Of Transportation So Office Of Materials PORTLAND CEMENT CONCRETE

Solution #2

Form E820150E

Project No.: S	TP 27-3980-31			County : C	layton
Mix No.: _	C-4	Pounds Cement:624			
1st Adius	sted lbs. Cement:624	Source: Contine	ntal 1	Sp. Gr.:	3.14
IM 491.17	Fly Ash:	Source:		Sp. Gr.:	2.68
IM 491.14	Slag GGBFS:	Source:		Sp. Gr.:	n de la company
2nd Adjus	sted lbs. Cement: 624				
To	otal Cementitious 624				
IM T203	Fine Aggregate Source:	Roverud		Sp. Gr.:	2.66
IM T203	Interm. Aggregate Source				A THE THE
IM T203	Coarse Agregate Source			Sp. Gr.:	
Basic w/c _	0.430	Water (lbs/cv) = Des	sign w/c (wt. cement + wt F	ly Ash +Slag) =	268
	0.488		sign w/c (wt. cement + wt F		
wax w/c_	0.466	Max. Water (IDS/Cy) - Des	sign w/c (wt. cement + wt)	ly Asii +Slag) =	303
Absolute Volumes	Cement	(lbs/cy)	/ (Sp. Gr. X 62.4 X 27)	_	0.118
	Fly Ash	(lbs/cy)	/ (Sp. Gr. X 62.4 X 27)		
	Slag	(lbs/cy)	/ (Sp. Gr. X 62.4 X 27)		
	Water	(lbs/cy)	/ (1.00 X 62.4 X 27)	-	0.159
	Air				0.060
			Subtotal		0.337
			1.000 - Subtotal		0.663
			Total	The state of the s	1.000
% FA Agg.: _	50 Fin	e Aggregate (1.000 - Subtotal) X % In Mix		0.331
% In. Agg.:	Inter	m. Aggregate (1.000 - Subtota	al) X % In Mix		
% CA Agg.: _		se Aggregate (1.000 - Subtota	al) X % In Mix	**************************************	0.332
		Ag	gregate Total		0.663
Aggregate Weights	Fine	Aggregate (abs vol.) X Sp. G	Gr. X 62.4 X 27		1483
	Intermed	iate Aggregate (abs vol.) X S	Sp. Gr. X 62.4 X 27		
	Coars	e Aggregate (abs vol.) X Sp.	Gr X 62 4 X 27		1488
	Court	A second			
Summary		Cement			
		Fly Ash			
		Slag			
		Water			
		Fine Agg14			
		Interm. Agg			
		10-4 Coarse Agg14	488 (lbs/cy)		
Distribution: Materials DM	F Proj Engr Contractor	10-7			

Proportion and Problem Solving

PART A

 Absolute Volume
 Dry Batch Masses

 Cement
 $0.104 \text{ yd}^3 \text{ x}$ 3.14 x $62.4 \text{ lb/ft}^3 \text{ x}$ $27 \text{ ft}^3/\text{yd}^3 =$ 550 lb

 Fine Agg.
 $0.306 \text{ yd}^3 \text{ x}$ 2.66 x $62.4 \text{ lb/ft}^3 \text{ x}$ $27 \text{ ft}^3/\text{yd}^3 =$ 1371 lb SSD

 Coarse Agg.
 $0.375 \text{ yd}^3 \text{ x}$ 2.68 x $62.4 \text{ lb/ft}^3 \text{ x}$ $27 \text{ ft}^3/\text{yd}^3 =$ 1693 lb SSD

 Water
 $0.155 \text{ yd}^3 \text{ x}$ 1.00 x $62.4 \text{ lb/ft}^3 \text{ x}$ $27 \text{ ft}^3/\text{yd}^3 =$ 261 lb

PART B

Fine Aggregate Moisture

1.000 $\underline{1371} = 1419 \text{ lb}$

<u>-0.034</u> 0.966

0.966

1419 lb - 1371 lb = **48 lb excess water**

Coarse Aggregate Moisture

1.000 $\underline{1693} = 1702 \text{ lb}$

-0.005 0.995

0.995

1702 lb - 1693 lb = **9 lb excess water**

Total free water: 48 lb + 9 lb = 57 lb

Basic - Agg. = Corrected

261 lb - 57 lb = 204 lb water

 $204 \text{ lb/yd} \div 8.33 \text{ lb/gal} = 24 \text{ gal/yd}^3$

Maximum allowable mixing water

 $0.532 \text{ lb/lb} \quad x \quad 550 \text{ lb} = 293 \text{ lb}$

293 lb - 57 lb = **236 lb**

236 lb \div 8.33 lb/gal = **28 gal**

- 1. Maximum w/c = 0.488 Maximum Water = 0.488 x 624 lb = 305 lb/yd^3 $305 \text{ lb/yd}^3 \div 8.33 \text{ lb/gal} = 37 \text{ gal/yd}^3$ Water Allowed = $37 \times 5 = 185 \text{ gal}$
- 2. Maximum w/c = 0.450 Maximum Water = 0.450 x 709 lb = 319 lb/yd^3 $319 \text{ lb/yd}^3 \div 8.33 \text{ lb/gal} = 38 \text{ gal/yd}^3$ Water Allowed = $38 \times 7 = 266 \text{ gal}$
- 3. Total Water = $(5 \text{ gal/yd}^3 \times 8.33 \text{ lb/gal}) + (27 \text{ gal/yd}^3 \times 8.33 \text{ lb/gal})$ = 42 lb + 225 lb= 267 lbw/c = $267 \div 603$ = 0.443
- 4. Total Water = $50 \text{ lb/yd}^3 + (30 \text{ gal/yd}^3 \times 8.33 \text{ lb/gal})$ = $50 \text{ lb/yd}^3 + 250 \text{ lb/yd}^3$ = 300 lb/yd^3 Total Cement = $529 \text{ lb/yd}^3 + 95 \text{ lb/yd}^3$ = 624 lb/yd^3 w/c = $300 \text{ lb/yd}^3 \div 624 \text{ lb/yd}^3$ = 0.481

5. Maximum w/c = 0.489

Maximum Water =
$$0.489 \times 593 \text{ lb/yd}^3 = 290.0 \text{ lb/yd}^3$$

= 35 gal/yd^3

Water Allowed =
$$35 \text{ gal/yd}^3 \times 7 \text{ yd}^3 = 245 \text{ gal}$$

Total Water =
$$48 \text{ lb/yd}^3 + (24 \text{ gal/yd}^3 \times 8.33 \text{ lb/gal}) =$$

$$= 30 \text{ gal/yd}^3$$

$$30 \text{ gal/yd}^3 \times 7 \text{ yd}^3 = 210 \text{ gal}$$

 $48 \text{ lb/yd}^3 + 200 \text{ lb/yd}^3 = 248 \text{ lb/yd}^3$

Amount of water that can be added at the paver:

1. Dry Batch Masses

Cement

 $0.156 \times 3.14 \times 27 \times 62.4 = 825 lb$

Fine Aggregate

0.311 x 2.67 x 27 x 62.4 = 1399 lb

Coarse Aggregate

 $0.312 \times 2.65 \times 27 \times 62.4 = 1393 lb$

Basic Water

 $0.161 \times 1.00 \times 27 \times 62.4 = 271 \text{ lb or } 33 \text{ gal}$

Actual Batch Masses

Fine Aggregate: $1399 \div (1-0.028) = 1439 \text{ lb}$

Coarse Aggregate: $1393 \div (1-0.006) = 1401 \text{ lb}$

2. Total Water

Water in the Materials

Fine Aggregate: 1439 - 1399 = 40 lb

Coarse Aggregate: 1401 - 1393 = 8 lb

Water added at the plant: $30 \times 8.33 = 250 \text{ lb}$

Water added at the grade: $(10 \div 7) \times 8.33 = 12 \text{ lb}$

310 lb

3. Water/Cement Ratio

 $310 \div 825 = 0.376$

1. Dry Batch Masses

Cement

$$0.108 \times 3.14 \times 27 \times 62.4 = 571 \text{ lb}$$

Fine Aggregate

$$0.309 \times 2.66 \times 27 \times 62.4 = 1385 lb$$

Coarse Aggregate

$$0.377 \times 2.60 \times 27 \times 62.4 = 1651 \text{ lb}$$

Basic Water

$$0.146 \times 1.00 \times 27 \times 62.4 = 246 \text{ lb or } 30 \text{ gal}$$

Actual Batch Masses

Fine Aggregate

$$1385 \div (1 - 0.030) = 1428 lb$$

Coarse Aggregate

$$1651 \div (1 - 0.005) = 1659 \text{ lb}$$

2. Total Water

Water in the Materials Fine Aggregate: 1428 - 1385 = 43 lb

Coarse Aggregate: 1659 - 1651 = 8 lb

Water Added at the Plant

$$23 \times 8.33 = 192 lb$$

Water Added at the Grade

$$(15 \div 7) \times 8.33 = 18 \text{ lb}$$

Total Water

$$192 + 18 + 43 + 8 =$$
261 lb

3. W/C

$$261 \div 571 = .457$$

Office Of Materials PORTLAND CEMENT CONCRETE

r roject No				oounty	
Mix No :	B-4-C15	Pounds Cement: _	492		
WIIX 140	0-7-0-10	Tourido ocinient.			
1st Adjus	sted lbs. Cement:4	Source: _		Sp. Gr.:	3.14
IM 491.17	Fly Ash:7	Source: _	<u> </u>	Sp. Gr.:	2.65
IM 491.14	Slag GGBFS:	Source: _	<u> </u>	Sp. Gr.: _	333
2nd Adjus	sted lbs. Cement:4	18			
To	otal Cementitious4	92			
IM T203	Fine Aggregate Source			Sn Gr	2.66
IM T203	Interm. Aggregate Sou				2.00
IM T203	Coarse Agregate Sour			Sp. Gr.: _	
1141 1203	Coarse Agregate Sour	Ce	TOTAL SUBSTITUTE A BOOK OF	ор. от	
Basic w/c_	0.536	Water (lbs/c	y) = Design w/c (wt. cement + wt F	ly Ash +Slag) = _	264
Max w/c _	0.600	Max. Water (lbs/c	y) = Design w/c (wt. cement + wt F	ly Ash +Slag) = _	295
Absolute Volumes	Cement	((lbs/cy) / (Sp. Gr. X 62.4 X 27)	= _	0.079
	Fly Ash	((lbs/cy) / (Sp. Gr. X 62.4 X 27)	= _	0.017
	Slag	((lbs/cy) / (Sp. Gr. X 62.4 X 27)	= _	
	Water	((lbs/cy) / (1.00 X 62.4 X 27)		0.157
	Air				0.060
			Cultardal		0.242
			Subtotal	<u> </u>	
			1.000 - Subtotal Total	-	1.000
% FA Agg.: _	50	Fine Aggregate (1.000 - S	Subtotal) X % In Mix	-	0.343
		term. Aggregate (1.000 -	Subtotal) X % In Mix		
		oarse Aggregate (1.000 -			0.344
			Aggregate Total	-	0.687
Aggregate Weights	F	ne Aggregate (abs vol.)	X Sp. Gr. X 62.4 X 27		1537
	Intern	nediate Aggregate (abs	vol.) X Sp. Gr. X 62.4 X 27	=_	
	Co	arse Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27		1571
Summary		Cement _	418 (lbs/cy)		
			74 (lbs/cy)		
		Slag_	(lbs/cy)		
		Water _	264 (lbs/cy)		
		Fine Agg	1537_ (lbs/cy)		
		Interm. Agg	(lbs/cy)		
		Coarse Agg	1571 (lbs/cy)		
		10-12			
Distribution: Materials, DM	E, Proj. Engr., Contracto	10-12			

Office Of Materials PORTLAND CEMENT CONCRETE

		County :	
D-57-F15	Pounds Cement:		
ted lbs. Cement:	603 Source:	Sp. Gr.:	3.14
Fly Ash:	106 Source:	Sp. Gr.:	2.60
Slag GGBFS:	Source:	Sp. Gr.:	
sted lbs. Cement:	603		
otal Cementitious	709		
			2.66
Coarse Agregate	Source:	Sp. Gr.:	2./1
0.423	Water (lhs/cv) = Design w/c (wt cement + wt Fly Ast	+Slan) =	300
	max. 11a. (135.5), 255.g. 110 (111.5011611 111.1), 12.		La Contra
Cement	(lbs/cy) / (Sp. Gr. X 62.4 X 27)	- 7 - 12	0.114
Fly Ash	(lbs/cy) / (Sp. Gr. X 62.4 X 27)	- 1,2	0.024
Slag	(lbs/cy) / (Sp. Gr. X 62.4 X 27)	-8-3-	
Water	(lbs/cy) / (1.00 X 62.4 X 27)		0.178
Air			0.060
	Subtotal	_	0.376
	Total	-	1.000
-	5 A		0.040
			0.312
		_	0.312
50			0.624
	Aggregate Total		0.024
	Fine Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27	= -	1398
	Intermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27	=-	
	Coarse Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27		1425
	Cement603 (lbs/cy)		
	Fly Ash106_ (lbs/cy)		
	Slag (lbs/cy)		
	Water300_ (lbs/cy)		
	Fine Agg1398_ (lbs/cy)		
	Interm Agg (Ibe/gy)		
	10 12 Coarse Agg1425 (lbs/cy)		
	10-13		
	ted lbs. Cement: Fly Ash: Slag GGBFS: ted lbs. Cement: tal Cementitious Fine Aggregate S Interm. Aggregate Coarse Agregate 0.423 0.450 Cement Fly Ash Slag Water Air	Description Description	D-57_F15

Office Of Materials PORTLAND CEMENT CONCRETE

Project No.:	Problem 9				County : _	
Mix No.:	C-3WR-C15-S35	F	ounds Cement:	571		
1st Adju	usted lbs. Cement:	485	Source:	Lafarge I/II	Sp. Gr.:	3.14
IM 491.17	Fly Ash: _	86	Source:	Louisa	Sp. Gr.:	2.68
IM 491.14	Slag GGBFS:	170	Source:	Lafarge Newcem	Sp. Gr.: _	2.93
2nd Adju	usted lbs. Cement:	315	_			
1	Total Cementitious	571		The same of the same of		
IM T203	Fine Aggregate		A37514	<u> </u>	Sp. Gr.:	2.66
IM T203	Interm. Aggregate		404000	<u> </u>	Sp. Gr.:	0.05
IM T203	Coarse Agregate	Source:	A94002		Sp. Gr.:	2.65
Basic w/c	0.430		Water (lhs	/cy) = Design w/c (wt. cement + wt	Fly Ash +Slag) =	246
Max w/c	0.489			/cy) = Design w/c (wt. cement + wt	_	279
	0.100		(120	, , , , , , , , , , , , , , , , , , ,		
Absolute Volumes	Cement			(lbs/cy) / (Sp. Gr. X 62.4 X 27)		0.060
	Fly Ash			(lbs/cy) / (Sp. Gr. X 62.4 X 27)	-	0.019
	Slag			(lbs/cy) / (Sp. Gr. X 62.4 X 27)	=	0.034
	Water			(lbs/cy) / (1.00 X 62.4 X 27)		0.146
	Air					0.060
				Subtotal		0.319
				1.000 - Subtotal	=	0.681
				Total	-	1.000
% FA Agg.:	45	Fine /	Aggregate (1.000 -	Subtotal) X % In Mix		0.306
% In. Agg.:	- X 11 14: 22 - 1	Interm.	Aggregate (1.000	- Subtotal) X % In Mix		
% CA Agg.:	55	Coarse	Aggregate (1.000	- Subtotal) X % In Mix		0.375
				Aggregate Total	<u> </u>	0.681
Aggregate Weights		Fine Ag	gregate (abs vol	.) X Sp. Gr. X 62.4 X 27		1371
		Intermediat	e Aggregate (abs	s vol.) X Sp. Gr. X 62.4 X 27	=_	
		Coarse A	Aggregate (abs vo	ol.) X Sp. Gr. X 62.4 X 27	=_	1674
Summary			Cement	315 (lbs/cy)		
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~			Fly Ash	86 (lbs/cy)		
			Slag	170 (lbs/cy)		
			Water	246 (lbs/cy)		
			Fine Agg.	1371 (lbs/cy)		
			Interm. Agg.	(lbs/cy)		
			Coarse Agg.	1674 (lbs/cy)		

Date of Placement

Mix 1

Mix 2

Mix 3

Mix 4

Remarks

VER 1-06

10/19/06

10/19/06

Location From T

To

Project No.: FM91(15)-56-91

Contract ID: 73912

 Plant Name:
 Jensen - R63 & Hwy.92
 Country:
 Warren

 Contractor:
 Irving F. Jensen
 Temp. (°F) Min:
 40

 Contractor:
 Irving F. Jensen
 Temp. (°F) Min:
 40

 Weather:
 Sunny-cool
 Temp. (°F) Max:
 65

CC	Plan	it Re	port	
----	------	-------	------	--

Check N	lix(x)	Check Or	SEND	
Central	X	Paving	Х	(Daily)
Ready		Structure		(Weekly)
		Incidental		(Weekly)
		Patching		(Weekly)

			1977	Fir	ne Aggre	gate	Interm	nediate A	ggregate	Co	arse Aggi	egate		Ac	tual Quant	ities Used	Per cy (i	n pounds	)			Avg	Max
	Mix	Batched	% Of Est.	Moist.	T-203	Wt. SSD	Moist.	T-203	Wt. SSD	Moist.	T-203	Wt. SSD								Water		w/c	w/c
	Residen	(CY)	Used	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	Cement	Fly Ash	GGBFS	Fine	Inter.	Coarse	In Agg.	Plant	Grade	Ratio	Ratio
C.	-3WR	1,011.50	ATOME !	3.3	2.65	1,380				0.5	2.68	1,702	571		2 70	1,427	1	1,711	56	175.0		0.404	0.489
C.	-3WR	425.00		3.0	2.65	1,380	7 4 6			0.3	2.68	1,702	571		Part I	1,423	E PANA	1,707	48	173.0		0.387	0.489
			M. Jane	100			4 6			1330	1923			1221	19			13.3				11150	
US.	4 .67			10 17 15					3000	4-16	91. "	13.73	A STATE				10-7 7	ME TO	1			3 1 2	
					1		100			727					Far 74								

Coarse	1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply
	100	95-100		25-60		0-10	0-5	0-1.5	Y/N
	200 300				100				
Mary Company				9157	The last	100		4 / 46	

Conc. Treatment	(X)	lb / cy
Ice		
Heated Water	18.00	1000
Heated Materials		14.77

Report No.: 9

Date This Report: 10/19/06

Date Of Last Report: 10/18/01

Structures Des. No:

	Batched	t	
Check One (X)	Today X	Week	Total To Date
Concrete (CY):	1,436.50	1. 15	
Cement (tons):	410.12		

Intermedia	ate	1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply
		Maria Carlo							1	NA
					100			a rem	100.11	NA
				1 14			三自身	A com		NA

0-1.5	Y/N
- 1.0	1/19
100	
Will V	100

	Brand / Source	Rate	Lot Number
Air Entraining:	AEA-15/Sika	4.5 oz./yd.	J60038M
Water Reducer:	Plastocrete 161	2 oz./100#	J60011P
Retarder:		O WAY	Mark to the
Calcium Chloride:	W.K. T.E. P. I.		
Superplasticizer:	1 12 14 4		first to the

	1.5"	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200	Within
Target							Value 15						Targe
28		E STATE						100	11/2				23 48
		of the party	200	3,50		ASS TY	S. C. S. R.	STATE	No site				- 24
								3 8				5	

100	Туре	Sp. Gr.	Source	
Cement:	- 1	3.14	Ash Grove	
Fly Ash:				
GGBFS:				

196	125.46	14 X	1-434	THE ST	17	

	Source	T-203 A#	Grad. No.
Coarse:	POLICE.	A25512	3
ntermediate:		544	
Fine:		A77522	1

Distribution:	DME	Proj. Eng.	Plan

C.P.I.:	John Doe	SE000
onitor:	Mike Brown	SE999

### lowa Department Of Transportation

## Office Of Materials PORTLAND CEMENT CONCRETE

Project No.: FM91(15)-56-91 County: Warren Mix No.: C-3WR **Pounds Cement:** 1st Adjusted lbs. Cement: Source: Ash Grove 1 Sp. Gr.: 3.14 IM 491.17 Fly Ash: Source: Sp. Gr.: IM 491.14 Slag GGBFS: Source: Sp. Gr.: 2nd Adjusted lbs. Cement: **Total Cementitious IM T203** Fine Aggregate Source: Sp. Gr.: **IM T203** Interm. Aggregate Source: Sp. Gr.: **IM T203** Coarse Agregate Source: Sp. Gr.: Basic w/c Water (lbs/cy) = Design w/c ( wt. cement + wt Fly Ash +Slag) = Max. Water (lbs/cy) = Design w/c ( wt. cement + wt Fly Ash +Slag) = Max w/c 0.489 **Absolute Volumes** (lbs/cy) / (Sp. Gr. X 62.4 X 27) Fly Ash ..... (lbs/cy) / (Sp. Gr. X 62.4 X 27) Slag ..... (lbs/cy) / (Sp. Gr. X 62.4 X 27) (lbs/cy) / ( 1.00 X 62.4 X 27 ) Water ..... 0.146 0.060 Subtotal 0.314 1.000 - Subtotal 0.686 Total 1.000 Fine Aggregate (1.000 - Subtotal) X % In Mix 0.309 % FA Agg.: Interm. Aggregate (1.000 - Subtotal) X % In Mix % In. Agg.: Coarse Aggregate (1.000 - Subtotal) X % In Mix 0.377 % CA Agg.: Aggregate Total 0.686 Fine Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 1380 **Aggregate Weights** Intermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Coarse Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 1702 571 (lbs/cy) Summary Cement (lbs/cy) Fly Ash Slag (lbs/cy) Water 246 (lbs/cy) 1380 (lbs/cy) Fine Agg. (lbs/cy) Interm. Agg. 1702 (lbs/cy) Coarse Agg.

Distribution: ___ Materials, ___ DME, ___ Proj. Engr., ___ Contractor

Mix 5

VER 1-06



PCC Plant Report

So	lut	ion	#1	1

Temp. (°F) Max:

		LUCA	tion			
Date of Placer	ment	From	То	Project No.:	FN-63-1(26)38-63	
Mix 1	6/18/06			Plant Name:	Manatt's Hwy 146	-
Mix 2				Contractor:	Manatt's Inc.	-
Mix 3				Weather:	Warm-Cloudy	-
Miss A						

ontract ID:	28634	Report No.:
County:	Jefferson	Date This Report: 06/

Date This Report:	06/18/06
Date Of Last Report:	06/17/06
Structures Des No	

Check N	lix(x)	Check On	SEND	
Central	X	Paving	X	(Daily)
Ready	15	Structure		(Weekly)
		Incidental		(Weekly)
				044 - 14 - 1

	1.00		Fin	e Aggre	gate	Interm	nediate A	ggregate	Co	arse Agg	regate	12	Ac	tual Quant	ities Used	Per cy (i	n pounds	)	1 4 5 7 1		Avg	Max
Mix	Batched	% Of Est.	Moist.	T-203	Wt. SSD	Moist.	T-203	Wt. SSD	Moist.	T-203	Wt. SSD	23.	- 300	1		and Gui			Water		w/c	w/c
90	(CY)	Used	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	Cement	Fly Ash	GGBFS	Fine	Inter.	Coarse	In Agg.	Plant	Grade	Ratio	Ratio
C-4-C20	500.00	That was	2.7	2.65	1,473			571375	0.2	2.66	1,479	499	125	E 60	1,514		1,482	44	240.0		0.455	0.488
					2-38																	
								1 4							100	1000	100				7	
1				-	1 1	THE VEN	- P.		7					9 10 10	- 1	7 2 7			1.1.50		7	

Coarse	1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply
	100	95-100	A C	25-60		0-10	0-5	0-1.5	Y/N
		100		100		E-12-10	100		200
						- 0			The live

Conc. Treatment	(X)	lb / cy
Ice		19:11
Heated Water		1 90
Heated Materials		- Alle

	Batched	1	
Check One (X)	Today X	Week	Total To Date
Concrete (CY):	500.00	16.16.7	
Cement (tons):	124.75		1000

Intermediate	1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply
Intermediate	5 7 7 7		0,1		0.0		2		NA
N TWO									NA
		1,0		AC 33	1. 14. 14		- but		NA

Fine	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200	Comply
		100	90-100	70-100		10-60			0-1.5	Y/N
		1		El-My,	1100		312.87			
	744									

	Brand / Source	Rate	Lot Number
Air Entraining:	Darex AEA	5.0 oz./yd.	399034
Water Reducer:			
Retarder:			
Calcium Chloride:	177 7777		
Superplasticizer:		A BOTH	

				Adjuste	d % Pass	ing Calc	ulated Con	nbined Gra	dation	Š.	1. 3	23.5	5
	1.5"	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200	Within
Target				12 7			4 1 14				100	1	Target
			7 1	1					100			150	1
							-5 (1)	1.36		3 4 13			
	Total M	WET'S	THE STATE OF	12	7 2		4216	10,40	0				

40.0	Туре	Sp. Gr.	Source
Cement:	1/11	3.14	Ash Grove
Fly Ash:	С	2.70	Louisa Generating
GGBFS:			

Remarks	

	Source	1-203 A#	Grad. No.
Coarse:	Moscow 3i	A70002	3
Intermediate:			
Fine:	Hoffman	A90504	1

Distribution:	DME	Proj. Eng.	Plan

C.P.I.:	John Doe	SE000
onitor:	Mike Brown	SE999

# Iowa Department Of Transportation Office Of Materials PORTLAND CEMENT CONCRETE

Project No.: FN-63-1(26)--38-63 County: Jefferson C-4-C20 **Pounds Cement:** 624 Mix No.: 499 Source: Ash Grove I/II 1st Adjusted lbs. Cement: Sp. Gr.: 3.14 IM 491.17 Fly Ash: 125 Source: Louisa Generating Sp. Gr.: 2.70 IM 491.14 Slag GGBFS: Source: Sp. Gr.: 2nd Adjusted lbs. Cement: 499 **Total Cementitious** 624 **IM T203** Fine Aggregate Source: Hoffman A90504 Sp. Gr.: 2.65 **IM T203** Interm. Aggregate Source: Sp. Gr.: **IM T203** Coarse Agregate Source: Moscow 3i A70002 Sp. Gr.: 2.66 0.430 Water (lbs/cy) = Design w/c ( wt. cement + wt Fly Ash +Slag) = 268 Basic w/c 0.488 Max. Water (lbs/cy) = Design w/c ( wt. cement + wt Fly Ash +Slag) = 305 Max w/c Absolute Volumes (lbs/cy) / (Sp. Gr. X 62.4 X 27) 0.094 Cement ..... (lbs/cy) / (Sp. Gr. X 62.4 X 27) 0.027 Fly Ash ..... Slag ..... (lbs/cy) / (Sp. Gr. X 62.4 X 27) (lbs/cy) / ( 1.00 X 62.4 X 27 ) 0.159 Water ..... 0.060 Subtotal 0.340 1.000 - Subtotal 0.660 Total 1.000 Fine Aggregate ( 1.000 - Subtotal ) X % In Mix 0.330 % FA Agg.: Interm. Aggregate ( 1.000 - Subtotal ) X % In Mix % In. Agg.: 50 Coarse Aggregate ( 1.000 - Subtotal ) X % In Mix 0.330 % CA Agg.: Aggregate Total 0.660 Fine Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 **Aggregate Weights** 1473 Intermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Coarse Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 1479 499 (lbs/cy) Cement Summary 125 (lbs/cy) Fly Ash Slag (lbs/cy) 268 (lbs/cy) Water 1473 (lbs/cy) Fine Agg. Interm. Agg. (lbs/cy) 1479 (lbs/cy) Coarse Agg. Distribution: ___ Materials, ___ DME, ___ Proj. Engr., ___ Contractor

10-17

VER 1-06

Location

#### **PCC Plant Report**

	Sol	lution	#12
--	-----	--------	-----

of Placen	nent	From	То
Mix 1	8/6/06		
Mix 2			
Mix 3			
Mix 4			

Project No.: BROS-68(22)10 Contract ID: 28634 County: Carroll

Plant Name: American Concrete - Carroll Temp. (°F) Min: _____72 Contractor: Iowa Culvert Builders

Weather: Warm-Dry Temp. (°F) Max: 85

Check Mix(x) Check One(x) Central Report No.: 1 Paving Date This Report: 08/06/06 Ready

SEND (Daily) Structure (Weekly) Incidental (Weekly) Patching (Weekly)

			Fin	e Aggre	gate	Interm	ediate A	ggregate	Co	arse Agg	regate		Ac	tual Quant	ities Used	Per cy (i	n pounds				Avg	Max
Mix	Batched	% Of Est.	Moist.	T-203	Wt. SSD	Moist.	T-203	Wt. SSD	Moist.	T-203	Wt. SSD	100							Water	N. N.	w/c	w/c
1701440	(CY)	Used	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	Cement	Fly Ash	GGBFS	Fine	Inter.	Coarse	In Agg.	Plant	Grade	Ratio	Rati
C-3WR-C20S35	77.00		3.1	2.66	1,371			1000	0.8	2.64	1,668	297	114	160	1,415		1,681	57	180.0	18.0	0.447	0.489
										-						1						
				- 3/		7.57									- 74.17	1111		7				100
J. 52 05 4 74 1	31.50.6		7 6.0		631.00	9.		73.6	1900		THE ALL			- 3	7	775	100				ROLL TO	100

Coarse	1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply
TO THE	100	95-100		25-60	THE I	0-10	0-5	0-1.5	Y/N
		1 1 1		30		C ( )			
A				74	-		100		
		1 30				130/90	1/2 3		

Conc. Treatment	(X)	lb / cy
Ice		
Heated Water		1112
Heated Materials		

Date Of Last Report:

Structures Des. No: 517

	Batche	d	71,71
	Today	Week	Total
Check One (X)		Х	To Date
Concrete (CY):		77.00	
Cement (tons):		11.43	

Intermedia	ite	1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply
								100		NA
		Y HOUSE				FE.W	1 19		11	NA
	We take						Y 47 (6)	3. 13.	4.7	NA

Fine	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200	Comply
		100	90-100	70-100		10-60	1 mg 1	100	0-1.5	Y/N
								-		
						1000				

	Brand / Source	Rate	Lot Number
Air Entraining:	Darex AEA	5.0 oz./yd.	3890334
Water Reducer:	Plastocrete 161	2 oz./100#	5577882
Retarder:		4-11	
Calcium Chloride:			
Superplasticizer:	Tall and the		

	1.5"	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200	Withir
Target												100	Targe
			17/201							24.0		No.	
												1000	

	Type	Sp. Gr.	Source
Cement:	1/11	3.14	Ash Grove
Fly Ash:	С	2.79	Burlington
GGBFS:		2.87	Holcim-Grancem

T-203 A# Grad. No.

3

1

Coarse:	A57018				
Intermediate: Fine:	A53508				

Source

emarks		
No. of London		

Distribution:	DME	Proj. Eng.	Plan

John Doe	NW000
Mike Brown	NW999
	Mike Brown

# Iowa Department Of Transportation Office Of Materials PORTLAND CEMENT CONCRETE

Project No.:	BROS-68(22)10				rroll		
Mix No.:	C-3WR-C20S35	Pounds	Cement:	571			
1st Adj	usted lbs. Cement:	457	Source:	Ash Grove I	/II	Sp. Gr.:	3.14
IM 491.17	Fly Ash: _	114	Source:	Burlington	<u> </u>	Sp. Gr.: _	2.79
IM 491.14	Slag GGBFS:	160	Source:	Holcim-Gran	ncem	Sp. Gr.:	2.87
2nd Adj	usted lbs. Cement:	297					
	Total Cementitious	571					
IM T203	Fine Aggregate					Sp. Gr.:	2.66
IM T203	Interm. Aggrega	te Source:				Sp. Gr.:	17.10.50
IM T203	Coarse Agregat	te Source:			A LABOR D	Sp. Gr.:	2.64
Basic w/c	0.430	Water	(lbs/cv) = E	esian w/c ( v	vt. cement + wt Fly	Ash +Slag) =	246
Max w/c	0.489				vt. cement + wt Fly	-	279
Absolute Volumes	Cement .			(lbs/cy) / ( S	p. Gr. X 62.4 X 27)		0.056
	Fly Ash .			(lbs/cy) / ( S	p. Gr. X 62.4 X 27)	= 2	0.024
	Slag .			(lbs/cy) / ( S	p. Gr. X 62.4 X 27)		0.033
	Water .			(lbs/cy) / ( 1.	00 X 62.4 X 27 )	=_	0.146
	Air .					<u> </u>	0.060
					Subtotal		0.319
					1.000 - Subtotal	=	0.681
					Total	=	1.000
0/ 54 4	45	Fine Annua	oto / 1 000	Cubtatal \ V	O/ Im Mile		0.200
% FA Agg.:	45	Fine Aggreg				]	0.306
% In. Agg.:		Interm. Aggre	_				0.075
% CA Agg.:	55	Coarse Aggre	gate ( 1.000				0.375
				Aggreg	gate Total		0.681
Aggregate Weights		Fine Aggregat	e (abs vol	.) X Sp. Gr. X	62.4 X 27	=_	1371
		Intermediate Aggr	egate (abs	vol.) X Sp. G	Gr. X 62.4 X 27	=_	
		Coarse Aggreg	ate (abs vo	ol.) X Sp. Gr. )	X 62.4 X 27		1668
Summary			Cement	297	(lbs/cy)		
Charles backets			Fly Ash		(lbs/cy)		
			Slag		(lbs/cy)		
			Water		(lbs/cy)		
			Fine Agg.		(lbs/cy)		
		1.					
			oarse Agg.		(lbs/cy)		
			ourse Agg.	1000	(ibaroy)		
Distribution: Materials, I	DME, Proj. Engr.,	Contractor					

PCC Plant Report

Conc. Treatment

Ice **Heated Water Heated Materials**  lb / cy

(X)

20	1.14	ion	#1	2	

		Loca	tion				Solution #13		
Date of Placer	ment	From	То	Project No.:	STP-64(12)28-58	Contract ID:	67592	Report No.:	4
Mix 1	9/17/06		1 75	Plant Name:	Carlson's - Hwy 218 & F62	County:	Louisa	Date This Report:	09/17/06
Mix 2	9/17/06			Contractor:	Fred Carlson Co.	Temp. (°F) Min:	69	Date Of Last Report:	09/16/06
Mix 3				Weather:	Sunny-hot	Temp. (°F) Max:	87	Structures Des. No:	17.74
Mix 4		音片	Description of						
Mix 5			1977						

Check N	lix(x)	Check On	e(x)	SEND
Central	X	Paving	X	(Daily)
Ready		Structure		(Weekly)
		Incidental	36.7	(Weekly)
		Patching		(Weekly)

		y 37 14	Fin	e Aggreg	ate	Interm	ediate A	ggregate	Coa	arse Aggr	regate		Ac	tual Quant	ities Used	Per cy ( i	n pounds	)			Avg	Max
Mix	Batched	% Of Est.	Moist.	T-203	Wt. SSD	Moist.	st. T-203 Wt. SSD Moist. T-203 Wt. SSD	F 4.5		Water		w/c	w/c									
The state of	(CY)	Used	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	Cement	Fly Ash	GGBFS	Fine	Inter.	Coarse	In Agg.	Plant	Grade	Ratio	Ratio
C-3WR-C20	1,256.00		3.1	2.66	1,380		30 F R. 1		0.7	2.62	1,664	451	113	0176	1,424		1,676	56	175.0		0.409	0.489
C-3WR-C20	1,384.00	1465	2.8	2.66	1,380				0.5	2.62	1,664	451	113	Color St	1,420		1,672	48	190.0		0.422	0.489
								1330				124		14.77	ob at						17.5	200
					2 17	1 1		3 7 2	Sec. 1	Secure				LE NO	-3. 3.				1			
		1978		-	THE P			2 Min	A Day So	4		3		Wint !		1		1	7.77			

Coarse	1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply
V MALE	100	95-100		25-60		0-10	0-5	0-1.5	Y/N
1 100 m		1221				m2.6	-77		
			2						

UE DEPTE	Batched	d	
Check One (X)	Today X	Week	Total To Date
Concrete (CY):	2,640.00		Trans.
Cement (tons):	595.32		

Intermedia	ate	1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply
									9 4 6	NA
		HE			- 4	9 E N	- 1		100	NA
									WE IN	NA

	Brand / Source	Rate	Lot Number
Air Entraining:	Ad/Aire	5.0 oz./yd.	233998
Water Reducer:	Daratard 17	3 oz./100#	5577882
Retarder:	2 t 173h 2 12 s		
alcium Chloride:	(C) 1 (C) 1 (C)		
······································			

Fine	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200	Comply
		100	90-100	70-100	1.4	10-60			0-1.5	Y/N
	1				8.8			3 %	2. 4	
	1 2 7					79.00		7 50	100	736

	Туре	Sp. Gr.	Source
Cement:	1SM	3.10	LaFarge
Fly Ash:	С	2.64	Council Bluffs#3
GGBFS:			

				Adjuste	ed % Pass	ing Calcu	ulated Con	nbined Gra	dation				
6	1.5"	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200	Within
Target		100			-50.41					-717	140.74		Target
		HI THE	1984					1 - 1 - 1	1	TI-CA			1-4
	1 7-7					A1 18/						14-10-	17.2
10.00			1	1.5					13 11			- 5 X	

	Source	T-203 A#	Grad. No.
Coarse:		A57004	3
Intermediate:	Carlotte Car		
Fine:		A58504	1

-					

C.P.I.:	John Doe	SE000
Monitor:	Mike Brown	SE999

Distribution:	DME	Proj. Eng.	Pla

# Iowa Department Of Transportation Office Of Materials PORTLAND CEMENT CONCRETE

Project No.: STP-64(12)28-58 County: Louisa Mix No.: C-3WR-C20 **Pounds Cement:** 1st Adjusted lbs. Cement: Source: LaFarge 1SM Sp. Gr.: 3.10 IM 491.17 Fly Ash: Source: Council Bluffs#3 Sp. Gr.: Sp. Gr.: IM 491.14 Slag GGBFS: Source: 2nd Adjusted lbs. Cement: **Total Cementitious IM T203** Fine Aggregate Source: Sp. Gr.: **IM T203** Interm. Aggregate Source: Sp. Gr.: **IM T203** Coarse Agregate Source: Sp. Gr.: 2.62 Basic w/c 0.430 Water (lbs/cy) = Design w/c ( wt. cement + wt Fly Ash +Slag) = 243 Max. Water (lbs/cy) = Design w/c ( wt. cement + wt Fly Ash +Slag) = 276 Max w/c 0.489 (lbs/cy) / (Sp. Gr. X 62.4 X 27) **Absolute Volumes** Cement ..... 0.086 Fly Ash ..... (lbs/cy) / (Sp. Gr. X 62.4 X 27) 0.025 Slag ..... (lbs/cy) / (Sp. Gr. X 62.4 X 27) (lbs/cy) / ( 1.00 X 62.4 X 27 ) 0.144 Water ..... 0.060 Subtotal 0.315 1.000 - Subtotal 0.685 Total 1.000 Fine Aggregate (1.000 - Subtotal) X % In Mix 0.308 % FA Agg.: Interm. Aggregate ( 1.000 - Subtotal ) X % In Mix % In. Agg.: 0.377 55 Coarse Aggregate ( 1.000 - Subtotal ) X % In Mix % CA Agg.: 0.685 Aggregate Total 1380 **Aggregate Weights** Fine Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Intermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Coarse Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 1664 Cement 451 (lbs/cy) Summary 113 (lbs/cy) Fly Ash Slag (lbs/cy) Water 243 (lbs/cy) 1380 (lbs/cy) Fine Agg. Interm. Agg. (lbs/cy) 1664 (lbs/cy) Coarse Agg.

Distribution: ___ Materials, ___ DME, ___ Proj. Engr., ___ Contractor

VER 1-06

Distribution:

DME



 44	A		

PCC Plant Report

		Loca	ition				Solution #14
Date of Placer	nent	From	То	Project No.:	STP-53-4(15)2C-53	Contract ID:	4920
Mix 1	8/6/06		787-5	Plant Name:	Kirk Ready Mix	County:	Jones
Mix 2	8/6/06			Contractor:	Kirk Const.	Temp. (°F) Min:	65
Mix 3	8/6/06			Weather:	Sunny/Warm	Temp. (°F) Max:	85
Mix 4		5 100	Y aut				
	A LANGE OF	111					

Check	Mix(x)	Check Or	ne(x)	SEND
Central		Paving	144	(Daily)
Ready	X	Structure	X	(Weekly)
		Incidental		(Weekly)
		Databina		Mankha

	Party (		15 15	Fin	ne Aggre	gate	Intern	nediate A	ggregate	Co	arse Agg	regate		Ac	tual Quant	ities Used	Per cy (i	n pounds	)			Avg	Max
	Mix	Batched	% Of Est.	Moist.	T-203	Wt. SSD	Moist.	T-203	Wt. SSD	Moist.	T-203	Wt. SSD	188					Sur S		Water		w/c	w/c
		(CY)	Used	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	(%)	Sp. G.	(lbs)	Cement	Fly Ash	GGBFS	Fine	Inter.	Coarse	In Agg.	Plant	Grade	Ratio	Ratio
C-3WI	R-C15S35	182.00		3.7	2.66	1,376		1 1		0.7	2.66	1,681	315	86	170	1,429	237	1,693	65	175.0	19.0	0.453	0.489
C-	-4-C15	35.00		3.4	2.66	1,479		4	3	0.8	2.66	1,483	530	94	A DO	1,531	3.45	1,495	64	183.0	25.0	0.436	0.488
	M-4	14.00		3.4	2.66	1,394			1 18 18	0.8	2.66	1,398	825			1,443		1,409	60	252.0	14.0	0.396	0.400
							1.00		V 17 14 5 1						The state of	Party.	Bath		10				
		Le Taylor	A TATAL		K 11 11	Takin Be	1.3	1	17-18		E IS				TE TE		11 1					4 10 10	

oarse	1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply
	100	95-100		25-60	1	0-10	0-5	0-1.5	Y/N
	44 2 11			374					
	and product	W 63		17			6-11		
1. 19-11	A Property Commence	17 4 7			1-0-1			HAT Y	==10

Conc. Treatment	(X)	lb / cy	Batched			
Ice	3.113			Today	Week	Total
Heated Water	t w	11 7 7 8	Check One (X)		Х	To Date
Heated Materials	HE .	F 36 7 7	Concrete (CY):		231.00	
			Cement (tons):		43.72	

Brand / Source

Intermedia	ite	1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#200	Comply
					75 (93	10 mg			EN THE	NA
				11/4					17.48	NA
			Town I							NA

Water Reducer:	WRDA w/Hyd
Retarder:	14.08
Calcium Chloride:	
Superplasticizer:	

Air Entraining: Daravair 1400

Report No.: 1
Date This Report: 08/06/06

Date Of Last Report: ______ Structures Des. No: 4920

Fine 1/	1/2"	3/8"	3/8" #4	#8	#16	#16 #30	#50	#100	#200	Comply
	1	100 90-100	70-100		10-60	181	0-1.5		Y/N	
	1837					2				
				77						13.60
		MATE IN						1 150		100

Cement:	- 11	3.14		LaFarge
Fly Ash:	С	2.79	12/11/20	Burlington
GGBFS:	120	2.93		NewCem

Rate

3 oz./yd. AA9912 3.0 oz/100# AWR99915

Lot Number

Source

-	1.5"	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200	Within
-	1.0	-	5/4	1/2	5/0	77	#10	#10	#50	#50	#100	#200	***************************************
Target									1		to the second	200	Target
				THE STATE OF		The same		37 9.99	10-10	77 X		WELL TO	-

	Source	T-203 A#	Grad. No.
Coarse:		A53004	3
Intermediate:		- 100	
Fine:	100	A53502	1

Type Sp. Gr.

marks		AND THE RESERVE OF TH		_ 300	
	The Tarret		1 . T. A. SSA		44.3

Proj. Eng.

C.P.I.:	John Doe	NE000
lonitor:	Jane Doe	NE999

Rev 02/01

# Iowa Department Of Transportation Office Of Materials PORTLAND CEMENT CONCRETE

Form E820150E

Project No.: STP-53-4(15)--2C-53 County: Jones Mix No.: C-3WR-C15S35 **Pounds Cement:** 571 1st Adjusted lbs. Cement: Source: LaFarge II Sp. Gr.: 3.14 IM 491.17 Fly Ash: Source: Burlington Sp. Gr.: 2.79 IM 491.14 Slag GGBFS: Source: NewCem Sp. Gr.: 2.93 2nd Adjusted lbs. Cement: **Total Cementitious IM T203** Fine Aggregate Source: Sp. Gr.: 2.66 **IM T203** Interm. Aggregate Source: Sp. Gr.: **IM T203** Coarse Agregate Source: Sp. Gr.: 2.66 Basic w/c 0.430 Water (lbs/cy) = Design w/c ( wt. cement + wt Fly Ash +Slag) = Max w/c 0.489 Max. Water (lbs/cy) = Design w/c ( wt. cement + wt Fly Ash +Slag) = **Absolute Volumes** (lbs/cy) / (Sp. Gr. X 62.4 X 27) Fly Ash ..... (lbs/cy) / (Sp. Gr. X 62.4 X 27) 0.018 Slag ..... (lbs/cy) / (Sp. Gr. X 62.4 X 27) 0.034 (lbs/cy) / ( 1.00 X 62.4 X 27 ) Water ..... 0.146 0.060 Subtotal 0.318 1.000 - Subtotal 0.682 Total 1.000 % FA Agg.: Fine Aggregate (1.000 - Subtotal) X % In Mix 0.307 Interm. Aggregate ( 1.000 - Subtotal ) X % In Mix % In. Agg.: 55 Coarse Aggregate ( 1.000 - Subtotal ) X % In Mix 0.375 % CA Agg.: Aggregate Total 0.682 **Aggregate Weights** Fine Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 1376 Intermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 Coarse Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27 1681 Summary Cement 315 (lbs/cy) Fly Ash 86 (lbs/cy) Slag 170 (lbs/cy) Water 246 (lbs/cy) 1376 (lbs/cy) Fine Agg. Interm. Agg. (lbs/cy) 1681 (lbs/cy) Coarse Agg. Distribution: ___ Materials, ___ DME, ___ Proj. Engr., ___ Contractor

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Projec	ct No.: S	TP-53-4(15)-2C-53	County: Jones	County: Jones	
Mi	ix No.: _	C-4-C15	Pounds Cement: 624		
	1st Adjus	ted lbs. Cement:	530 Source:	Sp. Gr.:	3.14
IM	491.17	Fly Ash: _	94 Source:	Sp. Gr.:	2.79
IM	491.14	Slag GGBFS:	Source:	Sp. Gr.:	
	2nd Adjus	sted lbs. Cement: _	530		
	То	otal Cementitious	624		
	M T203	Fine Aggregate		Sp. Gr.:	2.66
	M T203	Interm. Aggregat		Sp. Gr.:	
	M T203	Coarse Agregate	Source:	Sp. Gr.:	2.66
		0.420	Material Designation of the Asset Control of the As	L . CI\	000
	sic w/c	0.430	Water (lbs/cy) = Design w/c ( wt. cement + wt Fly As		268
	Max w/c_	0.488	Max. Water (lbs/cy) = Design w/c ( wt. cement + wt Fly As	n +Slag) = _	305
Absolute Volume	es	Cement	(lbs/cy) / ( Sp. Gr. X 62.4 X 27)		0.100
		Fly Ash	(lbs/cy) / ( Sp. Gr. X 62.4 X 27)		0.020
		Slag	(lbs/cy) / ( Sp. Gr. X 62.4 X 27)		
		Water	(lbs/cy) / ( 1.00 X 62.4 X 27 )	=_	0.159
		Air			0.060
			Subtotal	_	0.339
			1.000 - Subtotal	6 No. 10	0.661
			Total		1.000
% FA	A Agg.:	50	Fine Aggregate ( 1.000 - Subtotal ) X % In Mix	=	0.330
% In.	. Agg.: _		Interm. Aggregate ( 1.000 - Subtotal ) X % In Mix	1 J	
% CA	A Agg.:	50	Coarse Aggregate ( 1.000 - Subtotal ) X % In Mix	5-10 Z = 5	0.331
	70		Aggregate Total	= _	0.661
Aggregate Weig	hts		Fine Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27	-	1479
			Intermediate Aggregate (abs vol.) X Sp. Gr. X 62.4 X 27		
			Coarse Aggregate ( abs vol.) X Sp. Gr. X 62.4 X 27	_	1483
				01	- 1
Summary			Cement 530 (lbs/cy)		
			Fly Ash 94 (lbs/cy)		
			Slag (lbs/cy)		
			Water 268 (lbs/cy)		
			Fine Agg1479 (lbs/cy)		
			Interm. Agg. (lbs/cy) Coarse Agg. 1483 (lbs/cy)		

### Iowa Department Of Transportation

## Office Of Materials PORTLAND CEMENT CONCRETE

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Project No.: S	TP-53-4(15)-2C-53		County : Jo	nes	
Mix No.:	M-4	Pounds Cement:	825		
1st Adjus	sted lbs. Cement:	825 Source:		Sp. Gr.: _	3.14
IM 491.17	Fly Ash: _	Source:		Sp. Gr.:	
IM 491.14	Slag GGBFS:	Source:	No. 2 San Baser	Sp. Gr.:	
2nd Adjus	sted lbs. Cement: _	825			
To	otal Cementitious				
IM T203	Fine Aggregate	Source:	San Talk Sulta had	Sp. Gr.:	2.66
IM T203	Interm. Aggregat	te Source:	the state of the s	Sp. Gr.:	
IM T203	Coarse Agregate	e Source:		Sp. Gr.:	2.66
Basic w/c	0.328	Water (lbs/cv) = De	sign w/c ( wt. cement + wt Fly	Ash +Slag) =	271
Max w/c	0.400		sign w/c ( wt. cement + wt Fly	_	330
Absolute Volumes	Cement	(	lbs/cy) / ( Sp. Gr. X 62.4 X 27)	-	0.156
	Fly Ash	(	lbs/cy) / ( Sp. Gr. X 62.4 X 27)	=_	
	Slag	(	lbs/cy) / ( Sp. Gr. X 62.4 X 27)		
	Water	(	lbs/cy) / ( 1.00 X 62.4 X 27 )	-	0.161
	Air				0.060
			Subtotal	=	0.377
			1.000 - Subtotal	=	0.623
			Total	= -	1.000
% FA Agg.: _	50	Fine Aggregate ( 1.000 - S	ubtotal ) X % In Mix	udbio of # _	0.311
% In. Agg.:	The state of the second	Interm. Aggregate ( 1.000 -			
% CA Agg.:	50	Coarse Aggregate ( 1.000 -	Subtotal ) X % In Mix	1_2 to 200 = 3_0	0.312
			Aggregate Total	= _	0.623
Aggregate Weights		Fine Aggregate (abs vol.)	X Sp. Gr. X 62.4 X 27	3: ja 4 <u>= ∪</u>	1394
		Intermediate Aggregate (abs v	vol.) X Sp. Gr. X 62.4 X 27		
		Coarse Aggregate (abs vol.	) X Sp. Gr. X 62.4 X 27	A	1398
Summary		Cement _	825 (lbs/cy)		
		Fly Ash _	(lbs/cy)		
		Slag_	(lbs/cy)		
		Water _	271 (lbs/cy)		
		Fine Agg.	1394 (lbs/cy)		
		Interm. Agg.	(lbs/cy)		
		Coarse Agg.	1398 (lbs/cy)		

Total = 
$$3,461,034$$
 lb  $\div 2000 = 1730.52$ 

Left in scale hopper:  $3000 \text{ lb} \div 2000 = 1.50$ 

Left from last check:  $4096 \text{ lb} \div 2000 = 2.05$ 

$$1730.52 + 1.50 - 2.05 = 1729.97$$
Total billed = 3, 333, 333 ÷ 2000 = 1666.67
$$(1729.97 \div 1666.67) \times 100 = 103.8 \%$$

#### Remember:

- 1. Cement shipment yield determination must be made every 10,000 yd³ after the original determination has been made near the end of the first full day of production.
- 2. Cement yield cannot be under 99% or above 101.0%
- 3. Check your calculation, records, and equipment.

1480 batches x 492 lb/batch = 728,160 lb ÷ 2000 lb/ton = **364.08 ton** 

500 batches x 571 lb/batch =  $285,500 \text{ lb} \div 2000 \text{ lb/ton} = 142.75 \text{ ton}$ 

#### Total batched 506.83 ton

Left in scale

Last check:  $2600 \div 2000 = 1.30 \text{ ton}$ 

This check:  $3000 \div 2000 = 1.50 \text{ ton}$ 

Total billed: 1, 024,  $100 \div 2000 = 512.05$  ton

Total Cement + Left in Scale - Left in Scale Cement

Batched This Check From Last Check x 100 = Yield

**Total Cement Billed** 

 $506.83 + 1.50 - 1.30 \times 100 =$ Cement Yield 512.05

507.03

 $512.05 \times 100 = 99.0\%$ 

### Given:

Cement Yield

Tons Billed = 902.38

Number of Batches = 3180

571 lb cement per yd3

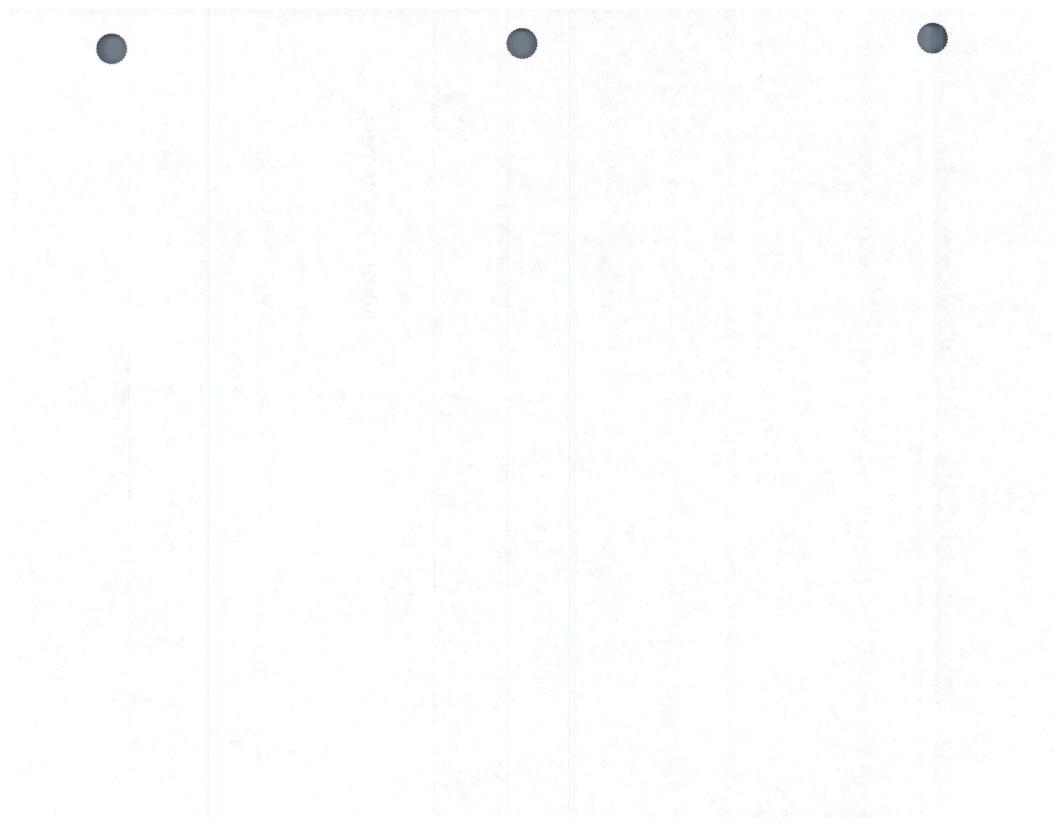
### **Solution and Answer**

Total Tons Batched =  $3180 \times 571 = 907.89$ 

2000

Cement Yield = <u>907.89 batched</u>

902.38 billed  $\times 100 = 100.6\%$ 



### **lowa Department of Transportation**

### Technical Training and Certification Program

#### **COURSE EVALUATION SHEET**

REMARKS:

In an effort to improve the Iowa DOT Technical Training and Certification Program, we ask that you fill out this evaluation form after you have taken the exam. Thank you for your cooperation.

Co	urse:	Location:
Ins	tructor:	
1.	What type of ager	ncy are you employed by?
2.	Please rate the fo	llowing portion of the course on a scale of 1-5. 1 = Poor, 5 = Excellent
		Facility:
		Material:
		Instructors:
		Course Activities: (lectures, videos, demonstrations, etc.)
3.	Are there any cha	anges you would like to see made in the course?

