

# Implementation of Low-Temperature Cracking Criteria in Iowa

**Final Report**  
**April 2021**



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<b>16. Abstract</b> <p>Iowa is among the northern US states that experience fluctuating low temperatures that cause low-temperature thermal cracking. Thermal stress buildup in pavements due to low temperatures—and often large, sudden drops in temperatures—result in excessive thermal cracking that requires frequent maintenance work. This increases maintenance costs for pavements and reduces pavement service life, adding an extra cost to departments of transportation (DOTs) budgets. To prevent this distress from occurring too soon in new pavements, there are specifications to guide engineers in designing asphalt pavement mixes. Generally, it is expected that field-produced mixes will have higher variance within their results when compared to laboratory-produced mixes. However, when the variance is too high, mix performance becomes compromised, thus leading to more excessive thermal fracture at low temperatures.</p> <p>This study evaluated the current performance of field-produced mixtures using various low-temperature cracking methods and recommends necessary adjustments to the limiting criteria for laboratory-produced mixes to enable asphalt pavements to perform better and last longer under low-temperature cracking. Ten different field-produced asphalt mixtures were obtained from paving projects paved within the past seven years. These mixtures were reheated and laboratory-compacted using a gyratory compactor to produce 6 in. (150 mm) diameter specimens with a height of approximately 2 in. (50 mm). To determine the fracture energies of the compacted sample, disk-shaped compact tension (DCT) and semi-circular bend (SCB) tests were carried out as specified by ASTM D7313-13 and AASHTO TP 105-13, respectively. Air voids were determined prior to testing to ensure that specimens used met the air void requirement of 7% for testing. Illinois Flexibility Index Test (I-FIT) Procedure 405 was used for testing at intermediate warmer temperatures to get the flexibility index (FI) as well.</p> <p>The 10 mixtures evaluated had an average fracture energy ranging from 265–470 J/m<sup>2</sup> and 485–905 J/m<sup>2</sup> for DCT and SCB, respectively. The FI obtained for the mixtures ranged from 8.36 to 23.32. The DCT fracture energies did not meet the DCT specifications contained in IM510 for the average minimum fracture energies, and the DCT and SCB fracture energies are lower than those produced for approval to pave. A performance criteria adjustment is recommended to ensure that field-produced mixtures meet design specifications from the laboratory to the field.</p>			
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## **Principal Investigator**

R. Christopher Williams, Director  
Asphalt Materials and Pavement Program  
Institute for Transportation, Iowa State University

## **Research Assistants**

Joseph Podolsky and Joyce Kamau

## **Authors**

R. Christopher Williams, Joseph Podolsky, and Joyce Kamau

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A report from

**Asphalt Materials and Pavement Program  
Institute for Transportation**

**Iowa State University**

2711 South Loop Drive, Suite 4700

Ames, IA 50010-8664

Phone: 515-294-8103 / Fax: 515-294-0467

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## **EXECUTIVE SUMMARY**

### **Goals**

The goals of this project were to assess the low-temperature cracking resistance of asphalt mixtures used by the Iowa Department of Transportation (DOT), correlate the laboratory results with field performance, and use those correlations to propose additional performance criteria.

### **Problem Statement**

Thermal stress buildup in pavements due to low temperatures—and often large, sudden drops in temperatures—result in excessive thermal cracking that requires frequent maintenance work. This increases maintenance costs for pavements and reduces pavement service life.

### **Background**

Iowa is among the northern US states that experience fluctuating low temperatures that cause low-temperature thermal cracking. To prevent this distress from occurring too soon in new pavements, engineers use specifications to guide them in designing asphalt pavement mixes.

Current Superpave specifications address thermal cracking at low temperatures based on creep and strength testing of asphalt binders and mixtures, but the specifications only have limiting criteria set forth in the asphalt binder specifications. In addition, these low-temperature characterization methods do not take into account the effect from the aggregate part of the mixture.

Mix test specifications consider the effect from both binder and aggregate. However, mix test specifications do not have clearly set national limits in Superpave; they are set by individual state agencies. Researchers and state DOTs within the Midwestern US have used the disk-shaped compact tension (DCT) test, the semi-circular bend (SCB) test, and the Illinois Flexibility Index Test (I-FIT) to assess low-temperature cracking/fracture in mixtures.

To avoid thermal cracking in the field, characterization of mechanical fracture of the asphalt mixture is important in predicting the pavement performance and assists the design engineer in establishing a mix design that can withstand the cold climate for the design period.

### **Project Description**

Ten field-produced asphalt mixtures were obtained from projects that represented typical asphalt mixtures used in Iowa. The mixtures were from Fayette, Hamilton, Harrison, Johnson, Lyon, Marshall, Polk, and Union counties.

Five mixtures were from the old design, and the other five mixtures were from the new design. The mixtures had different binder grades and aggregate gradation, voids in mineral aggregate (VMA), voids filled with asphalt (VFA), binder content, and varying percentage of the recycled material. These mixtures were reheated and laboratory-compacted using a gyratory compactor to produce 6 in. (150 mm) diameter specimens with a height of approximately 2 in. (50 mm).

To determine the fracture energies of the compacted samples, DCT and SCB tests were carried out as specified by ASTM D7313-13 and AASHTO TP 105-13, respectively. Air voids were determined prior to testing to ensure that the specimens used met the air void requirement of 7% for testing. I-FIT Procedure 405 was used for testing at intermediate warmer temperatures to get the flexibility index (FI) as well.

### **Key Findings**

- The 10 mixtures evaluated had an average fracture energy ranging from 265–470 J/m<sup>2</sup> and 485–905 J/m<sup>2</sup> for DCT and SCB, respectively.
- The DCT fracture energies did not meet the DCT specifications contained in Instructional Memorandum 510 for the average minimum fracture energies.
- The DCT and SCB fracture energies are lower than those produced for approval to pave.
- The FI obtained for the mixtures ranged from 8.36 to 23.32.

### **Implementation Readiness and Benefits**

This project assessed 10 field-produced asphalt mixtures used in Iowa to determine their low-temperature cracking resistance and recommends performance criteria adjustments to state specifications based on the results.

These recommended performance criteria adjustments to the state specifications will ultimately reduce maintenance costs and improve the service life of Iowa pavements.

### **Conclusions and Recommendations**

Performance criteria adjustments and a pavement distress survey are recommended to ensure that field-produced mixtures meet design specifications from the laboratory to the field.

- The specification on the need for a DCT test should be revised to state that the test is required when the asphalt binder replacement exceeds 15% for mixtures with recycled asphalt pavement (RAP) and reclaimed asphalt shingles (RAS), rather than the current value of 30% and 25% binder replacement, respectively.
- Since most of the pavements have shown that cracking resistance is low during service life, there is a need for revising the specification or improving the quality-control process, just as the Minnesota DOT (MnDOT) has allowed a 50 J/m<sup>2</sup> range for quality assurance.

- A pavement distress survey is recommended that focuses more on the intensity of thermal- and transverse-cracking distress over the years to assess the field performance of the pavements used in this study in relation to the DCT testing results.



## CHAPTER 1. INTRODUCTION

### Background Information

In cold regions of North America (northern US and Canada), the main distress observed in asphalt pavements is low-temperature cracking or thermal cracking. At very low temperatures, the top layer of asphalt concrete undergoes shrinking. However, the top layer is constrained because of friction occurring between itself and an underlying layer of asphalt concrete. This is the action by which thermal-induced tensile stresses are produced. As the temperature decreases, the thermal-induced tensile stress increases, and once it exceeds the pavement tensile strength, the asphalt concrete pavement cracks.

Current Superpave specifications address thermal cracking at low temperatures based on creep and strength testing of asphalt binders and mixtures, but it only has limiting criteria set forth in the asphalt binder specifications like the bending beam rheometer (BBR) test. In addition, these low-temperature characterization methods do not take into account the effect from the aggregate phase of the mixture. Mix test specifications consider the effect from both binder and aggregate. However, mix test specifications do not have clearly set national limits in Superpave; they are set by individual state agencies. The aggregate phase makes up 90% to 95% of the total weight of a typical asphalt concrete mixture. To address the impact of the aggregate phase on low-temperature cracking in asphalt mixtures, a fracture mechanics-based approach is necessary. The following low-temperature cracking/fracture mix tests have been used by researchers and state departments of transportation (DOTs) within the Midwestern US:

- Semi-circular bend (SCB)
- Illinois Flexibility Index Test (I-FIT)
- Disk-shaped compact tension (DCT)

The SCB test has become favored by industry due to the ease of fabrication and that it is reproducible. Two specimens can be obtained from one field core, reducing the number of cores to be obtained from the field (Wagoner et al. 2005a). The I-FIT has been found to be more effective at differentiating effects due to design factors and mixture aging than fracture energy ( $G_f$ ) by itself. The flexibility index (FI) is calculated using  $G_f$  and post-peak slope (Rivera-Perez et al. 2018). The DCT test can be used with field cores that have already undergone dynamic modulus and creep compliance testing. Additionally, the geometry maximizes the potential fracture area, which reduces statistical variability of the data obtained (Wagoner et al. 2005a).

### Research Objective

Durability and performance of pavements is one of the important aspects of design, and they are achieved by understanding the design product. For low-temperature cracking, characterizing asphalt mixes helps to understand the pavement performance by understanding the fracture strength of different materials. Previously, binder characterization has been used; however, asphalt mixes are composed of approximately 95% other materials than the asphalt binder. To

avoid thermal cracking in the field, characterization of mechanical fracture of the asphalt mixture is important in predicting the pavement performance and assists the design engineer in establishing a mix design that can withstand the cold climate for the design period.

The objective of this study was to assess the low-temperature cracking resistance of asphalt mixtures used by the Iowa DOT and correlate the laboratory results with field performance. Based on the developed correlations, performance criteria for the DCT and SCB tests were proposed. The results were compared with what other states in the Midwest are doing.

### **Overall Report Experimental Plan**

A technical advisory committee (TAC) was formed that consisted of representatives from Iowa DOT, local agencies, and industry professionals. A set of projects that represent typical mixtures and materials used by the Iowa DOT was identified for use in this study. DCT and SCB tests were used to evaluate the low-temperature cracking resistance of these mixtures.

### **Contents of this Report**

Chapter 1 introduces background information and the objectives of this study. Chapter 2 contains the literature review on low-temperature cracking,  $G_f$ , and the DCT, SCB, and I-FIT tests and their specifications, as well as what other states are doing. It also includes future recommended work. Experimental methods are covered in Chapter 3, while Chapter 4 presents the results and their analysis. Chapter 5 contains conclusions and recommendations on asphalt mix  $G_f$  characterization for design.



## CHAPTER 2. LITERATURE REVIEW

### Low-Temperature Cracking

Low-temperature cracking occurs when stress buildup from thermal contraction surpasses pavement tensile strength due to sudden temperature drop and/or repeated temperature fluctuation. The crack typically forms in a transverse direction on the pavement surface. Low-temperature cracking is affected by material, environment, and pavement-structure geometry (Kliwer et al. 1996). Thermal cracking is a distress that can compromise the structural integrity of the pavement (Behnia et al. 2018), and the primary concern about this distress is the infiltration of water into the pavement structure, which from a durability standpoint increases the rate of moisture and leads to earlier asphalt concrete deterioration. More so, water infiltration promotes pumping of the underlying unbound material, causing depression at the thermal cracks. Ice lenses could also form beneath a thermal crack and in turn would cause tenting of the crack edge (Marasteanu 2007).

Thermal cracks are categorized into two types of events: (1) single-event thermal cracks that occur due to fast cooling, e.g., a drop in temperature from  $-10^{\circ}\text{C}$  to  $-40^{\circ}\text{C}$  in a span of 24 hours, and (2) thermal-fatigue cracking that can develop due to several cooling cycles and daily temperature fluctuation. There have been great research efforts directed toward characterization and prevention of thermal cracks in pavement, and this has led to the development of mixture-based thermal-cracking performance evaluation tools such as the DCT test, SCB test, and the use of the combination of stiffness and relaxation properties of asphalt mixtures in black space to limit thermal stresses (Oshone et al. 2018).

$G_f$  is an asphalt mixture fracture parameter that recent studies have identified to have a correlation with thermal-cracking resistance. It is defined as the work that is required to cause a unit square ( $\text{m}^2$ ) crack to form in a laboratory test specimen. The  $G_f$  is affected by aggregate type, test temperature, the addition of recycled material, and air voids of the mix (Wagoner et al. 2005b, Li et al. 2010). High  $G_f$  indicates that the pavement has high tensile strength and thus can dissipate tensile stress buildup more easily in the pavement at low temperatures when the pavement is under loading.

Oshone et al. (2018) reported a positive correlation between  $G_f$  and properties that include effective binder content, asphalt film thickness, voids in mineral aggregate (VMA), performance-grade high temperature, and performance-grade spread. A good gradation of material ensures adequate VMA and thus sufficient binder. The voids filled with asphalt (VFA) and VMA are critical in mixture crack resistance and durability. Lowering VMA lowers the binder content for that specific air void content and leads to a more economical mixture but less durability.

Fracture temperature, or the critical cracking temperature, is an important aspect of thermal-crack resistance of a pavement. It is a function of the cooling rate and the temperature at which cooling starts and is affected by asphalt type and degree of aging. Warmer starting temperatures shift the cracking temperature (Mensching et al. 2014). The most frequent actual cooling rate in the field is  $1^{\circ}\text{C}$  to  $2^{\circ}\text{C}$  per hour. An increase in cooling rate results in an increase in the fracture

temperature. The cooling rate is the temperature drop per unit of time. Most tests have been conducted at a cooling rate of 10°C per hour by investigators; however, field cooling rates are slower than 10°C (Jung and Vinson 1994). Faster cooling rates cause quicker thermal stress buildup and material cracking at a warmer temperature due to the material lacking time to relax (Mensching et al. 2014).

Hot-mix asphalt (HMA) is designed to resist deterioration due to exposure to traffic and environmental loads. Different HMAs are chosen depending on traffic level and geological location, which influence the variability of mixture components such as binder grade and aggregate. Sustainability is one concern of engineers, and this has led to the use of recycled material as a part of pavement construction, as the milled material is reused as 30% of the asphalt components. This, in turn, has an impact on pavement performance, particularly on distress resistance. An asphalt mixture's fracture and viscoelastic properties play a significant role in controlling the ability of the mixture to limit thermal stress and maintain material integrity as the stress approaches the material stress capacity (Oshone et al. 2018).

Dave et al. (2016) recommended the critical selection of asphalt binder for use and argued that the use of asphalt binder with a low-temperature limit warmer than the required grade can shorten the pavement life significantly. They further strongly recommended the use of performance-based specifications that apply laboratory-mix performance tests. Additionally, the oxidative aging effects of the asphalt binder should be considered while determining asphalt crack resistance.

Hoare and Hesp (2000) state that for a pavement to fail at low temperatures, there has to be either poor material selection or an inadequate testing procedure. An understanding of the fundamental failure mechanisms and other material properties that facilitate crack growth at low temperatures is important.

Behnia et al. (2011) observed that the  $G_f$  of an asphalt mixture containing a virgin binder (PG 58-28) was drastically reduced when the recycled asphalt pavement (RAP) amount within the mix gradation exceeded 10%. While the  $G_f$  of mixtures containing virgin binder PG 64-22 initially increased with an increase in RAP amount up to 30%, any increase in RAP amount over 30% decreased the  $G_f$ . Using a different aging procedure, the study also indicated that the fracture energies of the asphalt mixtures increase with aging levels to a peak level where the fracture energies dropped with further aging. Behnia et al. pointed out that this trend will vary from mixture to mixture, between RAP sources, and from varying binder sources.

Marasteanu (2007) in the first phase of a national pooled fund study recommended the critical need for an asphalt mixture specification. Further, it was pointed out that the  $G_f$  of the asphalt mixture is a better parameter to identify an asphalt mixture's low-temperature cracking susceptibility compared to the  $K_{IC}$ . The reason for this being that  $G_f$  depends less on the conditions of linear elasticity and homogeneity of the tested materials.

In the second phase of the low-temperature cracking national pooled fund study, Mihai et al. (2012) proposed a thermal-cracking specification for asphalt mixtures; based on DCT results, a

minimum  $G_f$  of  $400 \text{ J/m}^2$  was suggested for protection against thermal cracking. Additionally, based on SCB results, a testing value of  $400 \text{ J/m}^2$  was suggested too. These suggested values were determined through a correlation of the fracture data and field thermal cracking. The DCT test was recommended to be included as a requirement in the low-temperature thermal-cracking mix performance-based specification.

The outcome of the studies that determined the correlation has been that many agencies have identified  $400 \text{ J/m}^2$  as the passing criteria for mixes tested at the low-temperature grade of the asphalt binder for the DCT test (Mihai et al. 2012). In Iowa, the DCT test is the method used for low-temperature cracking performance of asphalt mix. The criteria established by the Iowa DOT is  $400 \text{ J/m}^2$ ,  $460 \text{ J/m}^2$ , and  $690 \text{ J/m}^2$  for traffic levels of standard traffic, heavy traffic, and very heavy traffic, respectively. Dave et al. (2016) concluded that a variation of  $25 \text{ J/m}^2 G_f$  is enough to show a difference in cracking performance.

In a study by West et al. (2018), Iowa was among the states that use the balanced mix design approach, one which is Volumetric Design with Performance Verification. At the time of study, only Iowa, Minnesota, and Missouri required a thermal-cracking test in their mix design specifications, and they used the DCT. In the study, it was noted that lowering the number of design gyrations ( $N_{\text{design}}$ ) will result in an increase in the optimum asphalt content if aggregate gradation is fixed. Their recommendation was to reduce the  $N_{\text{design}}$  level by 20% to 25% depending on the design traffic (West et al. 2018).

The Minnesota DOT (MnDOT) has implemented DCT testing as a requirement to ensure the thermal-cracking resistance of asphalt mixtures at design and production. Additionally, a  $G_f$  limit has been established in its specification. The minimum  $G_f$  during mix design is  $450 \text{ J/m}^2$  for traffic levels 1, 2, and 3 and  $500 \text{ J/m}^2$  for traffic levels 4 and 5. For quality assurance, the  $G_f$  is reduced by  $50 \text{ J/m}^2$  to values of  $400 \text{ J/m}^2$  for traffic levels 1, 2, and 3 and  $450 \text{ J/m}^2$  for traffic levels 4 and 5 (Oshone et al. 2018).

The SCB test has been used to evaluate the factors that affect  $G_f$ , and these factors were identified to be aggregate type, air voids content, modifier type, and the binder type (Li et al. 2010). Different aggregate requires different amounts of energy for them to crack, and this compounds the total mixture crack resistance. More energy is needed to break a denser asphalt mixture. Li et al. in their research indicated that asphalt modified with different modifiers had different  $G_f$  for the same type of mixture. SCB has also been used to determine the effect of testing configuration on semi-circular bending fracture of asphalt mixture (Nsengiyumva and Kim 2019).

Rivera-Perez et al. (2018) in a study indicated that the FI is an indicator of ductility of the mixture but should be balanced with the stiffness and strength of the mixture. An increase in FI is associated with additional inelastic mechanisms (i.e., plasticity and viscoelasticity) of energy dissipation away from the crack front, which may delay fracture initiation and propagation. The results considered for correlations were those with 8% air void content and below; at 10% air void, the fracture test specimen experiences a high level of non-fracture-related energy

dissipation. However, correction factors proposed by Barry (2016) could be used to correct for the air void content variation.

### **SCB Test and I-FIT**

The SCB test is an HMA fracture test used at low temperatures. Recently, the SCB test has become favored among researchers, because specimen fabrication is simple and easily reproducible using both standard laboratory-compacted or field-cored asphalt concrete samples. Within this test, two fracture modes can be studied: Mode I or Mode II. The fracture mode depends on the initial notch orientation. For low-temperature tests, such as the Illinois Test Procedure 405 (I-FIT) developed by researchers from the University of Minnesota–Twin Cities and the University of Illinois–Urbana-Champaign and the SCB test according to AASHTO TP 105-13 (both shown in Figure 1), Mode I fracture is used for specimen preparation, testing, and analysis.



**Figure 1. I-FIT SCB test, left, and AASHTO TP 105-13 SCB test, right**

$G_f$ , fracture toughness ( $K_{IC}$ ), and stiffness ( $S$ ) are the parameters determined using the SCB test results according to AASHTO TP 105-13, while the parameters determined using the I-FIT protocol are  $G_f$  and FI (Test- 2007, Li et al. 2010, Marasteanu et al. 2012, Hill et al. 2013, Illinois Test Procedure 405 2016).

The SCB test method for low-temperature cracking was developed due to specifications utilizing only binder tests such as the BBR and direct tension tester (DTT) for characterization of low-temperature performance. These test methods do not include the response from the aggregate phase, even though the aggregate phase makes up 90% to 95% of the total weight of a typical asphalt concrete mixture. To address the impact of the aggregate phase on low-temperature cracking in asphalt mixtures, AASHTO TP 10-13 was developed. Testing takes place at both 10°C above the low-temperature binder grade and 2°C below the low-temperature binder grade. A vertical compressive load is applied at the top of each specimen, so a constant crack mouth opening displacement (CMOD) of 0.00002 in./s (0.0005 mm/s) is achieved. The parameter  $G_f$  is determined as the area under load-CMOD curve, while toughness and stiffness are determined using load and load line displacement (LLD) results recorded for each tested specimen.

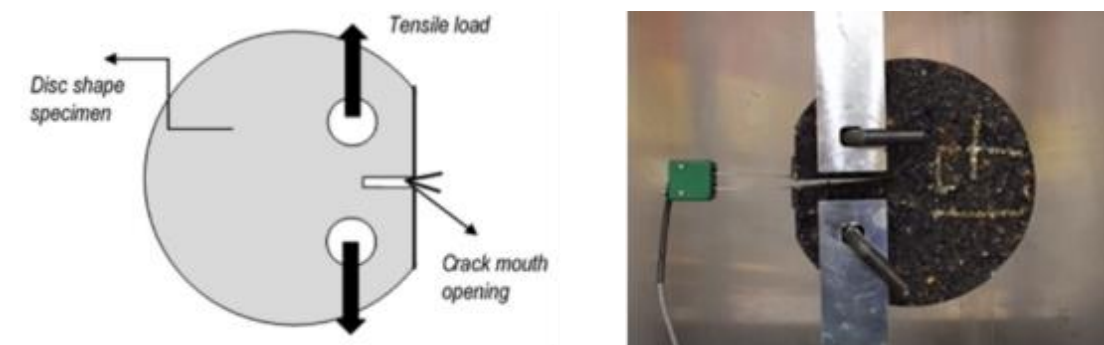
The I-FIT was developed to screen out potentially poor-performing mixtures with high amounts of RAP and reclaimed asphalt shingles (RAS) and correlates well to field results and other cracking tests, while still being practical and easily repeatable (Ozer et al. 2016, Rivera-Perez et al. 2018). In contrast to other SCB tests done at low temperatures, the I-FIT includes  $G_f$  and post-peak behavior in the determination of the FI, which has been found to be more effective at differentiating effects due to design factors and mixture aging than  $G_f$  by itself (Barry 2016).

Testing takes place at 25°C with a loading rate of 2 in./min (50 mm/min). Currently, the Illinois DOT has set the minimum criteria for FI at 8, but the I-FIT and FI parameter need to be further calibrated to different traffic levels, climates, mix types, and applications. Further, there are concerns that with the 25°C test temperature for the I-FIT that this does not comply with the principles of fracture mechanics. This is because the test specimens undergo deformation on the millimeter to centimeter scale prior to completion of cracking, and thus the test violates the small-scale yielding condition, so the samples would need to be much larger, e.g., on the scale of meters in diameter.

### DCT Test

To examine the fracture mechanics of asphalt concrete at low temperatures, the DCT test is of key interest. The DCT test has received favorable reviews because of its many advantages; the test can be used with field cores that have already undergone dynamic modulus and creep compliance testing, and specimens can be reproduced consistently for use in Mode I fracture testing (Wagoner et al. 2005c, T 322 2007, Test- 2007, Hill et al. 2012, 2013). This test is used to determine the  $G_f$  (Wagoner et al. 2005a, Zofka and Braham 2009, Hill et al. 2013).

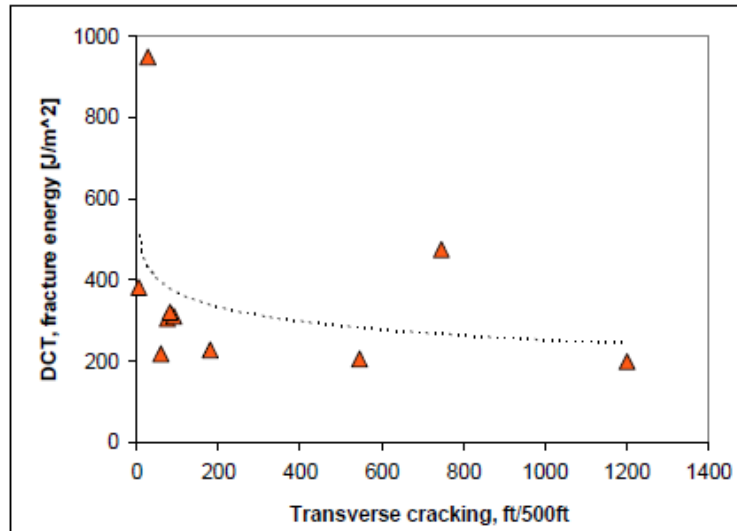
For the DCT test, a circular specimen with a single edge notch is subjected to tension as shown on the left in Figure 2.



**Figure 2. Schematic of DCT test, left, and clip gauge attached to buttons, right**

In this setup, a tensile load is applied at the top and bottom of each specimen to produce a constant CMOD with a constant rate of 0.0007 in./s (0.017 mm/s). An epsilon clip gauge as shown on the right in Figure 2 is used to measure the CMOD. The clip gauge is placed between two buttons that are glued to the flat face of the specimen. The  $G_f$  is determined through load and fitted CMOD results.

The outcomes of the two-phase national pooled fund study on low-temperature cracking (Mihai et al. 2012) identified the relationship between the amount of transverse cracking of field pavements and the  $G_f$  of cores from these pavements (Figure 3).



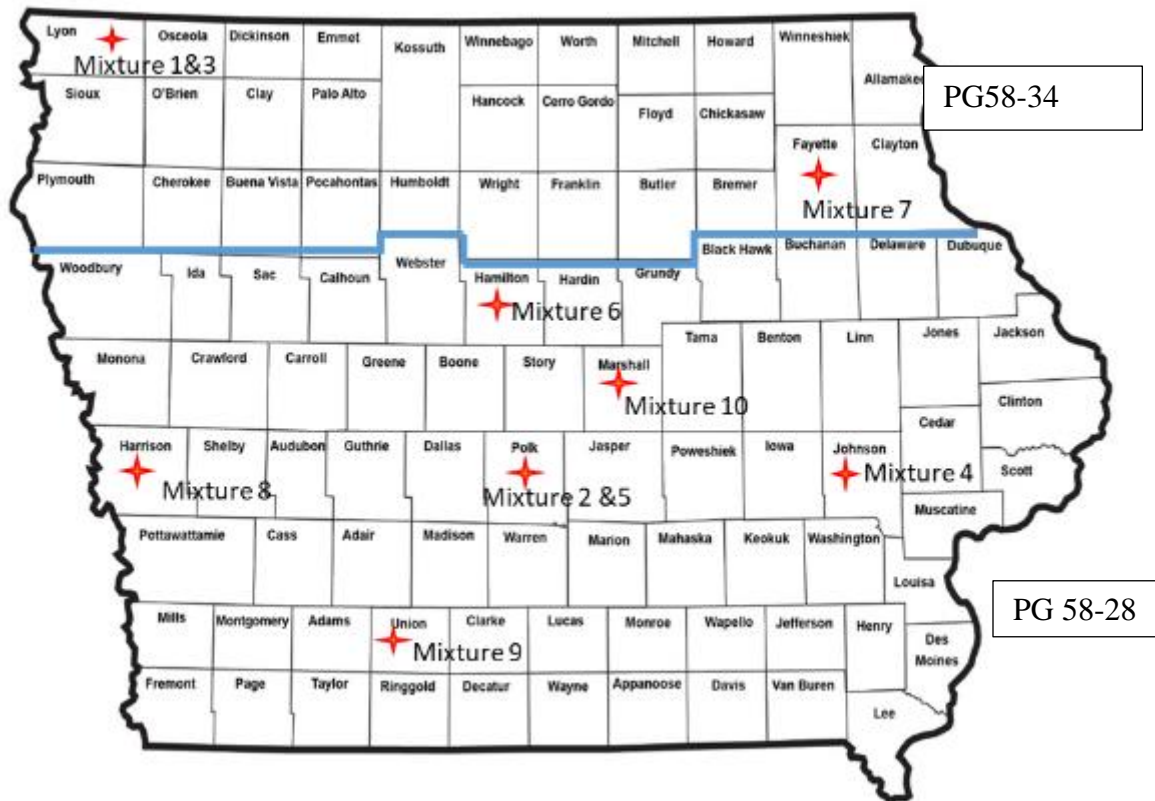
Marasteanu et al. 2012

**Figure 3. Relationship between transverse cracking and DCT  $G_f$**

## CHAPTER 3. EXPERIMENTAL METHODS AND MATERIALS

### Materials

Ten field-produced asphalt mixtures were obtained from projects located in Iowa that represented typical asphalt mixtures used in Iowa. The mixtures were from Fayette, Hamilton, Harrison, Johnson, Lyon, Marshall, Polk, and Union counties. Figure 4 shows the mixture locations, representing five of the six Iowa DOT districts.



**Figure 4. Mixture locations and regional recommended Project I type binder grade in Iowa**

Note that Project I types are full depth hot-mix asphalt, HMA + cold in-place recycling, HMA + rubblization, HMA + crack and seat HMA overlay >4 in., and HMA + full-depth reclamation (FDR).

Five mixtures were from the old design, and the other five mixtures were from the new design. The mixtures had different binder grades and aggregate gradation, VMA, VFA, binder content, and varying percentage of the recycled material as shown in Table 1.

**Table 1. Mixture properties**

<b>Mix</b>	<b>Year</b>	<b>Binder type</b>	<b>Binder content</b>	<b>VMA</b>	<b>VFA</b>	<b>AFT</b>	<b>Recycled material % in mix</b>	<b>Traffic level</b>	<b>District</b>
1	2013	PG58-28	5.33	16.7	76.1	10.84	11% RAP, 4% RAS	High	3
2	2014	PG64-22w/hG	5.28	16.8	76.1	10.22	9.5% RAP, 5% RAS	High	1
3	2013	PG58-28	5.33	16.7	76.1	10.84	5% RAP, 4% RAS	High	3
4	2013	PG64-28	4.49	13.2	69.7	8.43	12% slag, 34% RAP	High	6
5	2014	PG58-28	5.48	16.8	76.1	10.22	9.5% RAP, 5% RAS	High	1
6	2018	PG58-28V	4.75	13.9	71.2	9.3	19% RAP	Very high	1
7	2018	PG58-34H	5.34	14.4	72.3	9.85	15% RAP	High	2
8	2018	PG58-28S	5.89	14.7	72.7	8.71	-	Standard	4
9	2018	PG58-28H	5.36	15.3	73.8	14.45	15% RAP	High	4
10	2018	PG58-28S	5.02	14	71.3	8.74	17% RAP	Standard	1

Note: AFT = Asphalt film thickness



Figures 5 and 6 show the gradations of both the old design and the new Ndesign mixtures used in this project.

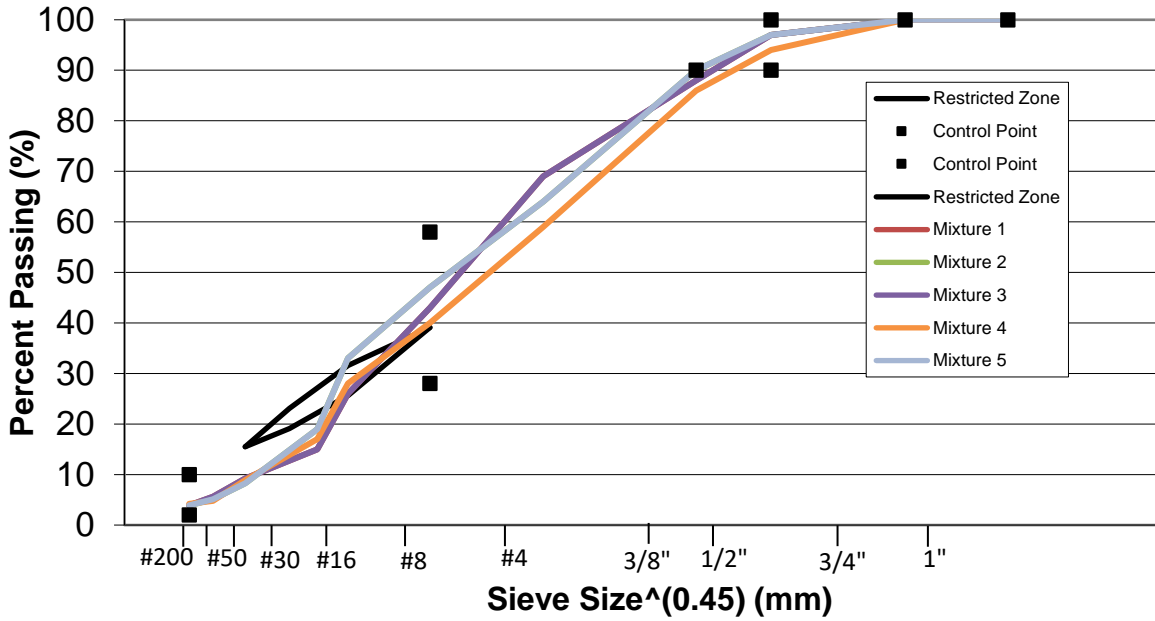


Figure 5. Old Ndesign aggregate mix gradations

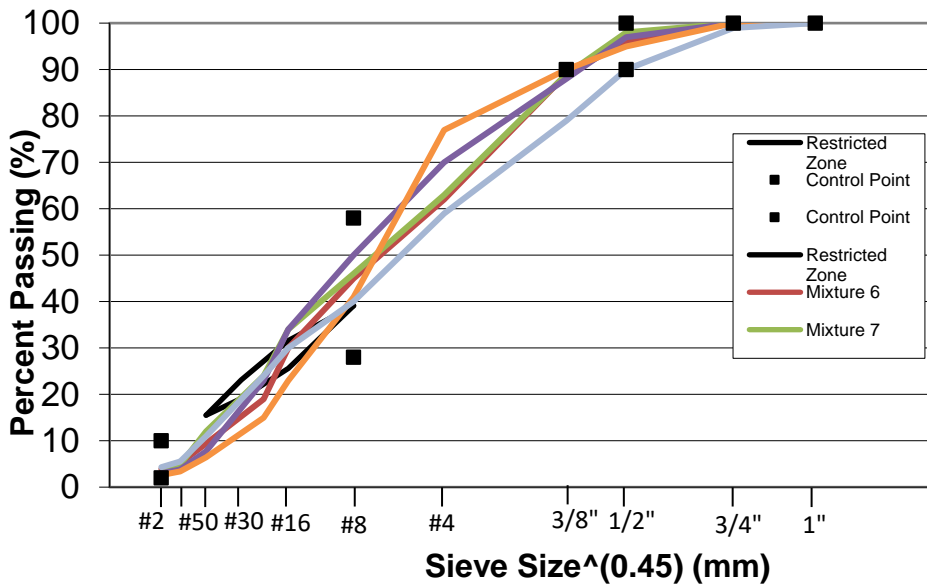
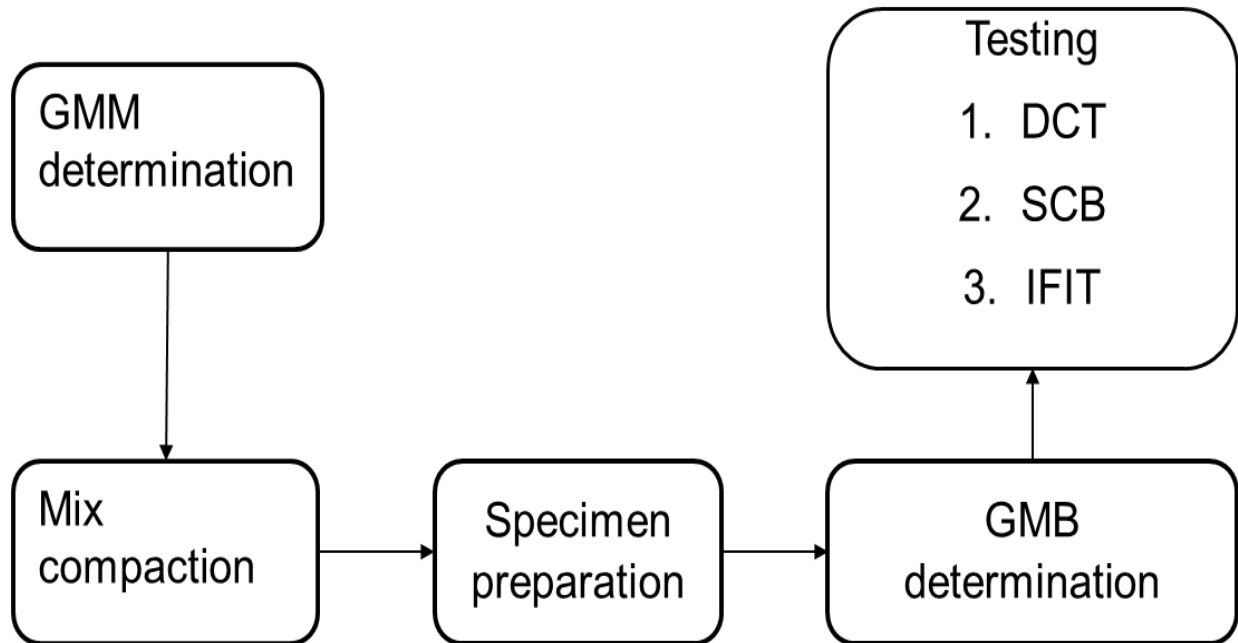


Figure 6. New Ndesign aggregate mix gradations

For the aggregate gradations, most of the aggregate sizes are in the range of 0.04 in. (1 mm) to 0.5 in. (12.5 mm). Although the Ndesign involves lowering the number of design gyrations, this was not evident between the old and new Ndesign gradation as there were not significant differences between asphalt content when lowering gyration levels based on traffic level design.

## Methods

The overall test plan is shown in Figure 7.



**Figure 7. Test plan**

Theoretical maximum specific gravity ( $G_{mm}$ ) was determined using AASHTO T 209-12. The loose mixtures were heated to 90°C, the conglomerates were separated to form fine particles of 0.25 in. (6 mm,) and the process was carefully done to prevent fracture of the aggregate. After cooling, 2,500 grams from the mixtures were measured per mix. Using the  $G_{mm}$  test container, the weight of the sample and container were recorded, as well as the weight of the container immersed in a water bath. Water was added to cover the sample in the vacuum equipment; a vacuum between 1 in. (25.5 mm) and 1.2 in. (30 mm) of mercury was applied. During the vacuum period, the container and the contents were agitated using a mechanical vibratory device. After 15 minutes, the sample was immersed in a water bath for 5 minutes, and the weight was recorded; the  $G_{mm}$  was then calculated.

The samples were cut to achieve the configuration specified for each test. Water was used while cutting to cool the saw and to wash away small particles to prevent smearing. A bulk specific gravity ( $G_{mb}$ ) test of the specimen was carried out following ASTM D2726. The samples were left to dry after cutting, and their dry weights were recorded. Each sample was then immersed in water for 5 minutes, and the immersed weight was recorded; the sample was then removed from

the water, and the surface wiped with a damp towel to achieve saturated surface dry condition. They were then weighed, and the weight recorded. The  $G_{mb}$  was then calculated.

The specimen air voids were calculated using the obtained  $G_{mm}$  and  $G_{mb}$  to identify the specimen that met the required air void criteria of  $7\% \pm 0.5\%$  to be used for DCT, SCB, and I-FIT tests. To determine the fracture energies of the compacted sample, specimen preparation was done following ASTM and AASHTO specifications for the respective tests. They were conditioned for minimum of two hours at the test temperature, and then DCT, SCB, and I-FIT were carried out, and four replicates were used per mix per test.

## **DCT**

The DCT tests were carried out in accordance with ASTM D7313-13. The different mixture specimens were tested at  $10^{\circ}\text{C}$  higher than the lower limit temperature of the performance grade, i.e., for PG 64-22, the samples were tested at  $-12^{\circ}\text{C}$ , and most of the samples were tested at  $-18^{\circ}\text{C}$ . A  $0.04 \text{ in./min}$  ( $1.0 \text{ mm/min}$ ) rate of CMOD was used. Continuous load and CMOD were measured and recorded using the test computer, and a plot of load-CMOD was also obtained.  $G_f$  is computed as the area under the load-CMOD curve; the equipment used calculated the  $G_f$  value immediately when the specimen fails under loading.

## **SCB**

Following AASHTO TP 105-13 (2015), the SCB tests were carried out with a constant CMOD of  $0.00002 \text{ in.}$  ( $0.0005 \text{ mm}$ ) to ensure the crack growth condition is stable at  $10^{\circ}\text{C}$  higher than the PG lower limit. LLD was measured and recorded using universal testing machine (UTM) equipment. MATLAB was used to plot load and LLD, and  $G_f$  was calculated as the area under load-LLD curve.

Table 2 shows a sample of the raw data obtained from an SCB test of one of the mixtures.

**Table 2. Sample of SCB raw data of one sample as obtained during the test**

<b>Time (seconds)</b>	<b>CMOD (mm)</b>	<b>Load (KN)</b>	<b>Stroke (mm)</b>	<b>LLD (mm)</b>	<b>Ext (mm)</b>	<b>Temp (°C)</b>
0	4.3736	-0.005	-18.419	9.554	0.005	-18
0.1	4.3742	-0.011	-18.424	9.56	0.006	-18
0.2	4.3738	-0.005	-18.417	9.562	0.005	-18
0.3	4.3731	-0.002	-18.409	9.557	0.004	-18
0.4	4.3736	-0.003	-18.412	9.564	0.005	-18
0.5	4.3736	0.001	-18.406	9.566	0.005	-18
0.6	4.374	0.006	-18.398	9.575	0.005	-18
0.7	4.3741	0.013	-18.391	9.585	0.005	-18
0.8	4.3739	0.019	-18.386	9.588	0.005	-18
0.9	4.3738	0.026	-18.383	9.59	0.004	-18
1.0	4.3744	0.039	-18.377	9.598	0.005	-18
1.1	4.3748	0.059	-18.373	9.603	0.006	-18
1.2	4.3743	0.05	-18.369	9.599	0.005	-18
1.3	4.3757	0.061	-18.367	9.609	0.007	-18
1.4	4.3741	0.058	-18.351	9.592	0.004	-18
1.5	4.374	0.044	-18.35	9.592	0.004	-18

**I-FIT**

The I-FIT was used for the intermediate warmer temperatures and was carried out as per Illinois Test Procedure 405 (2016). The specimens were conditioned at 25°C. A loading rate of 2 in./min (50 mm/min) was applied constantly for the duration of test. Similar to SCB testing, the load and LLD were measured, and the  $G_f$  was calculated as the area under load-LLD curve, and this value was further used to calculate the FI.

Table 3 shows a sample of the raw data obtained from an I-FIT of one of the mixtures.

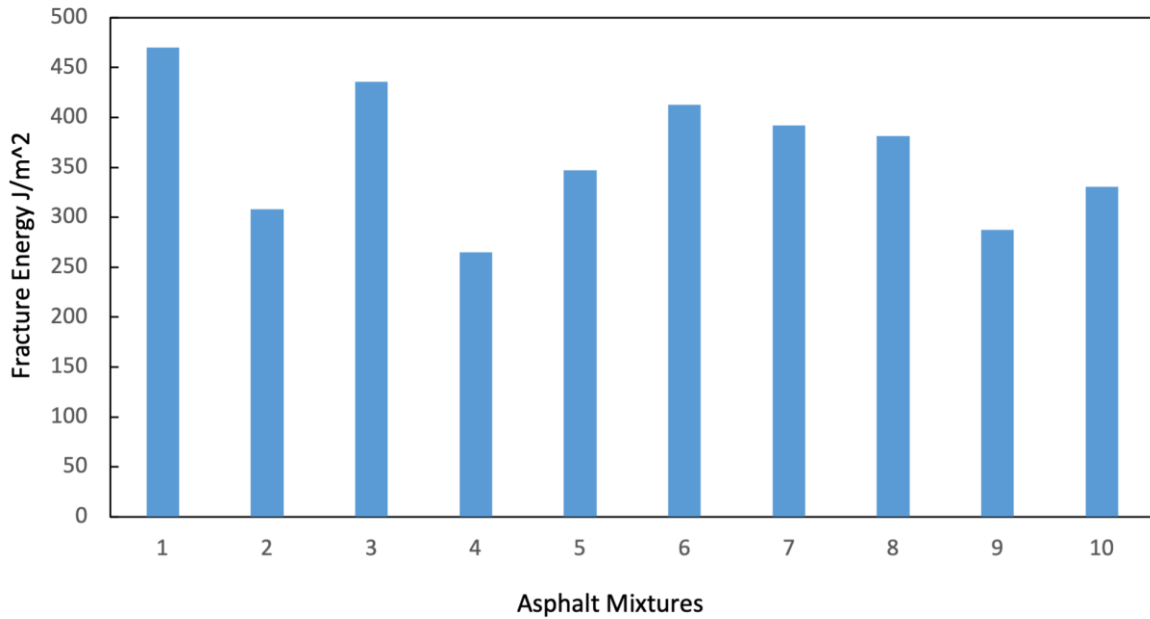
**Table 3. Sample of I-FIT raw data of one sample as obtained during the test**

<b>Point</b>	<b>Time (s)</b>	<b>Load (KN)</b>	<b>Displacement Channel 1 (mm)</b>	<b>Displacement Channel 2 (mm)</b>
1	0.000	0.08	0.000	0.000
2	0.025	0.11	0.008	0.010
3	0.050	0.27	0.029	0.036
4	0.075	0.47	0.050	0.060
5	0.100	0.68	0.070	0.084
6	0.125	0.89	0.090	0.105
7	0.150	1.11	0.110	0.129
8	0.175	1.33	0.131	0.152
9	0.200	1.55	0.150	0.176
10	0.225	1.78	0.170	0.198
11	0.250	2.02	0.191	0.223
12	0.275	2.25	0.213	0.248
13	0.300	2.46	0.232	0.270
14	0.325	2.67	0.252	0.295

## CHAPTER 4. TEST RESULTS

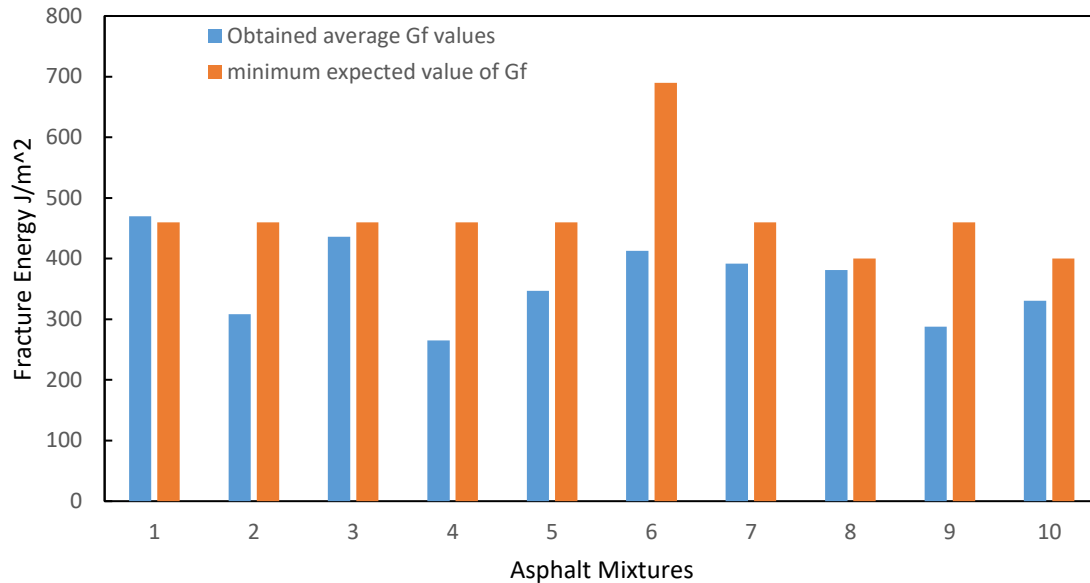
### DCT Results

The average  $G_f$  value ranged from 265.25 J/m<sup>2</sup> to 470.00 J/m<sup>2</sup> as shown in Figure 8.



**Figure 8. Average DCT fracture energies for the mixtures**

Mixture 1 is the only mixture that met the  $G_f$  value of the criteria it was designed for, having a  $G_f$  value of 470 J/m<sup>2</sup>, and it was designed for a minimum value of 460 J/m<sup>2</sup>. Mixtures 8 and 10 were designed for standard traffic, and they do not meet the specification of 400 J/m<sup>2</sup>, as they have  $G_f$  values of 381.25 J/m<sup>2</sup> and 330.50 J/m<sup>2</sup>, respectively. Mixtures 3 and 6 have  $G_f$  values that meet the criteria for standard traffic; however, they do not satisfy the specification for high traffic value of 460 J/m<sup>2</sup> as shown in Figure 9.

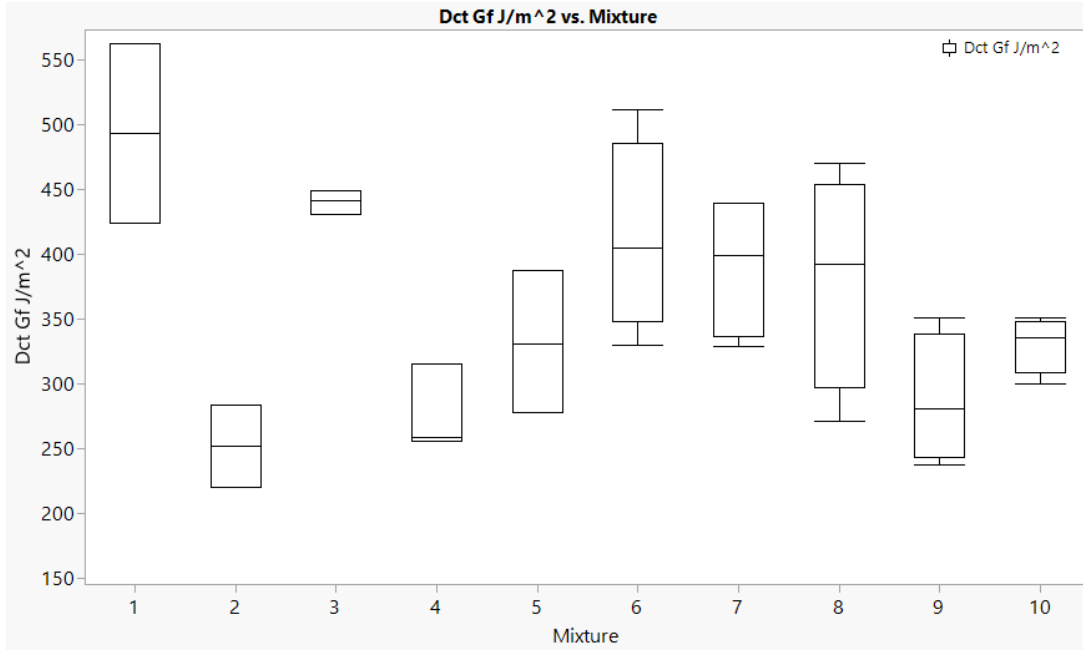


**Figure 9. Comparison of DCT  $G_f$  obtained to the expected minimum values as per the specification**

Mixtures 2, 4, 5, 7, and 9 did not meet their designed traffic specification minimum values nor the standard traffic specification value. Mixture 4 had the lowest fracture resistance, and the highest percentage of recycled material using slag; however, this does not mean the recycled material caused the low  $G_f$ , as other mixtures with no or little percentage of recycled material also did not have  $G_f$  values for the standard traffic specification. Mixtures 2 and 4 have 64°C as the upper temperature limit, and the  $G_f$  values obtained were lower than the other mixtures with a lower value of upper performance-grade temperature limit.

Mixture 3 had the lowest variance in the results followed by Mixture 10 and Mixture 4. Mixtures 2, 6, and 8 had the highest variance followed by Mixture 1, while Mixtures 5, 7, and 9 had variances between Mixture 4 and Mixture 7. The Ndesign for Mixtures 6 to 10 had DCT  $G_f$  mean values that were within a small range.

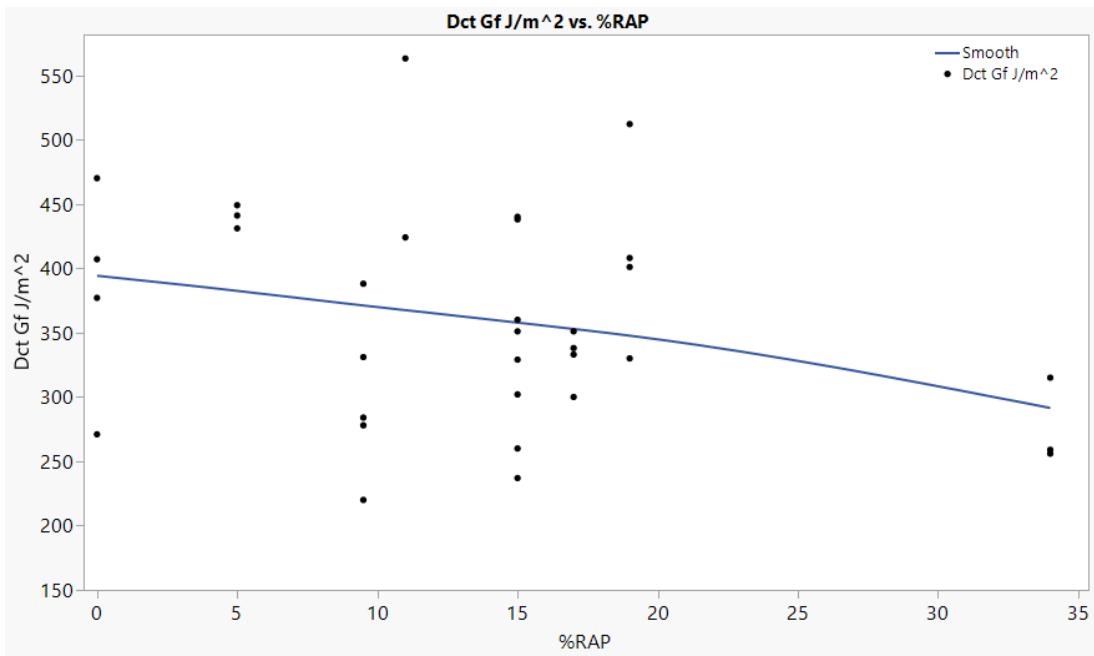
Figure 10 shows a box plot of the DCT test results for all 10 mixtures.



**Figure 10. Box plot of DCT results**

An increase in RAP caused a reduction in the DCT test fracture energies. This can be attributed to the fact that the RAP had binder that is old, and hence it's stiff and cannot resist fracture. As the binder ages, it exhibits less ductility and thus requires a small amount of energy to fracture.

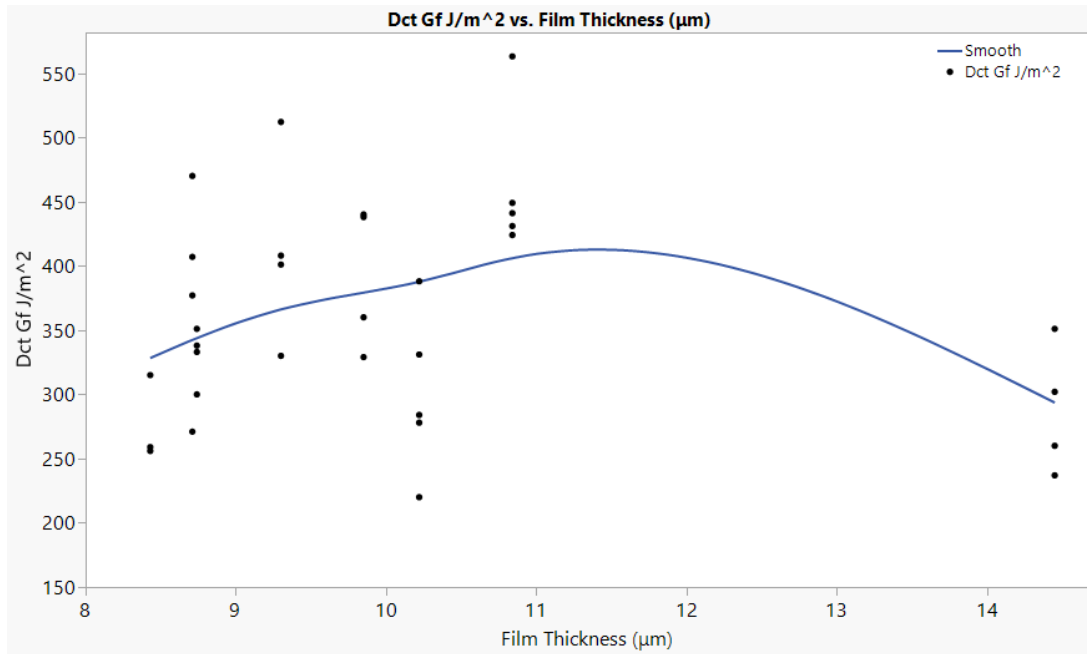
Figure 11 shows the effect of RAP on the  $G_f$  from the DCT results.



**Figure 11. RAP effect on DCT  $G_f$**



A high film thickness of the binder causes an increase in DCT fracture resistance up to an optimum value, after which the DCT  $G_f$  value decreases with an increase in film thickness. A sufficient asphalt content is required, just enough to coat the aggregates and bond them together. From the trend line shown in Figure 12, it is apparent that as film thickness increases, the  $G_f$  will increase, thus improving mix performance against low-temperature fracture.

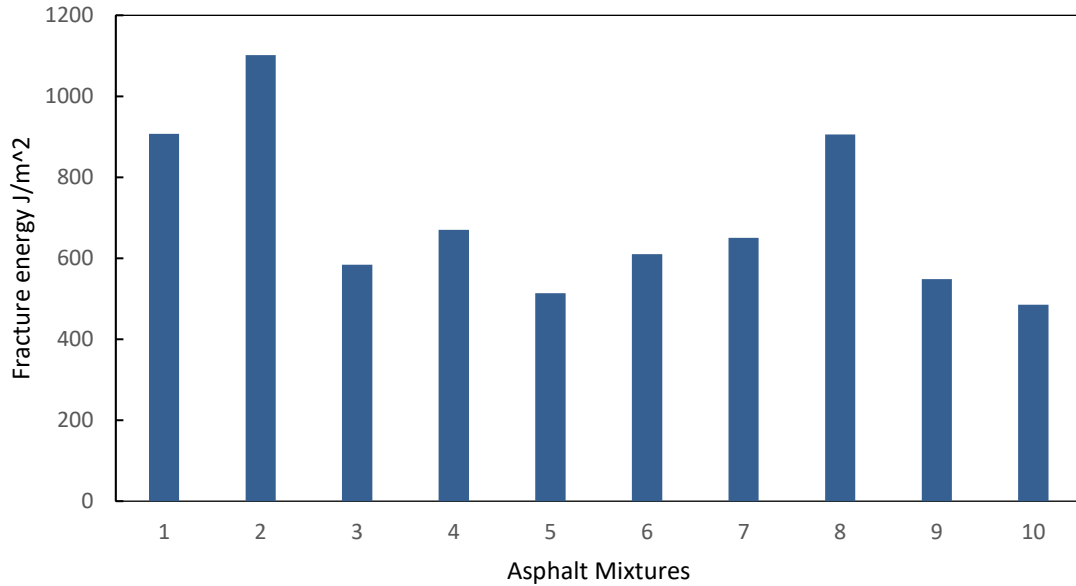


**Figure 12. Effect of film thickness on DCT  $G_f$**

However, when the film thickness became greater than 12 µm, as shown in the figure, performance decreased.

### SCB Results

The average  $G_f$  values from the SCB results ranged from 485 J/m<sup>2</sup> to 1,102 J/m<sup>2</sup>, as shown in Figure 13.

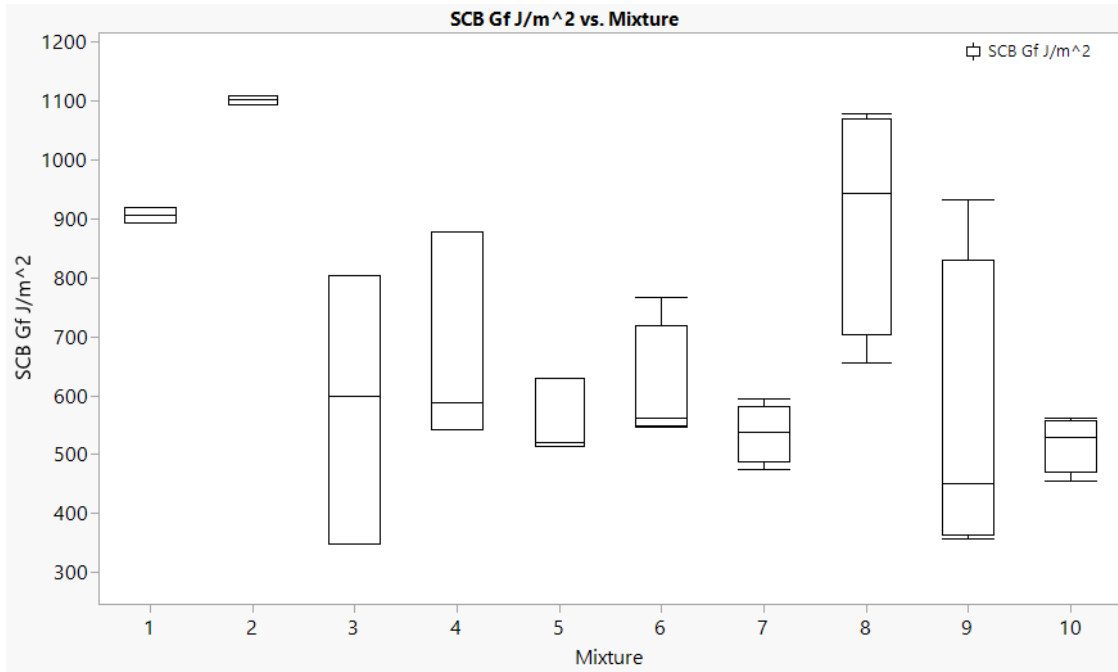


**Figure 13. Graph of average SCB  $G_f$  of the mixtures**

Mixture 2 had the highest SCB  $G_f$ , while it was among the low DCT  $G_f$  values. Mixture 1 had higher values for both DCT and SCB tests compared to the other mixtures. There was no trend noticed between SCB and DCT  $G_f$  values of the mixtures. This could be attributed to the differences in testing configurations of the specimens and the loading rate.

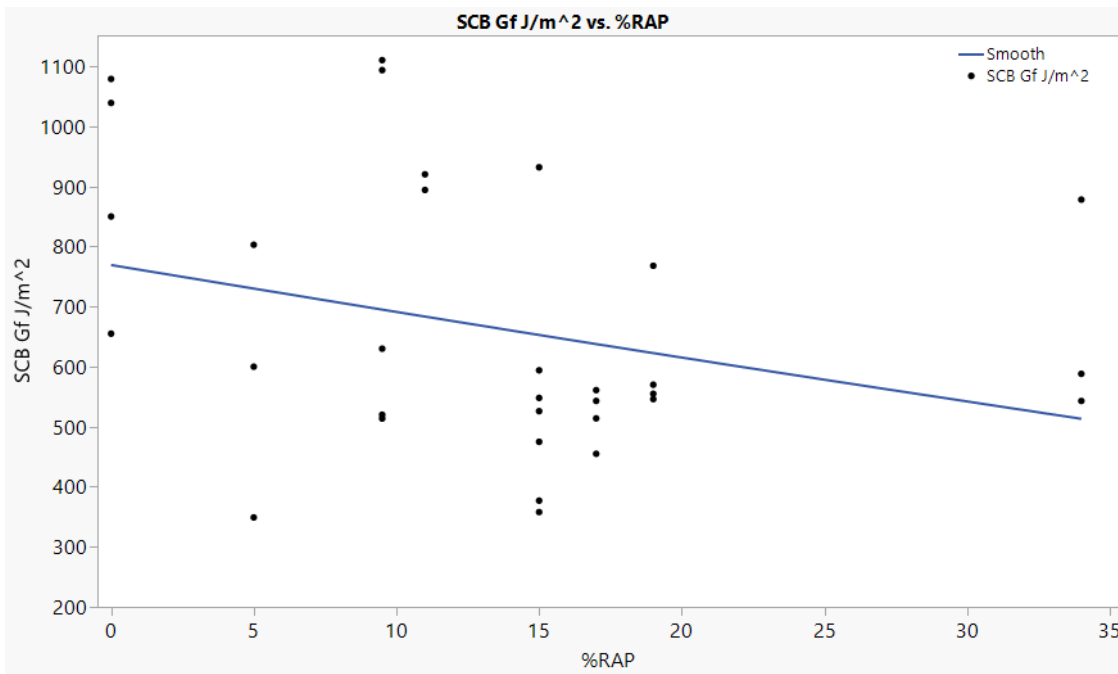
Mixture 10 had the lowest variance for SCB testing, of which this was also observed in the DCT results. Mixture 6 had the second lowest variance while Mixtures 7, 8, and 9 had the highest variance of the five mixtures. Mixtures 7 and 9 had outlier results, which were not used in calculating those mixtures' average mean fracture energies.

Figure 14 shows a box plot of the SCB test results for all 10 mixtures.



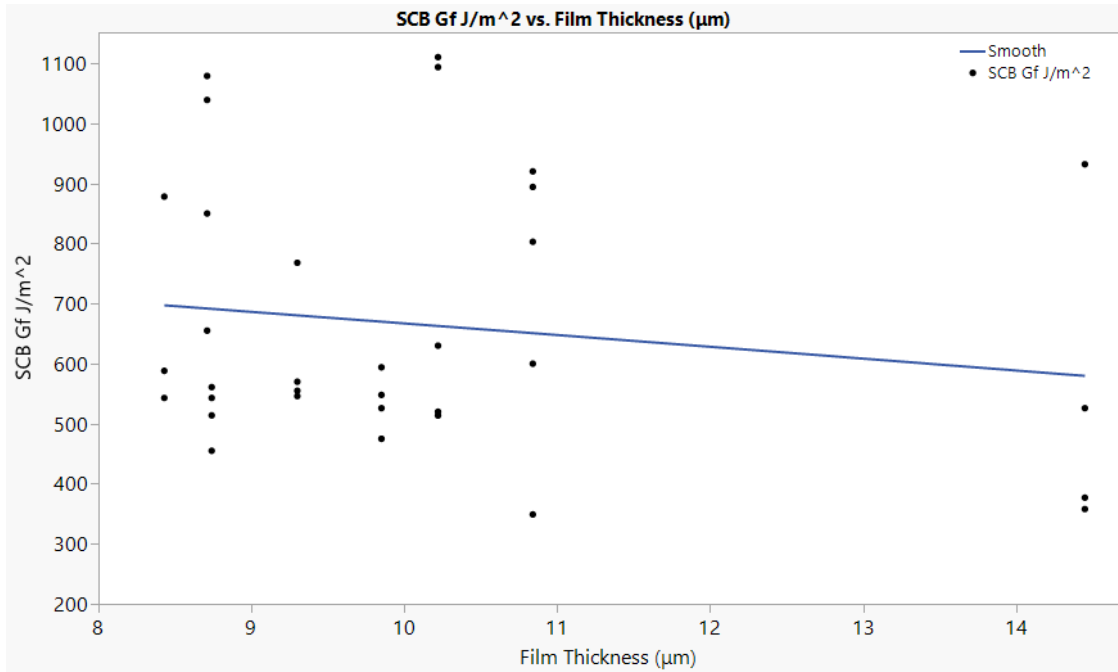
**Figure 14. Box plot of SCB G<sub>f</sub>**

An increase in RAP caused a decrease in the SCB G<sub>f</sub> as shown in Figure 15. This was also observed from the fracture energies of the DCT tests.



**Figure 15. Effect of RAP on SCB G<sub>f</sub>**

An increase in film thickness caused a decrease in SCB fracture energies (Figure 16).

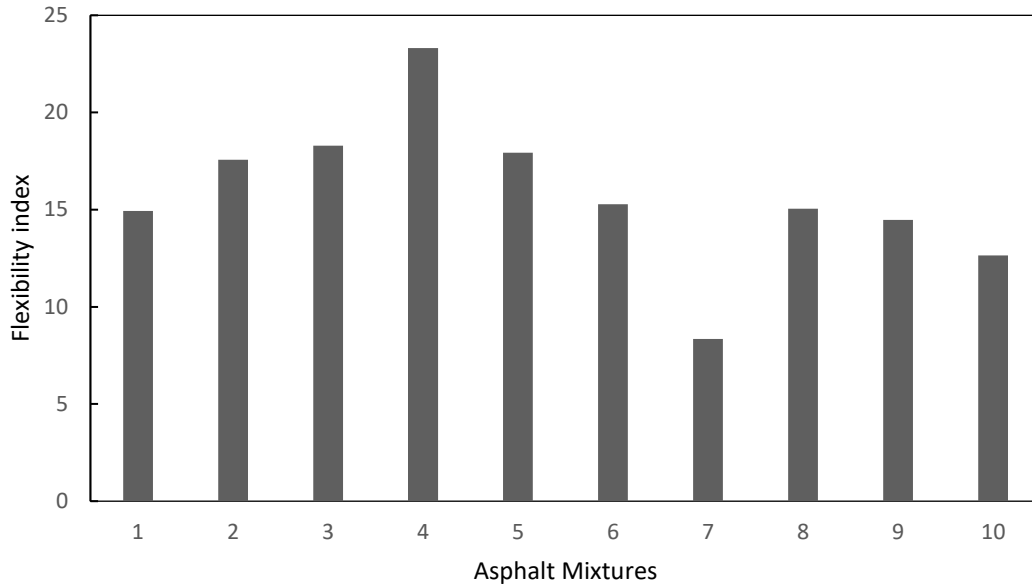


**Figure 16. Effect of film thickness on SCB Gr**

If asphalt is concentrated in the same point of the mixture, it gives a weak point for fracture and especially in low temperatures, as it becomes plastic; hence, low energy is needed to cause a crack.

### **I-FIT Results**

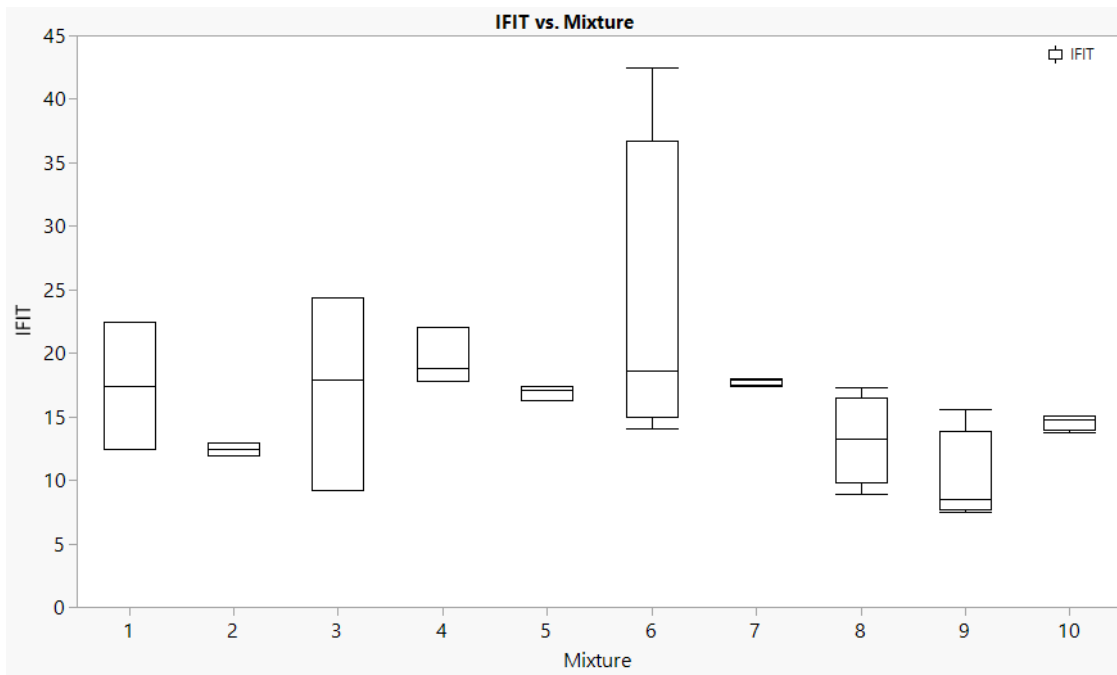
The FI was calculated from the  $G_f$  obtained during I-FIT testing (Illinois Test Procedure 405 2016). All FI values are about 8.0, which is the minimum recommended value for both HMA and stone-matrix asphalt (SMA) asphalt mixtures (Figure 17).



**Figure 17. Graph of average FI of the mixtures**

Mixture 7 had the lowest value of FI, and this could be related to the performance-grade lower limit temperature, which was lower than the other mixtures' performance-grade lower limit temperatures.

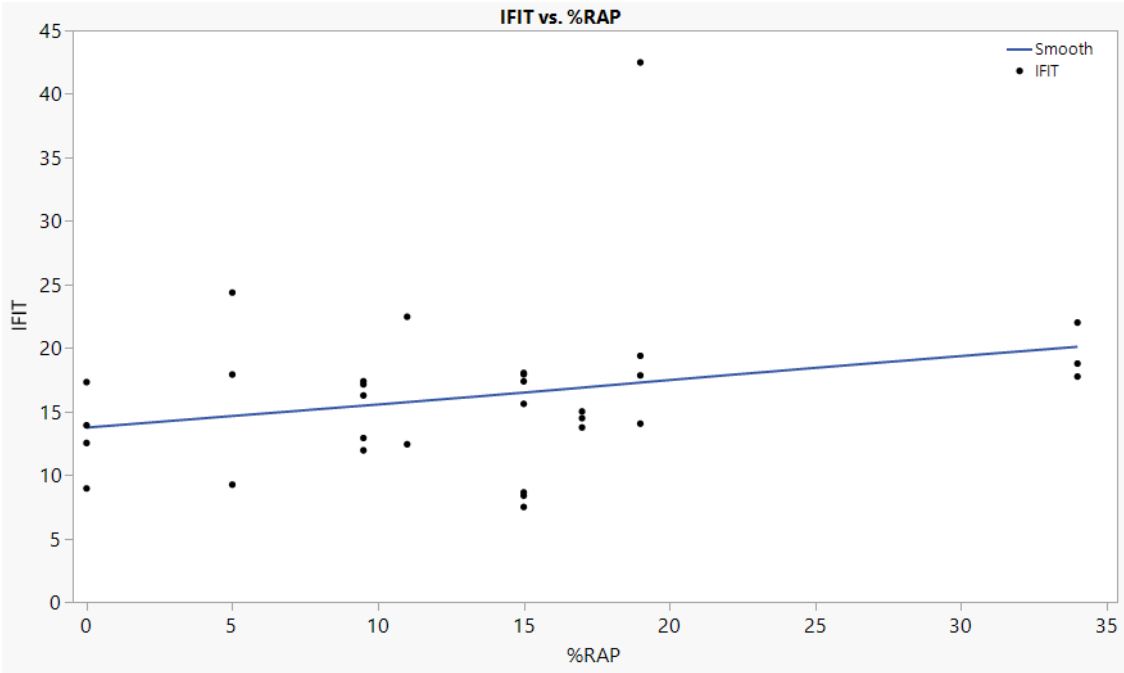
Generally, the mixtures had low variance as shown in the box plot in Figure 18.



**Figure 18. Box plot of FI**

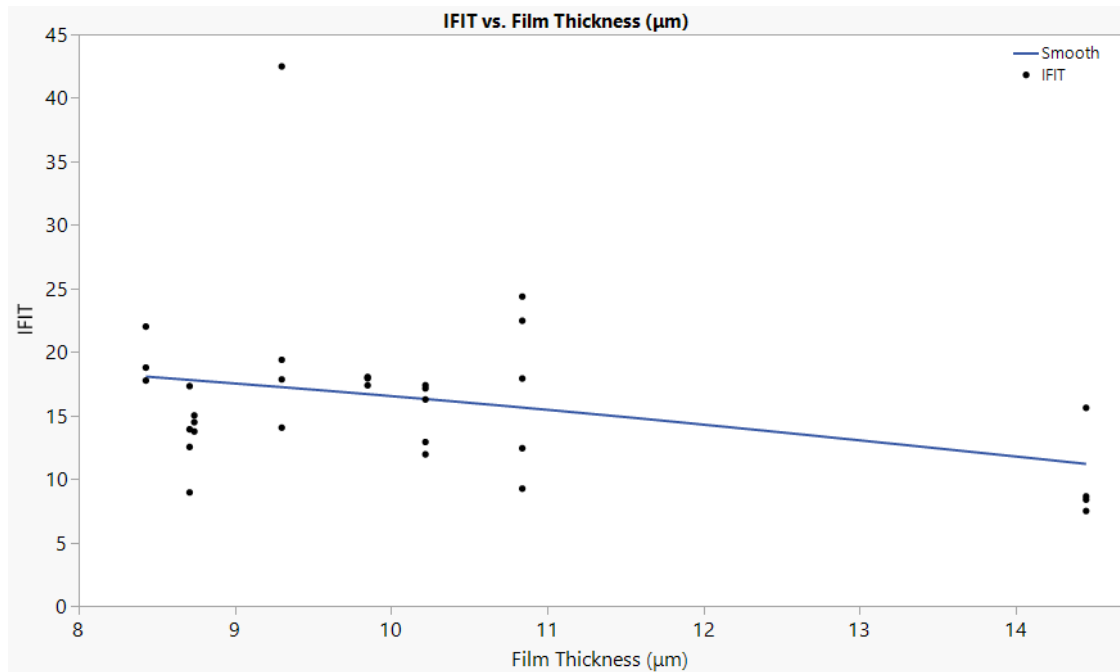
Mixture 4 had an outlier, which was not used when calculating the mean FI. Mixtures 1 and 2 had the highest variance as compared to the other mixtures.

Figure 19 shows the effect of RAP on the  $G_f$  from the I-FIT results.



**Figure 19. Effect of RAP on  $G_f$**

An increase in film thickness caused an increase in FI (Figure 20), of which this trend was also observed in the fracture energies of the SCB tests.



**Figure 20. Effect of film thickness on FI**

### Test Temperatures and Coefficients of Variation

All the mixtures have coefficients of variation (COV) below the recommend 25% for SCB and DCT tests, as shown in Table 4.

**Table 4. Test temperatures and COV for SCB and DCT**

Mixture	Test temperature (°C)	Reps	DCT		SCB	
			Mean	COV	Mean	COV
1	-18	4	470.00	13.53	907.20	15.23
2	-12	4	308.25	23.23	1102.00	17.52
3	-18	4	436.00	2.61	584.00	20.34
4	-18	4	265.25	13.37	670.00	18.68
5	-18	4	347.00	15.46	514.00	13.56
6	-18	4	412.75	18.16	609.75	17.39
7	-24	4	391.75	14.30	650.80	23.20
8	-18	4	381.25	21.79	905.75	21.49
9	-18	4	287.50	17.45	548.25	23.56
10	-18	4	330.5	6.57	485.17	13.52

Mixture 2 had the highest COV for the DCT test, at 23.23%, and Mixture 9 had the highest COV for SCB, at 23.56%, and the rest of the COV values were in the range of 2.61% to 21.79%.

Mixture 8 had COV values that were similar to one another based on results from both tests. This is an indicator that Mixture 8 met the required COV.

Table 5 shows the test temperatures and COV results from the I-FIT testing.

**Table 5. Test temperatures and COV for I-FIT**

Mixture	Test temperature (°C)	Reps	I-FIT	
			Mean	COV
1	25	4	14.93	33.71
2	25	4	17.57	35.56
3	25	4	18.29	13.95
4	25	4	23.32	32.21
5	25	4	17.93	0.44
6	25	4	15.28	16.03
7	25	4	8.36	7.52
8	25	4	15.05	7.79
9	25	4	14.47	4.60
10	25	4	12.65	15.09

### Overall Analysis

A JMP analysis of the  $G_f$  indicated: (1) based on the DCT and SCB results, Mixture 1 was significantly different from Mixtures 2, 4, 5, 9, and 10, while Mixture 2 was significantly different from Mixtures 1, 3, 6, and 7; (2) Mixtures 4, 5, 9, and 10 were not significantly different; and (3) RAP content was observed to be the factor that most affected  $G_f$  for the mixtures used in this study.



## CHAPTER 5. SUMMARY, CONCLUSIONS, AND RECOMMENDATIONS

The mixtures'  $G_f$  values of the DCT tests did not meet the design criteria for the traffic level, meaning that the fracture energies of the field-produced mixtures were lower than the value they were designed for demonstrated by the sample mixtures used in this study. It should be noted that the mixtures may have had low fracture energies because they had undergone more aging after mixing; during the laboratory tests, the mixtures were heated before compaction and before the  $G_{mm}$  tests.

DCT tests were not required for the laboratory-produced mixtures during construction since the binder replacement was less than 30% for mixtures with RAP and 25% for RAS. Additionally, the majority of mixtures studied in this work did not meet the requirement for DCT testing for their laboratory-designed mixtures and yet did not achieve  $G_f$  for their designed traffic volumes. The specification on the need for a DCT test should be revised to state that the test is required when the asphalt binder replacement exceeds 15% for mixtures with RAP and RAS, rather than the current value of 30% and 25% binder replacement, respectively.

The pavements that are still in use and have not had any major rehabilitation or maintenance activities show that these pavements have an adequate amount of cracking resistance as they have been able to carry the loads they were designed for. However, the laboratory tests on the mixtures show low cracking resistance and therefore a need for revising the specification or improving the quality-control process, just as MnDOT has allowed a  $50 \text{ J/m}^2$  range for quality assurance.

A pavement distress survey is recommended that focuses more on the intensity of thermal- and transverse-cracking distress over the years to assess the field performance of the pavements used in this study in relation to the DCT testing results.



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**APPENDIX. GRADATION AND ADDITIONAL DETAILS ON MIXTURES**

**Table 6. Mixture aggregate gradation**

Gradation (mm)	Mixtures									
	1	2	3	4	5	6	7	8	9	10
25	100	100	100	100	100	100	100	100	100	100
19	100	100	100	100	100	100	100	100	100	99
12.5	97	97	97	94	97	96	98	97	95	90
9.5	88	90	88	86	90	89	89	88	90	79
4.76	69	64	69	59	64	62	63	70	77	59
2.36	43	47	43	40	47	45	46	50	41	40
1.18	26	33	26	28	33	30	34	34	23	30
0.85	15	19	15	17	19	19	24	23	15	24
0.3	9.2	8.3	9.2	8.9	8.3	9.4	12	7.7	6.4	11
0.15	5.6	5.1	5.6	4.8	5.1	5.2	4.8	3.8	3.4	5.5
0.075	3.9	3.9	3.9	4.2	3.9	3.9	2.9	3	2.6	4.3

H0C5-200-4

4/25/13 Ver. 9.05

10/8/2014  
 Active Project No.: MP-017-1(705)0-76-77  
 Contract ID: 77-0171-705  
 Mix Design No.: 1BD14-065

**IOWA DOT ASPHALT PAVING DAILY PLANT REPORT**

10/6/14 3:59 PM

Contractor: DMAP  
 County: Polk  
 RAP Stockpile ID: 7.8% (ABC9-100) ABC14-0080 (7.4% AC)

Active Placement: Surface (Travel Lane)  
 Mix Type: 3M Surface 1/2 L-2 (HMA)  
 Active Bid Item: 2303-0043502 3M Surf 1/2in L-2 (HMA)  
 Report No.: 3  
 Lab Voids Target: 4.0  
 Design Gyration: 86

UNCOMPACTED MIXTURE			
Hot Box I.D. (Theoretical %AC)	HB-A (5.01%)	HB-P (4.99%)	
Date Sampled	10/8/14	10/8/14	
Time	1:55 PM	2:00 PM	
Station	367+00		
Side	2L-SB WB		
Sample (Tons)	459.54	523.44	
G <sub>mb</sub>	2.383	2.384	
G <sub>mb</sub> (DOT)			
G <sub>mm</sub>	2.474	2.475	
G <sub>mm</sub> (DOT)			
P <sub>a</sub> (%)	3.7	3.7	
P <sub>a</sub> (%) (DOT)			
Avg G <sub>mb</sub>		Avg G <sub>mm</sub>	Avg P <sub>a</sub> (%)
2.384		2.475	3.7

COMPACTED JOINT			
Core #	Station	Joint ID	G <sub>mb</sub>
1			
2			
3			
4			
5			
6			
7			
8			
9			
10			
11			
12			
Average G <sub>mb</sub>			

COMPACTED MAT											Cores have been waived		
Core	Date of Placement	Station	CL Reference	W1 Dry (g)	W2 in H2O (g)	W3 Wet (g)	G <sub>mb</sub>	% of G <sub>mm</sub>	P <sub>a</sub> (%)	Thickness (in.)			
1													
2													
3													
4													
5													
6													
7													
8													

GRADATION (% Passing)					Use DOT District
Sieve	Specs	CFA 10-08		Avg	
1 in.	100	100.0		100.0	
3/4 in.	100	100.0		100.0	
1/2 in.	90-100(97)	99.0		99.0	
3/8 in.	83-97(90)	92.0		92.0	
*#4	57-71(64)	66.0		66.0	
*Dev	± 7.0	2.0		2.0	
*#8	42-52(47)	46.0		46.0	
*Dev	± 5.0	-1.0		-1.0	
#16		31.0		31.0	
*#30	15-23(19)	18.0		18.0	
*Dev	± 4.0	-1.0		-1.0	
#50		8.5		8.5	
#100		4.8		4.8	
*#200	1.9-5.9(3.9)	3.8		3.8	
*Dev	± 2.0	-0.1		-0.1	
Gradation Compliance?					Yes
DBR	0.6 - 1.4	0.78		0.78	
% +4 Type 4	80	#DIV/0!		#DIV/0!	
% +4 Type 3		#DIV/0!		#DIV/0!	
(+4/4) Type 2	25/0	#DIV/0!		#DIV/0!	

**USE D.O.T. RESULTS**  
 (Enter an 'X')

**TEST STRIP**  
 (Enter an "X")

FILM THICKNESS (FT) (8.0-15.0)	
FT, μm	10.9
Price Adjustment	\$0.00

Gyratory VMA (15.8-17.8)	
VMA, %	15.5

QUANTITY FOR PAYMENT	
Mix Unit Price (\$/ton)	\$60.00
Binder Unit Price (\$/ton)	\$550.00
Tons of Mix on Road	385.61
Tons to Other Bid Item(s)	
Tons of Binder	20.37
Tons of Waste	
Tons of Binder to Date	
Tons of Mix to Date	

Course Placed: Surface (Travel Lane)  
 Intended Lift Thickness: 2.00  
 Date Placed: 10/08/14  
 Test Date/By:  
 Thickness QI:  
 Avg. Mat Density:  
 Avg. % of G<sub>mb</sub>:  
 Avg. % Field Voids:

Q.I. (lower) = \_\_\_\_\_ → PWL (lower) = \_\_\_\_\_  
 Q.I. (upper) = \_\_\_\_\_ → PWL (upper) = \_\_\_\_\_  
 PWL (total) = \_\_\_\_\_ + \_\_\_\_\_ - 100.0 = \_\_\_\_\_  
 Pay Factor = \_\_\_\_\_

Tons of Mix for PWL Field Voids Analysis (00.00 deducted) = 385.61  
 Field Voids Price Adjustment = \_\_\_\_\_

Time	TEMPERATURE, °F							Spec	Comply?
	7:00	9:00	11:00	1:00	3:00	5:00	7:00		
Air Temp	46	50	61	67	71	71			
Binder Temp			306	308			260-330 °F	Yes	
Plant Temp			328	330			225-330 °F	Yes	
Mat Temp			305	300	295		225-330 °F	Yes	

Break Down  
 Rain Out  
 Re-start after mandatory shutdown  
 Mix Change Information (When changes are made to start the day, identify them on previous day's report):

BINDER				
	Target	Actual	Spec	Comply?
% Added Binder	4.20	4.44	N/A	
% Total Binder	5.30	5.28	5.00-5.60	Yes
% RAP	9.50	7.81%	≤100%	Yes
% RAS	5.00	4.11%	≤ 5%	Yes
% Binder Replacement	19.33%	15.91%	≤ 30%	Yes
PG Grade	64-22		58-28	No
Binder replacement exceeded. Binder grade does not comply AC > 0.2% different than				
G <sub>b</sub>	1.03193	G <sub>sb</sub> : 2.652	P <sub>be</sub> (%):	4.87

PLACEMENT RECORD			
From Station	To Station	Lane	Width (ft)

Old Target	New Target	Tons	Agg	Initial %	New %	Agg	Initial	New %

Certified Tech: Ryan Horn Cert. No. C1316  
 Certified Tech: Ben Crawford Cert. No. SW498  
 Distribution: \_\_\_\_\_ Dist. Materials \_\_\_\_\_ Proj. Engineer \_\_\_\_\_ Contractor \_\_\_\_\_

Comment:  
 1st sample was a road box at 459.54 tons. 2nd sample was from the plant at 523.44 tons

**Iowa Department of Transportation**  
 Highway Division-Office of Materials  
 Proportion & Production Limits For Aggregates

ABC 5-2-4 DCT

County: Polk Project No.: MP-017-1(705)0--76-77 Date: 04/01/14  
 Project Location: From Iowa 141 to NW 158th Avenue Mix Design No.: 1BD14-065  
 Contract Mix Tonnage: 1,597 Course: Surface Mix Size (in.): 1/2  
 Contractor: DMAP Mix Type: HMA 3M Design Life ESAL's: 3,000,000

Material	Ident #	% in Mix	Producer & Location	Type (A or B)	Friction Type	Beds	Gsb	%Abs
3/4 Chips	A85006	5.5%	Martin Marietta/Ames Mine	A	5	47	2.655	0.88
1/2 Add Rock-Quartzite	ASD002	9.0%	Lg Everist Inc/Dell Rapids E. Minnehaha C	A	2		2.652	0.42
3/8" Washed Chips L4	A85006	21.5%	Martin Marietta/Ames Mine	A	4	49	2.652	0.78
Manufactured Sand	A85006	32.5%	Martin Marietta/Ames Mine	A	5	47	2.666	0.71
Asphalt Sand	A77504	17.0%	Hallett Materials Co/Denny-Johnston	A	4		2.648	0.69
RAP/RAS	ABC9-100	14.5%	9.5% RAP/5% RAS (7.8% AC)	A	2	BC14-008	2.606	1.80

Type and Source of Asphalt Binder: St. Paul Park Refinery Co. LLC (St. Paul P)

Material	Individual Aggregates Sieve Analysis - % Passing (Target)										
	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
3/4 Chips	100	100	60	31	5.0	2.5	2.0	1.7	1.5	1.2	1.0
1/2 Add Rock-Quartzite	100	100	99	81	10	1.5	1.0	1.0	1.0	1.0	1.0
3/8" Washed Chips L4	100	100	100	86	18	2.5	2.0	1.8	1.7	1.3	1.0
Manufactured Sand	100	100	100	100	97	68	39	20	8.0	5.0	3.5
Asphalt Sand	100	100	100	100	95	88	76	41	8.0	1.0	0.8
RAP/RAS	100	100	98	93	80	65	50	38	30	23	18

Preliminary Job Mix Formula Target Gradation

Upper Tolerance	100	100	100	97	71	52		23			5.9
Comb Grading	100	100	97	90	64	47	33	19	8.3	5.1	3.9
Lower Tolerance	100	100	90	83	57	42		15			1.9
S.A.sq. m/kg	Total	4.56		+0.41	0.26	0.38	0.54	0.55	0.51	0.63	1.26

Production Limits for Aggregates Approved by the Contractor & Producer.

Sieve Size in.	5.5% of mix 3/4 Chips		9.0% of mix 1/2 Add Rock-Quartzite		21.5% of mix 3/8" Washed Chips L4		32.5% of mix Manufactured Sand		17.0% of mix Asphalt Sand		14.5% of mix RAP/RAS	
	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max
1"	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0		
3/4"	98.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0		
1/2"	53.0	67.0	95.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0		
3/8"	24.0	38.0	74.0	88.0	79.0	93.0	100.0	100.0	100.0	100.0		
#4	0.0	12.0	3.0	17.0	11.0	25.0	90.0	100.0	88.0	100.0		
#8	0.0	6.0	0.0	6.0	0.0	6.0	63.0	73.0	83.0	93.0		
#30	0.0	4.0	0.0	4.0	0.0	4.0	16.0	24.0	37.0	45.0		
#200	0.0	1.5	0.0	1.5	0.0	1.5	0.0	5.0	0.0	1.5		

Comments: Signatures on file in District 1 Materials Office  
 Copies to: DMAP Rex Kinkade Cheryl Barton Rita Eichhorst  
 Vicky Rink Jefferson RCE Mark Trueblood Central Materials

The above target gradations and production limits have been discussed with and agreed to by an authorized representative of the aggregate producer.

Signed: \_\_\_\_\_ Producer  
 Signed: \_\_\_\_\_ Contractor

**Iowa Department of Transportation**  
Highway Division - Office of Materials  
HMA Gyrotory Mix Design

N <sub>max</sub>			Letting Date :		
County :	Polk	Project :	MP-017-1(705)0--76-77	Mix No. :	IBD14-065
Mix Size (in.) :	1/2 Type A	Contractor :	DMAP	Contract #:	77-0171-705
Mix Type:	HMA 3M L-2	Design Life ESAL's :	3,000,000	Date:	04/01/14
Intended Use :	Surface	Location :	MP 0 - 7	From Iowa 141 to NW 158th Avenue	

Aggregate	% in Mix	Source ID	Source Location	Beds	Gsb	%Abs	FAA	Friction
3/4 Chips	5.5%	A85006	Martin Marietta/Ames Mine	47	2.655	0.88	46.0	5
1/2 Add Rock-Quartzite	9.0%	ASD002	Lg Everist Inc/Dell Rapids E. Minneh		2.652	0.42	47.0	2
3/8" Washed Chips L4	21.5%	A85006	Martin Marietta/Ames Mine	49	2.652	0.78	46.0	4
Manufactured Sand	32.5%	A85006	Martin Marietta/Ames Mine	47	2.666	0.71	47.0	5
Asphalt Sand	17.0%	A77504	Hallett Materials Co/Denny-Johnston		2.648	0.69	40.0	4
RAP/RAS	14.5%	ABC9-100	9.5% RAP/5% RAS (7.8% AC)	ABC14-0080	2.606	1.80	43.9	2

Job Mix Formula - Combined Gradation (Sieve Size in.)

1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
Upper Tolerance										
100	100	100	97	71	52	33	23	8.3	5.1	5.9
100	100	97	90	64	47	33	19	8.3	5.1	3.9
100	100	90	83	57	42	33	15			1.9
Lower Tolerance										

Asphalt Binder Source and Grade: St. Paul Park Refinery Co. LLC (St. Paul Park, MN)					Gyrotory Data				
Adjust grade to PG 58-28									
% Asphalt Binder	4.75	5.25	5.48	5.75	Number of Gyrotations				
Corrected Gmb @ N-Des.	2.342	2.363	2.369	2.376	N-Initial				
Max. Sp.Gr. (Gmm)	2.484	2.472	2.468	2.463	7				
% Gmm @ N- Initial	87.1	88.2	88.7	89.2	N-Design				
%Gmm @ N-Max	94.5	95.9	96.3	96.7	86				
% Air Voids	5.7	4.4	4.0	3.5	N-Max				
% VMA	17.1	16.8	16.8	16.8	134				
% VFA	66.5	73.7	76.1	78.9	Gsb for Angularity				
Film Thickness	9.01	9.89	10.22	10.66	Method A				
Filler Bit. Ratio	0.95	0.86	0.84	0.80	2.651				
Gsc	2.693	2.701	2.707	2.713	Pba / %Abs Ratio				
Pbe	4.11	4.51	4.66	4.86	0.52				
Pba	0.62	0.73	0.82	0.90	Slope of Compaction				
% New Asphalt Binder	77.2	79.5	80.4	81.3	Curve				
Combined Gb @ 25°C	1.0300	1.0300	1.0300	1.0300	16.9				
					Mix Check				
					Poor				
					Pb Range Check				
					1.00				
					RAM Check				
					OK				
					Specification Check				
					Comply				
					Moisture Sensitivity Check				
					SIP (0% AS)=14,187				
					Please choose AS Dosage if req.				

Disposition : An asphalt content of 5.5% is recommended to start this project.  
 Data shown in 5.48% column is interpolated from test data.  
 The % ADD AC to start project is 4.4%  
 Comments : Final approval based upon plant produced mix

Copies to : DMAP Rex Kinkade Cheryl Barton Rita Eichhorst Vicky Rink  
Jefferson RCE Mark Trueblood Central Materials

Mix Designer & Cert.# : Thuisman CI-515 Signed : Cheryl L. Barton, District 1 Materials



425113 - rev 11/07

10/3/2018

Active Project No: MX-035-5(108)131-02-40
Contract ID: 85-0355-109
Mix Design No: 1BD18-011

IOWA DOT ASPHALT PAVING DAILY PLANT REPORT

Contractor: MANATTS INC - AMES
County: HAMILTON
RAP Stockpile ID: 1RAP15-021 (4.9 % AC)

Active Placement: Surface (Travel Lane)
Mix Type: Vt Surface L - 2 1/2 (HMA)
Active Bid Item: 2303-1053502 VT SURF 1/2IN L-2 (HMA)
Report No: 15
Lab Voids Target: 4.0
Design Gyration: 95

Table with columns: Hot Box ID, D1, D1-006893, D1-006894, D1-008890. Rows include Date Sampled, Time, Station, Bar Code ID, Sample (Tons), Gmb, Gmm, Gmm (DOT), Ps (%), Ps (% (DOT)).

GRADATION (%Passing) table with columns: Sieve, Specs, Missing Tons, Avg, District. Rows include 1 in, 3/4 in, 1/2 in, 3/8 in, #4, #8, #16, #30, #50, #100, #200.

BINDER table with columns: Target, Actual, Spec, Comply?. Rows include % Added Binder, % Total Binder, % RAP, % RAS, % Binder Replacement, PG Grade, Gb, Gsc, Pbe (%).

COMPACTED JOINT table with columns: Core #, Station, Joint ID, Gmb. Includes Average Joint Gmb, Average Mat Gmb, % Mat Density, and Joint Price Adjustment.

USE D.O.T. RESULTS (Enter an 'X')

TEST STRIP (Enter an 'X')

FILM THICKNESS (FT) 18.0-15.0 table with columns: FT, Price Adjustment.

Gyration VMA table with column: VMA % = 14.0

QUANTITY FOR PAYMENT table with columns: Mix Unit Price (\$/ton), Binder Unit Price (\$/ton), Tons of Mix on Road, Tons of Binder, Tons of Waste, Tons of Binder to Date, Tons of Mix to Date.

PLACEMENT RECORD table with columns: From Station, To Station, Lane, Width (ft).

Certified Tech: CINDY DELA ROSA, Cert No: CI722

COMPACTED MAT table with columns: Core, Date of Placement, Station, CL Reference, W1 Dry (g), W2 in H2O (g), W3 Wet (g), Gmb, % of Gmm, Ps (%), Thickness (in).

Course Placed: Surface (Travel Lane), Thickness QI, Intended Lift Thickness: 2.00, Date Placed: 10/03/18, Test Date/By: 10/04/18, Dennis Ackerman

Q.I (lower) = ... PWL (lower) = ...
Q.I (upper) = ... PWL (upper) = ...
PWL (total) = ... + ... - ... 100.0 = ...

Pay Factor = ...
Tons of Mix for PWL Field Voids Analysis (00.00 deducted) = 1,839.00 Field Voids Price Adjustment =

TEMPERATURE, °F table with columns: Time, Air Temp, Binder Temp, Plant Temp, Mat Temp, Spec, Comply?.

Break Down, Rain Out, Register after mandatory shutdown, Mix Change Information

Table with columns: Old Target, New Target, Tons, Agg, Initial %, New %, Agg, Initial, New %.

Comments:



**Iowa Department of Transportation**  
 Highway Division - Office of Construction & Materials  
 HMA Gyrotory Mix Design

Notesign		County :		Story	Project :	IMX-035-5(109)112--02-85	Letting Date :	10/17/2017
Mix Size (in.) :		1/2	Type A	Contractor :	MANATTS INC - AMES	Mix No. :	IBD18-011	
Mix Type :		VT	L - 2	Design Traffic :	Very High Traffic	Contract # :	85-0355-109	
Intended Use :		Surface		Location :	MP 111.78 - 116.74	Date :	05/22/18	
						I-35 - US 30 INTERCHANGE TO THE CO RD E-29 NB		

Aggregate	% in Mix	Source ID	Source Location	Beds	Gsb	%Abs	FAA	Friction
1/2 CRUSHED L-4	21.0%	A85006	Martin Marietta Aggregates/Ames Mi	49-50	2.651	0.81	47.0	4
1/2 QUARTZITE	12.0%	ASD002	L G Everist Inc/Dell Rapids-East		2.641	0.14	47.5	2
3/8 CL CHIP L-4	8.0%	A85006	Martin Marietta Aggregates/Ames Mi	49-50	2.672	0.55	47.0	4
MANF SAND	15.0%	A85006	Martin Marietta Aggregates/Ames Mi	47	2.673	0.60	45.0	5
QUARTZ M SAND	15.0%	ASD002	L G Everist Inc/Dell Rapids-East		2.639	0.25	49.0	2
SAND	10.0%	A85510	Hallett Materials Co/Ames South		2.617	1.03	40.0	4
Classified RAP	19.0%	I-35	19% TRAP15-021 (4.9 % AC)		2.613	1.65	42.9	2

Job Mix Formula - Combined Gradation (Sieve Size in.)

1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
Upper Tolerance										
100	100	100	96	69	50		23			5.9
<b>100</b>	<b>100</b>	<b>96</b>	<b>89</b>	<b>62</b>	<b>45</b>	<b>30</b>	<b>19</b>	<b>9.4</b>	<b>5.2</b>	<b>3.9</b>
Lower Tolerance										
100	100	89	82	55	40		15			1.9

Asphalt Binder Source and Grade:		BITUMINOUS MATERIALS TAMA, IA PG 58-28V					
		Gyrotory Data					
% Asphalt Binder	4.25	4.70	4.75	5.25			<u>Number of Gyrotions</u>
Gmb @ N-Des.	2.353	<b>2.388</b>	2.391	2.401			N-Initial
Max. Sp.Gr. (Gmm)	2.503	<b>2.487</b>	2.486	2.466			9
% Gmm @ N- Initial	86.8	<b>88.6</b>	88.8	89.8			N-Design
%Gmm @ N-Max							95
% Air Voids	6.0	4.0	3.8	2.6			N-Max
% VMA	14.7	<b>13.9</b>	13.8	13.9			<u>Gsb for Angularity</u>
% VFA	59.4	<b>71.2</b>	72.4	81.0			<u>Method A</u>
Film Thickness	8.36	<b>9.30</b>	9.39	10.53			2.638
Filler Bit. Ratio	1.02	<b>0.92</b>	0.91	0.81			<u>Pba / %Abs Ratio</u>
Gse	2.674	<b>2.676</b>	2.676	2.675			0.62
Pbe	3.81	<b>4.24</b>	4.28	4.80			<u>Slope of Compaction</u>
Pba	0.46	<b>0.49</b>	0.49	0.48			<u>Curve</u>
% New Asphalt Binder	78.8	<b>81.0</b>	81.2	83.0			<u>Mix Check</u>
Combined Gb @ 25°C	1.0237	<b>1.0235</b>	1.0235	1.0233			Excellent
Aggregate Type Used	A			Contribution From RAM			
G <sub>sb</sub>	2.642	% Friction Type 4 (+4)		64	12		
G <sub>sa</sub>	2.697	Or Better		94	13		
% Water Abs	0.77	% Friction Type 3 (+4)		0	0	1.00	
S.A. m <sup>2</sup> / Kg.	4.56	Or Better		30	1		
Angularity-method A	45	% Friction Type 2 (+4)		30	1		
% Flat & Elongated	2.0	% Friction Type 2 (-4)		26	0		
Sand Equivalent	96	Type 2 Fineness Modulus		1.9	0.7		
Virgin G <sub>b</sub> @ 25°C	1.022	% Crushed		88.0	16.8		
Anti-Strip Dose (%)	0.00						
Stripping Inflection Point	20,000.0						

Disposition : An asphalt content of 4.7% is recommended to start this project.  
 Data shown in 4.70% column is interpolated from test data.  
 The % ADD AC to start project is 3.8%

SIP (0% AS)=20,000  
 Please choose AS Dose/Type if req.

0.00 % of binder

Comments : Hamburg results included= PASS

Copies to : MANATTS INC - AMES

Mix Designer & Cert.# : CINDY DELA ROSA CI 722

Signed : Shane Fetters(District 1 Materials)

**Iowa Department of Transportation**  
 Highway Division-Office of Materials  
 Proportion & Production Limits For Aggregates

County : Story Project No.: IMX-035-5(109)112-02-85 Date: 05/22/18  
 Project Location: I-35 - US 30 INTERCHANGE TO THE CO RD E-29 NB Mix Design No.: IBD18-011  
 Contract Mix Tonnage: 18,627 Course: Surface Mix Size (in.): 1/2  
 Contractor: MANATTS INC - AMES Mix Type: VT Design Traffic: Very High Traffic

Material	Ident #	% in Mix	Producer & Location	Type (A or B)	Friction Type	Beds	Gsb	%Abs
1/2 CRUSHED L-4	A85006	21.0%	Martin Marietta Aggregates/Ames Mine	A	4	49-50	2.651	0.81
1/2 QUARTZITE	ASD002	12.0%	L G Everist Inc/Dell Rapids-East	A	2		2.641	0.14
3/8 CL CHIP L-4	A85006	8.0%	Martin Marietta Aggregates/Ames Mine	A	4	49-50	2.672	0.55
MANF SAND	A85006	15.0%	Martin Marietta Aggregates/Ames Mine	A	5	47	2.673	0.60
QUARTZ M SAND	ASD002	15.0%	L G Everist Inc/Dell Rapids-East	A	2		2.639	0.25
SAND	A85510	10.0%	Hallett Materials Co/Ames South	A	4		2.617	1.03
Classified RAP	I-35	19.0%	19% 1RAP15-021 (4.9% AC)	A	2		2.613	1.65

Type and Source of Asphalt Binder: PG 58-28V BITUMINOUS MATERIALS TAMA, IA

Material	Individual Aggregates Sieve Analysis - % Passing (Target)										
	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
1/2 CRUSHED L-4	100	100	92	77	38	25	17	13	11	8.5	7.0
1/2 QUARTZITE	100	100	99	81	10	1.1	0.6	0.5	0.4	0.3	0.2
3/8 CL CHIP L-4	100	100	100	92	22	3.5	2.5	1.8	1.7	1.6	1.5
MANF SAND	100	100	100	100	96	68	38	20	7.5	3.5	2.5
QUARTZ M SAND	100	100	100	100	99	74	47	30	12	2.8	0.9
SAND	100	100	100	100	98	87	69	40	8.0	0.6	0.2
Classified RAP	100	99	90	82	65	47	36	26	17	12	9.3

Preliminary Job Mix Formula Target Gradation											
Upper Tolerance	100	100	100	96	69	50	23				5.9
Comb Grading	100	100	96	89	62	45	30	19	9.4	5.2	3.9
Lower Tolerance	100	100	89	82	55	40	15				1.9
S.A.sq. m/kg	Total	4.56		+0.41	0.26	0.37	0.50	0.55	0.58	0.64	1.27

Sieve Size in.	Production Limits for Aggregates Approved by the Contractor & Producer.											
	21.0% of mix		12.0% of mix		8.0% of mix		15.0% of mix		15.0% of mix		10.0% of mix	
	1/2 CRUSHED L-4	1/2 QUARTZITE	3/8 CL CHIP L-4	MANF SAND	QUARTZ M SAND	SAND	Min	Max	Min	Max	Min	Max
1"	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0
3/4"	98.0	100.0	98.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0
1/2"	85.0	99.0	92.0	100.0	98.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0
3/8"	70.0	84.0	74.0	88.0	85.0	99.0	98.0	100.0	98.0	100.0	98.0	100.0
#4	31.0	45.0	3.0	17.0	15.0	29.0	89.0	100.0	92.0	100.0	91.0	100.0
#8	20.0	30.0	0.0	6.1	0.0	8.5	63.0	73.0	69.0	79.0	82.0	92.0
#30	9.0	17.0	0.0	4.5	0.0	5.8	16.0	24.0	26.0	34.0	36.0	44.0
#200	5.0	9.0	0.0	2.2	0.0	3.5	0.5	4.5	0.0	2.9	0.0	2.2

Comments: \_\_\_\_\_  
 Copies to: MANATTS INC - AMES

The above target gradations and production limits have been discussed with and agreed to by an authorized representative of the aggregate producer.

Signed: \_\_\_\_\_  
 Producer

Signed: \_\_\_\_\_  
 Contractor



**Iowa Department of Transportation**  
 Highway Division - Office of Construction & Materials  
 HMA Gytratory Mix Design

Ndesign

County : Marshall  
 Mix Size (in.) : 3/4 Type A  
 Mix Type: ST No Frictn  
 Intended Use : Surface  
 Project : FM-CO64(127)--55-64  
 Contractor : Manatt's Inc.  
 Design Traffic : Standard Traffic  
 Location : E41/235th St, from ECL. of State Center E 9 Miles to IA 330.

Letting Date : 4/17/2018  
 Mix No. : 1BD16-065  
 Contract #: 64-CO64-127  
 Date: 08/16/18

Aggregate	% in Mix	Source ID	Source Location	Beds	Gsb	%Abs	FAA	Friction
3/4" Clean	34.0%	A64002	Martin Marietta Aggregates/Ferguson	10-17	2.630	1.78	46.0	4
3/8" Chips	5.0%	A64002	Martin Marietta Aggregates/Ferguson	10-17	2.628	1.85	47.0	4
Manufactured Sand	24.0%	A64002	Martin Marietta Aggregates/Ferguson	10-17	2.646	1.75	47.0	4
Screened	20.0%	A64002	Martin Marietta Aggregates/Ferguson		2.630	0.55	39.5	
Classified RAP	17.0%	IRAP18-020	17% ABC18-0068 (5.97 % AC)		2.585	1.63	41.6	4

Job Mix Formula - Combined Gradation (Sieve Size in.)

1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
Upper Tolerance										
100	100	97	85	66	45		28			6.3
<b>100</b>	<b>99</b>	<b>90</b>	<b>78</b>	<b>59</b>	<b>40</b>	<b>30</b>	<b>24</b>	<b>11</b>	<b>5.5</b>	<b>4.3</b>
Lower Tolerance										
100	92	83	71	52	35		20			2.3

Asphalt Binder Source and Grade:	BITUMINOUS MATERIALS TAMA, IA PG 58-28S					
	Gytratory Data					
% Asphalt Binder	4.60	5.00	5.02	5.50	6.00	<u>Number of Gytrations</u>
Gmb @ N-Des.	2.365	2.378	2.379	2.402	2.409	N-Initial
Max. Sp.Gr. (Gmm)	2.494	2.479	2.478	2.461	2.453	7
% Gmm @ N-Initial	89.6	90.5	90.6	92.1	92.5	N-Design
%Gmm @ N-Max						50
% Air Voids	5.2	4.1	4.0	2.4	1.8	N-Max
% VMA	14.1	14.0	14.0	13.6	13.8	<u>Gsb for Angularity</u>
% VFA	63.3	70.8	71.3	82.3	87.0	<u>Method A</u>
Film Thickness	7.87	8.68	8.74	9.70	10.37	2.624
Filler Bit. Ratio	1.11	1.01	1.00	0.90	0.84	<u>Pba / %Abs Ratio</u>
Gse	2.679	2.679	2.678	2.679	2.692	0.55
Pbe	3.87	4.27	4.30	4.77	5.10	<u>Slope of Compaction</u>
Pba	0.77	0.77	0.76	0.77	0.96	<u>Curve</u>
% New Asphalt Binder	78.7	80.5	80.6	82.4	83.9	<u>Mix Check</u>
Combined Gb @ 25°C	1.0260	1.0259	1.0259	1.0258	1.0257	Good

Aggregate Type Used	A	Combined	Contribution From RAM
G <sub>ab</sub>	2.626	% Friction Type 4 (+4)	93
G <sub>mb</sub>	2.734	Or Better	93
% Water Abs	1.50	% Friction Type 3 (+4)	0
S.A. m <sup>2</sup> / Kg.	4.92	Or Better	0
Angularity-method A	42	% Friction Type 2 (+4)	0
% Flat & Elongated	0.0	% Friction Type 2 (-4)	0
Sand Equivalent	85	Type 2 Fineness Modulus	0.0
Virgin G <sub>b</sub> @ 25°C	1.0249	% Crushed	73.0
Anti-Strip Dose (%)	0.00		9.7

Number of Gytrations  
 N-Initial  
 7  
 N-Design  
 50  
 N-Max  
Gsb for Angularity  
Method A  
 2.624  
Pba / %Abs Ratio  
 0.55  
Slope of Compaction  
Curve  
Mix Check  
 Good  
Pb Range Check  
 1.40  
RAM Check  
 OK  
Specification Check  
 Comply  
Hamburg Check  
 Not Required

Disposition : An asphalt content of 5.0% is recommended to start this project.  
 Data shown in 5.02% column is interpolated from test data.  
 The % ADD AC to start project is 4.0%

Comments : \_\_\_\_\_

Copies to : Manatt's Inc. \_\_\_\_\_

Mix Designer & Cert.# : Brad Karsten CI391 Signed : Shane Fetters(District 1 Materials)

**Iowa Department of Transportation**  
 Highway Division-Office of Materials  
 Proportion & Production Limits For Aggregates

County : Marshall Project No.: FM-CO64(127)-55-64 Date: 08/16/18  
 Project Location: E41/235th St, from ECL of State Center E 9 Miles to IA 330. Mix Design No.: 1BD16-065  
 Contract Mix Tonnage: 15,340 Course: Surface Mix Size (in.): 3/4  
 Contractor: Manatt's Inc. Mix Type: ST Design Traffic: Standard Traffic

Material	Ident #	% in Mix	Producer & Location	Type (A or B)	Friction Type	Beds	Gsb	%Abs
3/4" Clean	A64002	34.0%	Martin Marietta Aggregates/Ferguson	A	4	10-17	2.630	1.78
3/8" Chips	A64002	5.0%	Martin Marietta Aggregates/Ferguson	A	4	10-17	2.628	1.85
Manufactured Sand	A64002	24.0%	Martin Marietta Aggregates/Ferguson	A	4	10-17	2.646	1.75
Screened	A64002	20.0%	Martin Marietta Aggregates/Ferguson				2.630	0.55
Classified RAP	RAP18-02	17.0%	17% ABC18-0068 (5.97 % AC)	A	4		2.585	1.63

Type and Source of Asphalt Binder: PG 58-28S BITUMINOUS MATERIALS TAMA, IA

Material	1"	Individual Aggregates Sieve Analysis - % Passing (Target)									
		3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
3/4" Clean	100	98	72	42	8.0	3.5	3.0	2.9	2.8	2.7	2.5
3/8" Chips	100	100	100	94	27	5.0	3.5	3.0	2.8	2.6	2.5
Manufactured Sand	100	100	100	100	97	41	16	9.0	4.0	3.5	2.8
Screened	100	100	100	99	98	95	87	75	33	8.0	5.0
Classified RAP	100	100	97	91	73	57	46	34	17	12	9.8

Preliminary Job Mix Formula Target Gradation

Upper Tolerance	100	100	97	85	66	45		28			6.3
Comb Grading	100	99	90	78	59	40	30	24	11	5.5	4.3
Lower Tolerance	100	92	83	71	52	35		20			2.3
S.A.sq. m/kg	Total	4.92		+0.41	0.24	0.33	0.49	0.69	0.71	0.67	1.39

Production Limits for Aggregates Approved by the Contractor & Producer.

Sieve Size in.	34.0% of mix 3/4" Clean		5.0% of mix 3/8" Chips		24.0% of mix Manufactured Sand		20.0% of mix Screened		17.0% of mix Classified RAP	
	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max
1"	98.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0		
3/4"	91.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0		
1/2"	65.0	79.0	98.0	100.0	100.0	100.0	98.0	100.0		
3/8"	35.0	49.0	87.0	100.0	98.0	100.0	92.0	100.0		
#4	1.0	15.0	20.0	34.0	90.0	100.0	91.0	100.0		
#8	0.0	8.5	0.0	10.0	36.0	46.0	90.0	100.0		
#30	0.0	6.9	0.0	7.0	5.0	13.0	71.0	79.0		
#200	0.5	2.5	0.5	2.5	0.8	2.8	2.0	5.0		

Comments: \_\_\_\_\_

Copies to: Manatt's Inc. \_\_\_\_\_

The above target gradations and production limits have been discussed with and agreed to by an authorized representative of the aggregate producer.

Signed: \_\_\_\_\_  
 Producer

Signed: \_\_\_\_\_  
 Contractor

4/25/15 REV 11 07

10/10/2018  
Active Project No FM-C064(127)-55-64  
Contract ID 64-C064-127  
Mix Design No 1BD18-065R1

IOWA DOT ASPHALT PAVING DAILY PLANT REPORT

Contractor: Manatt's Inc.  
County: Marshall  
RAP Stockpile ID: ABC18-0658 (5.97 % AC)

Active Placement: Surface (Travel Lane)  
Mix Type: ST Surface None 3/4 (HMA)  
Active Bid Item: 2303-1033750 ST SURF 3/4IN NO (HMA)  
Report No: 7  
Lab Voids Target: 4.0  
Design Gyration: 50

10/10/18 7:43 PM

Table with 5 columns: SUR-07-A (5.24%), SUR-07-B (5.14%), SUR-C (5.07%), SUR-D (5.24%). Includes sections for UNCOMPACTED MIXTURE, GRADATION (%Passing), and various material properties like Gmb, Gmm, and Pn.

Table with 4 columns: Core #, Station, Joint ID, Gmb. Includes sections for COMPACTED JOINT and For information Only.

USE D.O.T. RESULTS (Enter an 'X')

TEST STRIP (Enter an "X")

Table with 2 columns: FT, µm and Price Adjustment. Value: 8.8, \$0.00.

Table with 2 columns: Gyratory VMA and VMA, %. Value: 14.1.

Table with 2 columns: Mix Unit Price (\$/ton) and Binder Unit Price (\$/ton). Values: \$22.60, \$400.00.

Table with 4 columns: From Station, To Station, Lane, Width (ft). Values: 0+00, 96+00, SB/WB Drive Lr, 12.

Certified Tech: Brad Karsten, Cert No C1391  
Certified Tech: Sally Slaven, Cert No C1489

Table with 11 columns: Core, Date of Placement, Station, CL Reference, W1 Dry (g), W2 in H2O (g), W3 Wet (g), Gmb, % of Gmm, Pn (%), Thickness (in). Includes sections for COMPACTED MAT and Course Placed.

Course Placed: Surface (Travel Lane). Thickness: 2.00. Avg Mat Density: 2.325. Avg % of Gmm: 93.838.

Q1 (lower) = (0.965 x 2.477) / 0.018 = 2.325 = 3.63 → PWL (lower) = 100.0  
Q1 (upper) = 2.325 / 0.018 = 134.72 = 3.25 → PWL (upper) = 100.0  
PWL (total) = 100.0 + 100.0 = 200.0 = 100.0

Pay Factor = 1.040

Tons of Mix for PWL Field Voids Analysis (189.33 deducted) = 2,157.86. Field Voids Incentive = \$1,950.71

Table with 10 columns: Time, Temperature (°F), Spec, Comply? for Air Temp, Binder Temp, Plant Temp, Mat Temp.

Break Down, Rain Out, Re-start after mandatory shutdown, etc.

Table with 10 columns: Old Target, New Target, Tons, Agg, Initial %, New %, Agg, Initial, New %.

Comments section for reporting.

Table with 5 columns: Target, Actual, Spec, Comply? for % Added Binder, % Total Binder, % RAP, % RAS, % Binder Replacement, PG Grade, Gb, Gsb, Pbe (%).

4/25/13 ver 11.07

10/11/2018  
Active Project No. FM-C064(127)-55-64  
Contract ID 64-C064-127  
Mix Design No 1BD18-065R1



IOWA DOT ASPHALT PAVING DAILY PLANT REPORT

10/11/18 2:54 PM

Contractor: Manatt's Inc.  
County: Marshall  
RAP Stockpile ID: ABC18-0058 (5.97 % AC)

Surface (Travel Lane)  
ST Surface None 3/4 (HMA)  
2303-1033750 ST SURF 3/4IN NO (HMA)  
Report No: 8  
Lab Voids Target: 4.0  
Design Gyration: 50

UNCOMPACTED MIXTURE table with columns for Hot Box I.D., SUR-A, SUR-B, Date Sampled, Time, Station, Bar Code ID, Sample (Tons), Gmb, Gmb (DOT), Gmm, Gmm (DOT), Pa, Pa (DOT), Avg Gmb, Avg Gmm, Avg Pa.

GRADATION (%Passing) table with columns for Sieve, Specs, CF10-11, Avg, District, Use DOT. Includes rows for 1 in, 3/4 in, 1/2 in, 3/8 in, #4, #6, #16, #30, #50, #100, #200.

BINDER table with columns for Target, Actual, Spec, Comply?. Includes rows for % Added Binder, % Total Binder, % RAP, % RAS, % Binder Replacement, PG Grade, Gb, Gsb, Pbe (%).

COMPACTED JOINT table with columns for Core #, Station, Joint ID, Gmb. Includes Average Joint Gmb, Average Mat Gmb, % Mat Density, For information Only, Joint Length, Unit Price Adjustment, Joint Price Adjustment.

USE D.O.T. RESULTS (Enter an 'X')

TEST STRIP (Enter an "X")

FILM THICKNESS (FT) [6.0-15.0] table with columns for FT, μm, Price Adjustment.

Gyratory VMA table with columns for VMA, %.

QUANTITY FOR PAYMENT table with columns for Mix Unit Price, Binder Unit Price, Tons of Mix on Road, Tons of Binder, Tons of Waste, Tons of Binder to Date, Tons of Mix to Date.

PLACEMENT RECORD table with columns for From Station, To Station, Lane, Width (ft).

Certified Tech: Brad Karsten, Sally Slaven  
Cert No: C1391, C1489  
Distributor, Dist Materials, Proj Engineer, Contractor

COMPACTED MAT table with columns for Core, Date of Placement, Station, CL Reference, W1 Dry (g), W2 in H2O (g), W3 Wet (g), Gmb, % of Gmm, Pa (%), Thickness (in). Includes note: Cors have been waived.

Course Placed: Surface (Travel Lane). Includes Intended Lift Thickness, Date Placed, Test Date/By, Rich Amendt, Avg. Mat Density, Avg. % of Gmb, Avg. % Field Voids, Q.I. (lower), Q.I. (upper), PWL (total), Pay Factor.

TEMPERATURE, °F table with columns for Time, 7:00, 9:00, 11:00, 1:00, 3:00, 5:00, 7:00, Spec, Comp. Includes rows for Air Temp, Binder Temp, Plant Temp, Mat Temp.

Break Down, Rain Out, Restart after mandatory shutdown, Change information when changes are made to start the day. Identify them on previous day's report.

Table with columns for Old Target, New Target, Tons, Agg, Initial %, New %, Agg, Initial, New.

Comments section for reporting additional information.

9/8/2013

Active Project No.: STP-006-6(74)-2C-52

Contract ID: 52-0015-101

Mix Design No.: ABC13-6043

IOWA DOT ASPHALT PAVING DAILY PLANT REPORT

Contractor: L.L. Pelling

County: Johnson

RAM Lab Number: ABC13-0119 (3.38 % AC)

Active Placement: Surface (Travel Lane)

Mix Type: 10M Surface 1/2 L-3 (HMA)

Active Bid Item: 2303-0053503 10M Surf 1/2in L-3 (HMA)

9/8/13 1:42 PM

Report No.: 1

Lab Voids Target: 4.0

Design Gyration: 96

ABC13-6043

UNCOMPACTED MIXTURE table with columns for Hot Box I.D., Su9-8c, Date Sampled, Time, Station, Side, Sample (Tons), Gmb, Gmm, Pn, Pa, etc.

Article 2303.03,E (Small Quantities) Applies for 300 ton plan quantity

Avg Gmb, Avg Gmm, Avg Pa (%) summary table

GRADATION (%Passing) table with columns for Sieve, Specs, Su9-8c, Avg, District, etc.

BINDER table with columns for Target, Actual, Spec, Comply?, % Added Binder, etc.

COMPACTED JOINT table with columns for Core ID, Lane, Gmb, Pa (%)

USE D.O.T. RESULTS (Enter an "X")

TEST STRIP (Enter an "X")

FILM THICKNESS (FT) [8.0-15.0] table with FT, um, Price Adjustment

Mix Unapproved (See IM 510A) table with VMA, %

QUANTITY FOR PAYMENT table with Mix Unit Price, Binder Unit Price, Tons of Mix on Road, etc.

PLACEMENT RECORD table with From Station, To Station, Lane, Width (ft)

Certified Tech: Taylor Maxfield, Dave McDowell; Dist. Materials; Prof. Engineer; Contractor

COMPACTED MAT table with columns for Core, Station, CL Reference, W1, W2, W3, Diff, Gmb, % of Gmm, Pa, Thickness

Course Placed: Surface (Travel Lane); Thickness QI: 0.96; Intended Lift Thickness: 1.50; Avg. Mat Density: 2.460; Date Placed: 09/08/13; Avg. % of Gmm: 94.300; Test Date/By: 09/08/13; Mike Bloom; Avg. % Field Voids: 5.70

Q.I. (lower) = (0.965 x 2.609) - 2.460 = 1.80 -> PWL (lower) = 98.0; Q.I. (upper) = 2.460 - (0.915 x 2.609) = 2.27 -> PWL (upper) = 99.9; PWL (total) = 98.0 + 99.9 = 197.9; Field Voids Price Adjustment = \$0.00

TEMPERATURE, °F table with columns for Time, Air Temp, Binder Temp, Plant Temp, Mat Temp, Spec, Comply?

Mix Change Information (when changes are made to start the day, identify them on previous day's report): Break Down, Rain Out, Re-start after mandatory shutdown

Table with columns: Old Target, New Target, Tons, Agg, Initial %, New %, Agg, Initial, New %

Comments: The asphalt mixture contains certified asphalt binder and approved aggregate as specified in the approved mix design and was produced in compliance with the provisions of Article 2303.03, E.



**Iowa Department of Transportation**

Highway Division-Office of Materials  
 Proportion & Production Limits For Aggregates

County : Johnson Project No.: STP-006-6(74)--2C-52 Date: 09/08/13  
 Project Location: In Iowa City from 500' N of S Jet IA 1 to Lakeside Dr Mix Design No.: ABC13-6043  
 Contract Mix Tonnage: 300 Course: Surface (Travel Lane) Mix Size (in.): 1/2  
 Contractor: L.L. Pelling Mix Type: HMA (10M ESAL), Surface, 1/2, FRICL-3

Material	Ident #	% in Mix	Producer & Location	Type (A or B)	Friction Type	Beds	Gsb	%Abs
Sand	A52508	11.0%	Williams/S&G Materials Inc	A	4		2.634	0.47
TAT4 M. Sand	A52006	14.0%	Klein/River Products Co	A	4	2-10	2.649	0.84
3/8"chips	A58002	12.0%	Columbus Junction/River Products Co	A	4	16-19	2.583	3.23
3/4" A	A52006	11.0%	Klein/River Products Co	A	4	2-10	2.652	0.86
3/8" Slag	A70008	14.0%	Montpelier/Blackheart Slag	A	2		3.709	1.20
RAP	Surface mi	38.0%	ABC13-0119 (3.38 % AC)	A	2	0	2.662	1.30

Type and Source of Asphalt Binder: 64-28 Bituminous Matr'l & Supply (Tama, IA)

Material	Individual Aggregates Sieve Analysis - % Passing (Target)										
	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
Sand	100	100	100	100	95	90	79	53	16	2	1
TAT4 M. Sand	100	100	100	100	98	76	43	20	8.3	2.8	2.5
3/8"chips	100	100	100	95	50	15	4	2.7	2.6	2.5	2.3
3/4" A	100	100	55	19	4	3	3	2.5	2.5	2	2
3/8" Slag	100	100	100	100	31	1.8	1.6	1.5	1.5	1.4	1
RAP	100	100	93	80	51	36	27	20	14	10	8.8

Preliminary Job Mix Formula Target Gradation

Upper Tolerance	100	100	99	90	61	42		21			6
Comb Grading	100	100	92	83	54	37	26.0	17.0	8.0	5.1	4.4
Lower Tolerance	100	100	85	76	47	32		13			2.4
S.A.sq. m/kg	Total	4.46		+0.41	0.22	0.30	0.43	0.49	0.55	0.62	1.44

Production Limits for Aggregates Approved by the Contractor & Producer.

Sieve Size in.	11.0% of mix Sand		14.0% of mix TAT4 M. Sand		12.0% of mix 3/8"chips		11.0% of mix 3/4" A		14.0% of mix 3/8" Slag		38.0% of mix RAP	
	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max
1"	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0
3/4"	100.0	100.0	100.0	100.0	100.0	100.0	98.0	100.0	100.0	100.0	98.0	100.0
1/2"	100.0	100.0	100.0	100.0	98.0	100.0	48.0	62.0	100.0	100.0	86.0	100.0
3/8"	98.0	100.0	98.0	100.0	88.0	100.0	12.0	26.0	98.0	100.0	73.0	87.0
#4	88.0	100.0	91.0	100.0	43.0	57.0	0.0	11.0	24.0	38.0	44.0	58.0
#8	85.0	95.0	71.0	81.0	10.0	20.0	0.0	8.0	0.0	6.8	31.0	41.0
#30	49.0	57.0	16.0	24.0	0.0	6.7	0.0	6.5	0.0	5.5	16.0	24.0
#200	0.0	3.0	0.5	4.5	0.3	4.3	0.0	4.0	0.0	3.0	6.8	10.8

Comments: This is a revised report which includes field changes to the aggregate proportions

Copies to: \_\_\_\_\_

The above target gradations and production limits have been discussed with and agreed to by an authorized representative of the aggregate producer.

Signed: \_\_\_\_\_  
 Producer

Signed: \_\_\_\_\_  
 Contractor

**Iowa Department of Transportation**

Highway Division - Office of Materials  
HMA Gyratory Mix Design

Letting Date : 4/16/2013  
Mix No. : ABD13-3034  
Contract # :  
Date: 08/22/13

Nmax  
County : Lyon  
Project : STPN-182-1(7)-2J-60  
Mix Size (in.) : 1/2 Type A  
Contractor : TriState  
Design Life ESAL's : 3,000,000  
Mix Type: HMA 3M L - 3  
Location : MP 0 - 9

Aggregate	% in Mix	Source ID	Source Location	Beds	Gsb	%Abs	FAA	Friction
3/8 X 8	10.0%	ASD004	Sioux Falls Quartzite/Concrete Mats	1	2.633	0.35	46.0	2
Manf. Sand	5.5%	ASD004	Sioux Falls Quartzite/Concrete Mats	1	2.633	0.35	46.0	2
4 X 20	27.5%	ASD004	Sioux Falls Quartzite/Concrete Mats	1	2.634	0.30	46.0	2
Sand	17.0%	A84510	Hawarden-North/Lg Everist Inc		2.617	0.76	40.0	4
1/2 Cr. Gravel	25.0%	A60548	O'Conner/Hallett Materials Co		2.669	1.10	46.0	3
RAP/RAS	15.0%	ABC13-0094	11% RAP/4% RAS (8.4% AC)		2.633	1.03	42.0	2

Job Mix Formula - Combined Gradation (Sieve Size in.)

1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
			95	76	48		19			5.9
100	100	100	88	69	43	26	15	9.2	5.6	3.9
100	100	97	81	62	38		11			1.9
100	100	90								

Asphalt Binder Source and Grade:

	Gyratory Data			
	4.60	5.10	5.33	5.60
Adjust grade to PG 58-28	2.315	2.317	2.352	2.391
% Asphalt Binder	2.471	2.460	2.450	2.438
Corrected Gmb @ N-Des.	86.2	86.4	88.2	90.2
Max. Sp.Gr. (Gmm)	93.7	94.2	96.0	98.1
% Gmm @ N- Initial			4.0	1.9
% Gmm @ N-Max	6.3	5.8	4.0	1.9
% Air Voids	17.4	17.8	16.7	15.6
% VMA	63.7	67.3	76.1	87.6
% VFA	9.35	10.25	10.84	11.53
Film Thickness	0.94	0.86	0.81	0.76
Filler Bit. Ratio	2.670	2.678	2.676	2.673
Gse	4.14	4.54	4.80	5.11
Pbe	0.44	0.55	0.52	0.48
Pba	73.5	76.3	77.3	78.5
% New Asphalt Binder	1.0300	1.0300	1.0300	1.0300
Combined Gb @ 25°C				

Number of Gyration

N-Initial  
7  
N-Design  
86  
N-Max  
134  
Gsb for Angularity  
Method A  
2.627  
Pba / %Abs Ratio  
0.29  
Slope of Compaction  
Curve  
Mix Check  
Good  
Pb Range Check  
1.00  
RAM Check  
OK  
Specification Check  
Comply  
Moisture Sensitivity Check  
SIP (0% AS)=11,393  
SIP (0.75% AS)=18,577

Aggregate Type Used	A	Combined		From RAM
		0.00	0.50	
G <sub>ab</sub>	2.640			8.1
G <sub>sa</sub>	2.689			8.5
% Water Abs	0.69			0.0
S.A. m <sup>2</sup> / Kg.	4.43			0.4
Angularity-method A	43			0.0
% Flat & Elongated	0.6			0.4
Sand Equivalent	87			0.4
Virgin G <sub>b</sub> @ 25°C	1.03			5.3
Anti-Strip Dose (%)	0.00	0.50	0.75	
Stripping Inflection Point	11,393	9,382	18,577	

Disposition : An asphalt content of 5.33% is recommended to start this project.  
Data shown in 5.33% column is interpolated from test data.  
The % ADD AC to start project is 4.1%

AS Source: LOF6500  
Dose Rate= 0.75 % of binder

Comments :

Copies to : TriState

Mix Designer & Cert.# : Thuisman CI-515 Signed :

**Iowa Department of Transportation**

Highway Division-Office of Materials  
Proportion & Production Limits For Aggregates

County: Lyon Project No.: STPN-182-1(7)--2I-60 Date: 08/22/13  
 Project Location: IA 182 fto US18 in Inwood N. to IA 9 Mix Design No.: ABD13-3034  
 Contract Mix Tonnage: 13,571 Course: Surface Mix Size (in.): 1/2  
 Contractor: TriState Mix Type: HMA 3M Design Life ESAL's: 3,000,000

Material	Ident #	% in Mix	Producer & Location	Type (A or B)	Friction Type	Beds	Gsb	%Abs
3/8 X 8	ASD004	10.0%	Sioux Falls Quartzite/Concrete Matls Co	A	2	1	2.633	0.35
Manf. Sand	ASD004	5.5%	Sioux Falls Quartzite/Concrete Matls Co	A	2	1	2.633	0.35
4 X 20	ASD004	27.5%	Sioux Falls Quartzite/Concrete Matls Co	A	2	1	2.634	0.30
Sand	A84510	17.0%	Hawarden-North/Lg Everist Inc	A	4		2.617	0.76
1/2 Cr. Gravel	A60548	25.0%	O'Conner/Hallett Materials Co	A	3		2.669	1.10
RAP/RAS	BC13-009	15.0%	11% RAP/4% RAS (8.4% AC)	A	2		2.633	1.03

Type and Source of Asphalt Binder:

Material	Individual Aggregates Sieve Analysis - % Passing (Target)										
	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
3/8 X 8	100	100	100	100	40	4.0	2.0	1.0	1.0	1.0	1.0
Manf. Sand	100	100	100	100	100	97	75	57	37	16	5.6
4 X 20	100	100	100	100	99	46	12	5.8	4.5	3.6	2.8
Sand	100	100	100	100	96	78	55	27	7.5	1.2	0.6
1/2 Cr. Gravel	100	100	88	57	16	8.5	6.2	5.1	4.4	3.7	3.0
RAP/RAS	100	100	99	93	80	67	52	35	26	19	15

Preliminary Job Mix Formula Target Gradation

	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
Upper Tolerance	100	100	100	95	76	48		19		5.9	
Comb Grading	100	100	97	88	69	43	26	15	9.2	5.6	3.9
Lower Tolerance	100	100	90	81	62	38		11		1.9	
S.A.sq. m/kg	Total	4.43		+0.41	0.28	0.35	0.42	0.44	0.57	0.69	1.29

Production Limits for Aggregates Approved by the Contractor & Producer.

Sieve Size in.	10.0% of mix 3/8 X 8		5.5% of mix Manf. Sand		27.5% of mix 4 X 20		17.0% of mix Sand		25.0% of mix 1/2 Cr. Gravel		15.0% of mix RAP/RAS	
	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max
1"	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0		
3/4"	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0		
1/2"	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	81.0	95.0		
3/8"	95.0	100.0	100.0	100.0	98.0	100.0	100.0	100.0	50.0	64.0		
#4	33.0	47.0	95.0	100.0	92.0	100.0	89.0	100.0	9.0	23.0		
#8	0.0	9.0	0.0	100.0	41.0	51.0	73.0	83.0	0.0	13.0		
#30	0.0	5.0	50.0	65.0	0.0	10.0	23.0	31.0	0.0	8.0		
#200	0.0	3.0	0.0	8.0	0.0	4.5	0.0	1.5	0.0	5.0		

Comments:

Copies to: TriState

The above target gradations and production limits have been discussed with and agreed to by an authorized representative of the aggregate producer.

Signed: \_\_\_\_\_  
Producer

Signed: \_\_\_\_\_  
Contractor

**Iowa Department of Transportation**

Highway Division - Office of Materials  
HMA Gyratory Mix Design

Letting Date : 4/16/2013  
Mix No. : ABD13-3034  
Contract #:  
Date: 08/30/13

Nmax  
County : Lyon  
Project : STPN-182-1(7)-2I-60  
Contractor : TriState  
Design Life ESAL's : 3,000,000  
Mix Size (in.) : 1/2 Type A  
Mix Type : HMA 3M L-3  
Location : MP 0-9

IA 182 fro US18 in Inwood N to IA 9

Intended Use :	Surface	Source ID	Source Location	Beds	Gsb	%Abs	FAA	Friction
Aggregate	% in Mix							
3/8 X 8	13.0%	ASD004	Sioux Falls Quartzite/Concrete Matls	1	2.633	0.35	46.0	2
Manf. Sand	8.5%	ASD004	Sioux Falls Quartzite/Concrete Matls	1	2.634	0.30	46.0	2
4 X 20	24.5%	ASD004	Sioux Falls Quartzite/Concrete Matls	1	2.617	0.76	40.0	4
Sand	20.0%	A84510	Hawarden-North/Lg Everist Inc		2.669	1.10	46.0	3
1/2 Cr. Gravel	25.0%	A60548	O'Conner/Hallett Materials Co		2.634	1.16	42.4	2
RAP/RAS	9.0%	ABC13-0094	5% RAP/4% RAS (10.6% AC)					

Job Mix Formula - Combined Gradation (Sieve Size in.)

1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
					Upper Tolerance					
100	100	100	96	75	49		20			5.4
100	100	97	89	68	44	27	16	9.3	5.2	3.4
100	100	90	82	61	39		12			1.4
					Lower Tolerance					

Asphalt Binder Source and Grade:

Adjust grade to PG 58-28	Gyratory Data			
	4.60	5.10	5.33	5.60
% Asphalt Binder	2.315	2.317	2.352	2.391
Corrected Gmb @ N-Des.	2.471	2.460	2.450	2.438
Max. Sp.Gr. (Gmm)	86.2	86.4	88.2	90.2
% Gmm @ N- Initial	93.7	94.2	96.0	98.1
%Gmm @ N-Max	6.3	5.8	4.0	1.9
% Air Voids	17.4	17.8	16.7	15.6
% VMA	63.7	67.3	76.1	87.6
% VFA	9.65	10.54	11.14	11.87
Film Thickness	0.82	0.75	0.71	0.67
Filler Bit. Ratio	2.670	2.679	2.677	2.674
Gse	4.13	4.51	4.77	5.08
Pbe	0.45	0.58	0.55	0.51
Pba	80.0	82.0	82.9	83.7
% New Asphalt Binder	1.0300	1.0300	1.0300	1.0300
Combined Gb @ 25°C				
Aggregate Type Used	A	Combined		From RAM
Gsb	2.639	% Friction Type 4 (+4)	6.1	3.5
Gsa	2.687	Or Better	100.3	3.7
% Water Abs	0.68	% Friction Type 3 (+4)	68.0	0.0
S.A. m <sup>2</sup> / Kg.	4.28	Or Better	94.1	0.2
Angularity-method A	43	% Friction Type 2 (+4)	26.2	0.2
% Flat & Elongated	0.6	% Friction Type 2 (-4)	56.7	0.0
Sand Equivalent	87	Type 2 Fineness Modulus	2.2	0.2
Virgin Gb @ 25°C	1.03	% Crushed	76.0	3.6
Anti-Strip Dose (%)	0.00	0.50	0.75	
Stripping Inflection Point	11,393	9,382	18,577	

Number of Gyration

N-Initial  
7  
N-Design  
86  
N-Max  
134  
Gsb for Angularity  
Method A  
2.627  
Pba / %Abs Ratio  
0.32  
Slope of Compaction  
Curve

Mix Check

Good  
Pb Range Check  
1.00  
RAM Check  
OK

Specification Check

Comply  
Moisture Sensitivity Check

SIP (0% AS)=11,393  
SIP (0.75% AS)=18,577

Disposition: An asphalt content of 5.3% is recommended to start this project.  
Data shown in 5.33% column is interpolated from test data.  
The % ADD AC to start project is 4.4%

AS Source: LOF6500  
Dose Rate= 0.75 % of binder

Comments :

Copies to : TriState

Mix Designer & Cert.# :

Thuisman

CI-515

Signed :

**Iowa Department of Transportation**  
 Highway Division-Office of Materials  
 Proportion & Production Limits For Aggregates

*Revised (REV)*  
*Version*

County: Lyon Project No.: STPN-182-1(7)-2J-60 Date: 08/30/13  
 Project Location: IA 182 from US18 in Inwood N. to IA 9 Mix Design No.: ABD13-3034  
 Contract Mix Tonnage: 13,571 Course: Surface Mix Size (in.): 1/2  
 Contractor: TriState Mix Type: HMA 3M Design Life ESAL's: 3,000,000

Material	Ident #	% in Mix	Producer & Location	Type (A or B)	Friction Type	Beds	Gsb	%Abs
3/8 X 8	ASD004	13.0%	Sioux Falls Quartzite/Concrete Matls Co	A	2	1	2.633	0.35
Manf. Sand	ASD004	8.5%	Sioux Falls Quartzite/Concrete Matls Co	A	2	1	2.633	0.35
4 X 20	ASD004	24.5%	Sioux Falls Quartzite/Concrete Matls Co	A	2	1	2.634	0.30
Sand	A84510	20.0%	Hawarden-North/Lg Everist Inc	A	4		2.617	0.76
1/2 Cr. Gravel	A60548	25.0%	O'Conner/Hallett Materials Co	A	3		2.669	1.10
RAP/RAS	BC13-009	9.0%	5% RAP/4% RAS (10.6% AC)	A	2		2.634	1.16

Type and Source of Asphalt Binder:

Material	Individual Aggregates Sieve Analysis - % Passing (Target)										
	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
3/8 X 8	100	100	100	100	100	40	4.0	2.0	1.0	1.0	1.0
Manf. Sand	100	100	100	100	100	97	75	57	37	16	5.6
4 X 20	100	100	100	100	99	46	12	5.8	4.5	3.6	2.8
Sand	100	100	100	100	96	78	55	27	7.5	1.2	0.6
1/2 Cr. Gravel	100	100	88	57	16	8.5	6.2	5.1	4.4	3.7	3.0
RAP/RAS	100	100	99	95	84	71	56	38	31	23	17

Preliminary Job Mix Formula Target Gradation

Upper Tolerance	100	100	100	96	75	49	20	5.4			
Comb Grading	100	100	97	89	68	44	27	3.4			
Lower Tolerance	100	100	90	82	61	39	12	1.4			
S.A.sq. m/kg	Total	4.28		+0.41	0.28	0.36	0.43	0.46	0.57	0.64	1.11

Production Limits for Aggregates Approved by the Contractor & Producer.

Sieve Size in.	13.0% of mix 3/8 X 8		8.5% of mix Manf. Sand		24.5% of mix 4 X 20		20.0% of mix Sand		25.0% of mix 1/2 Cr. Gravel		9.0% of mix RAP/RAS	
	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max
1"	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0		
3/4"	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	81.0	95.0		
1/2"	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	50.0	64.0		
3/8"	95.0	100.0	100.0	100.0	98.0	100.0	100.0	100.0	9.0	23.0		
#4	33.0	47.0	95.0	100.0	92.0	100.0	89.0	100.0	0.0	13.0		
#8	0.0	9.0	0.0	100.0	41.0	51.0	73.0	83.0	0.0	8.0		
#30	0.0	5.0	50.0	65.0	0.0	10.0	23.0	31.0	0.0	8.0		
#200	0.0	3.0	0.0	8.0	0.0	4.5	0.0	1.5	0.0	5.0		

Comments: \_\_\_\_\_

Copies to: TriState

The above target gradations and production limits have been discussed with and agreed to by an authorized representative of the aggregate producer.

Signed: \_\_\_\_\_  
 Producer

Signed: \_\_\_\_\_  
 Contractor

4/25/13 ver.11.07

9/14/2018

Active Project No.: NHSX-018-8(45)-3H-33
Contract ID: 33-0188-045
Mix Design No.: ABD18-2027



IOWA DOT ASPHALT PAVING DAILY PLANT REPORT

9/15/18 10:38 AM

Contractor: Mathy Construction
County: Fayette
RAP Stockpile ID: ABC14-0118 (5.52 % AC)

Active Placement: Surface (Travel Lane)
Mix Type: HT Surface L - 4 1/2 (HMA)
Active Bid Item: 2303-1043504 HT SURF 1/2IN L-4 (HMA)
Report No.: 9
Lab Voids Target: 4.0
Design Gyration: 75

UNCOMPACTED MIXTURE table with columns for Hot Box I.D., Date Sampled, Time, Station, Bar Code ID, Sample (Tons), Gmb, Gmm, Gmm (DOT), Pa (%), Pa (% (DOT))

COMPACTED JOINT table with columns for Core #, Station, Joint ID, Gmb, Average Joint Gmb, Average Mat Gmb, % Mat Density, Joint Length, Unit Price Adjustment, Joint Incentive

COMPACTED MAT table with columns for Core, Date of Placement, Station, CL Reference, W1 Dry (g), W2 in H2O (g), W3 Wet (g), Gmb, % of Gmm, Pa (%), Thickness (in.)

GRADATION (% Passing) table with columns for Sieve, Specs, CF 9-14 A, Avg, District, Use DOT

USE D.O.T. RESULTS (Enter an 'X')

TEST STRIP (Enter an 'X')

FILM THICKNESS (FT) [8.0-15.0] FT, um 8.1 Price Adjustment \$0.00

Gyratory VMA VMA, % 13.5

QUANTITY FOR PAYMENT table with columns for Mix Unit Price, Binder Unit Price, Tons of Mix on Road, Tons of Binder, Tons of Waste, Tons of Binder to Date, Tons of Mix to Date

Course Placed: Surface (Travel Lane) Thickness QI: 0.49
Intended Lift Thickness: 2.00 Avg. Mat Density: 2.301
Date Placed: 09/14/18 Avg. % of Gmm: 92.433
Test Date/By: 09/15/18 Jimmy Lemke Avg. % Field Voids: 7.57
Q.I. (lower) = (0.965 x 2.489) - 2.301 / 0.027 = 3.74 -> PWL (lower) = 100.0
Q.I. (upper) = 2.301 - (0.915 x 2.489) / 0.027 = 0.87 -> PWL (upper) = 80.3
PWL (total) = 100.0 + 80.3 - 100.0 = 80.3
Pay Factor = 1.000
Tons of Mix for PWL Field Voids Analysis (304.06 deducted) = 584.53 Field Voids Price Adjustment = \$0.00

TEMPERATURE, °F table with columns for Time (7:00, 9:00, 11:00, 1:00, 3:00, 5:00, 7:00), Spec, Comply?

BINDER table with columns for Target, Actual, Spec, Comply?

PLACEMENT RECORD table with columns for From Station, To Station, Lane, Width (ft)

Old Target, New Target, Tons, Agg, Initial %, New %, Agg, Initial, New % table with Comments section

9/15/2018

Active Project No.: NHSX-018-8(45)-3H-33
Contract ID: 33-0188-045
Mix Design No.: ABD18-2027

IOWA DOT ASPHALT PAVING DAILY PLANT REPORT
Contractor: Mathy Construction
County: Fayette
RAP Stockpile ID: ABC14-0116 (5.52 % AC)

Active Placement: Surface (Travel Lane)
Mix Type: HI Surface L - 4 1/2 (HMA)
Active Bid Item: 2303-1043504 HT SURF 1/2IN L-4 (HMA)
Report No.: 10
Lab Voids Target: 4.0
Design Gyration: 75

Table with 5 columns: Hot Box I.D. (Theoretical %AC), 9-15-A (5.30%), 9-15B (5.30%), 9-15C (5.25%), 9-15D (5.26%). Rows include Date Sampled, Time, Station, Bar Code ID, Sample (Tons), Gmb, Gmm, Pn (%), and Pn (%)(DOT).

Table with 5 columns: Sieve, Specs, CF 9-15 A, Avg, District. Rows include 1 in., 3/4 in., 1/2 in., 3/8 in., #4, #8, #16, #30, #50, #100, #200. Includes Dev and Gradation Compliance? sections.

Table with 5 columns: % Added Binder, % Total Binder, % RAP, % RAS, % Binder Replacement, PG Grade, Gb, Gsb, Pbe (%). Rows include Target, Actual, Spec, and Comply? columns.

Table with 4 columns: Core #, Station, Joint ID, Gmb. Rows include 1, 2, 3. Includes Average Joint Gmb, Average Mat Gmb, % Mat Density, and For information Only section.

USE D.O.T. RESULTS (Enter an 'X')

TEST STRIP (Enter an 'X')

Table with 2 columns: FT, Price Adjustment. Row includes 8.2 and \$0.00.

Table with 2 columns: Gyratory VMA, VMA, %. Row includes 13.6.

Table with 2 columns: Mix Unit Price (\$/ton), Binder Unit Price (\$/ton), Tons of Mix on Road, Tons of Binder, Tons of Waste, Tons of Binder to Date, Tons of Mix to Date. Includes \$25.97, \$481.81, 2,389.35, 126.04, 6.00, 971.01, 17,882.01.

Table with 4 columns: From Station, To Station, Lane, Width (ft). Rows include 422+45, 502+20, 502+20, 529+98.46, 524+60.5, 541+20, 541+20, 546+75, 546+75, 549+46, 549+46. Includes Certified Tech: Jay Haas, Jen Stanley and Cert. No. NE208, EC223.

Table with 11 columns: Core, Date of Placement, Station, CL Reference, W1 Dry (g), W2 in H2O (g), W3 Wet (g), Gmb, % of Gmm, Pn (%), Thickness (in.). Rows include 1 through 8.

Course Placed: Surface (Travel Lane) Thickness QI: 1.04
Intended Lift Thickness: 2.00 Avg. Mat Density: 2.341
Date Placed: 09/15/18 Avg. % of Gmm: 94.000
Test Date/By: 09/17/18 Jamie Haas Avg. % Field Voids: 6.00

Q.I. (lower) = (0.965 x 2.491) / 0.020 = 2.341 = 3.14 -> PWL (lower) = 100.0
Q.I. (upper) = 2.341 - (0.915 x 2.491) / 0.020 = 3.09 -> PWL (upper) = 100.0
PWL (total) = 100.0 + 100.0 - 100.0 = 100.0
Pay Factor = 1.040

Tons of Mix for PWL Field Voids Analysis (420.15 deducted)= 1,969.20 Field Voids Incentive = \$2,045.61

Table with 10 columns: Time, 7:00, 9:00, 11:00, 1:00, 3:00, 5:00, 7:00, Spec, Comply?. Rows include Air Temp, Binder Temp, Plant Temp, Mat Temp.

Break Down, Rain Out, Re-start after mandatory shutdown, Mix Change Information (when changes are made to start the day, identify them on previous day's report):

Table with 10 columns: Old Target, New Target, Tons, Agg, Initial %, New %, Agg, Initial, New %. Rows include 2395.35 Tons produced, 6.0 Tons road waste, 2389.35 Tons used for surface on Hwy. 18.

**Iowa Department of Transportation**  
 Highway Division-Office of Materials  
 Proportion & Production Limits For Aggregates

County : Fayette Project No.: NHSX-018-8(45)--3H-33 Date: 09/14/18  
 Project Location: On US 18 from Co. Rd. B64 to the Turkey River in Clermont Mix Design No.: ABD18-2027  
 Contract Mix Tonnage: 17,481 Course: Surface Mix Size (in.): 1/2  
 Contractor: Mathy Construction Mix Type: HT Design Traffic: High Traffic

Material	Ident #	% in Mix	Producer & Location	Type (A or B)	Friction Type	Beds	Gsb	%Abs
1/2" AC	A96004	35.0%	Skyline Materials Ltd/Hovey	A	4	1-6	2.570	2.40
Man. Sand	A96011	34.0%	Bruening Rock Products Inc/Gjetley	A	4	1-3	2.731	1.04
Concrete Sand	A33522	16.0%	Bruening Rock Products Inc/Pape	A	5		2.623	0.69
Classified RAP	rings 2RAL	15.0%	15% ABC14-0116 (5.52 % AC)	A			2.599	1.13
Type and Source of Asphalt Binder:			PG 58-34H MIDWEST LACROSSE, WI					

Material	Individual Aggregates Sieve Analysis - % Passing (Target)										
	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
1/2" AC	100	100	95	70	13	5.0	4.5	4.3	4.2	4.1	3.5
Man. Sand	100	100	100	100	95	64	39	24	11	3.3	1.3
Concrete Sand	100	100	100	100	94	84	72	45	10	0.7	0.3
Classified RAP	100	100	99	97	78	63	54	49	34	15	8.4

Preliminary Job Mix Formula Target Gradation

Upper Tolerance	100	100	100	96	70	51		28			4.9
Comb Grading	100	100	98	89	63	46	34	24	12	4.8	2.9
Lower Tolerance	100	100	91	82	56	41		20			0.9
S.A.sq. m/kg	Total	4.57		+0.41	0.26	0.38	0.56	0.69	0.72	0.59	0.96

Production Limits for Aggregates Approved by the Contractor & Producer.

Sieve Size in.	35.0% of mix 1/2" AC		34.0% of mix Man. Sand		16.0% of mix Concrete Sand		15.0% of mix Classified RAP	
	Min	Max	Min	Max	Min	Max	Min	Max
1"	100.0	100.0	100.0	100.0	100.0	100.0		
3/4"	98.0	100.0	100.0	100.0	100.0	100.0		
1/2"	88.0	100.0	100.0	100.0	100.0	100.0		
3/8"	63.0	77.0	98.0	100.0	98.0	100.0		
#4	6.0	20.0	88.0	100.0	87.0	100.0		
#8	0.0	10.0	59.0	69.0	79.0	89.0		
#30	0.3	8.3	20.0	28.0	41.0	49.0		
#200	1.5	5.5	0.0	3.3	0.0	2.3		

Comments: Item #0140  
 Copies to: Mathy Construction

The above target gradations and production limits have been discussed with and agreed to by an authorized representative of the aggregate producer.

Signed: \_\_\_\_\_  
 Producer

Signed: \_\_\_\_\_  
 Contractor





**Iowa Department of Transportation**  
 Highway Division - Office of Construction & Materials  
 HMA Gyratory Mix Design

Ndesign		Project : NHSX-018-8(45)--3H-33		Letting Date :	1/17/2018			
County :	Fayette	Contractor : Mathy Construction		Mix No. :	ABD18-2027			
Mix Size (in.) :	1/2	Type A	Design Traffic : High Traffic	Contract #:	33-0188-045			
Mix Type:	HT	L - 4		Date:	09/14/18			
Intended Use :	Surface	Location : On US 18 from Co. Rd. B64 to the Turkey River in Clermont						
Aggregate	% in Mix	Source ID	Source Location	Beds	Gsb	%Abs	FAA	Friction
1/2" AC	35.0%	A96004	Skyline Materials Ltd/Hovey	1-6	2.570	2.40	45.0	4
Man. Sand	34.0%	A96011	Bruening Rock Products Inc/Gjetley	1-3	2.731	1.04	45.0	4
Concrete Sand	16.0%	A33522	Bruening Rock Products Inc/Pape		2.623	0.69	38.0	5
Classified RAP	15.0%	prings 2RAP  15% ABC14-0116 (5.52 % AC)			2.599	1.13	39.8	

Job Mix Formula - Combined Gradation (Sieve Size in.)

1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
Upper Tolerance										
100	100	100	96	70	51		28			4.9
<b>100</b>	<b>100</b>	<b>98</b>	<b>89</b>	<b>63</b>	<b>46</b>	<b>34</b>	<b>24</b>	<b>12</b>	<b>4.8</b>	<b>2.9</b>
100	100	91	82	56	41		20			0.9
Lower Tolerance										

Asphalt Binder Source and Grade: MIDWEST LACROSSE, WI PG 58-34H				Gyratory Data		Contribution From RAM	
% Asphalt Binder	5.11	5.34	5.80				
Gmb @ N-Des.	2.377	2.383	2.395				
Max. Sp.Gr. (Gmm)	2.476	2.464	2.440				
% Gmm @ N- Initial	90.1	90.6	91.7				
%Gmm @ N-Max							
% Air Voids	4.0	3.3	1.8				
% VMA	14.4	14.4	14.4				
% VFA	72.3	77.2	87.2				
Film Thickness	9.85	10.48	11.77				
Filler Bit. Ratio	0.64	0.61	0.54				
Gse	2.681	2.676	2.667				
Pbe	4.50	4.79	5.38				
Pba	0.65	0.58	0.45				
% New Asphalt Binder	84.5	85.2	86.4				
Combined Gb @ 25°C	1.0241	1.0240	1.0239				
Aggregate Type Used	A	Combined		Contribution From RAM			
Gsb	2.636	% Friction Type 4 (+4)		88	0		
Gsa	2.742	Or Better		88	0		
% Water Abs	1.47	% Friction Type 3 (+4)		0	0		
S.A. m <sup>2</sup> / Kg.	4.57	Or Better		0	0		
Angularity-method A		% Friction Type 2 (+4)		0	0		
% Flat & Elongated		% Friction Type 2 (-4)		0	0		
Sand Equivalent		Type 2 Fineness Modulus		0.0	0.4		
Virgin Gb @ 25°C	1.023	% Crushed		75.0	5.3		
Anti-Strip Dose (%)	0.00						
Stripping Inflection Point							

Disposition : An asphalt content of 5.1% is recommended to start this project.  
 Data shown in 5.11% column is interpolated from test data.  
 The % ADD AC to start project is 4.3%

Comments : Item #0140 Surface.

One point Volumetrics Verification for RAM substitution.

Copies to : Mathy Construction

DOC Field Materials Tech.

Mix Designer & Cert.# :

Signed : Jon Kleven

Not Required



**Iowa Department of Transportation**  
 Highway Division - Office of Construction & Materials  
 WMA Gyrotory Mix Design

Letting Date : 3/20/2018  
 County : Harrison Project : FM-C043(84)-55-43 Mix No. : ABD18-4057  
 Mix Size (in.) : 1/2 Type A Contractor : Western Engineering Co., Inc Contract # : 43-C043-084  
 Mix Type: ST No Frictn Design Traffic : Standard Traffic Date: 10/22/18  
 Intended Use : Surface Location : On F66 from L-20 E. 4.8 miles to Nixon Ave.

Aggregate	% in Mix	Source ID	Source Location	Beds	Gsb	%Abs	FAA	Friction
5/8" Type A	10.0%	A78002	Schildberg Construction Co/Crescent	25B-25E	2.599	1.50	45.0	5
1/2" Type A	30.0%	A78002	Schildberg Construction Co/Crescent	25B-25E	2.599	1.50	45.0	5
Limestone Mansand	20.0%	ANE010	Martin Marietta Aggregates/Ft Calhou	25B-25E	2.592	1.52	45.0	5
Oakland Sand	40.0%	A78504	Western Engineering Company/Oakla		2.635	0.50	40.0	4

Job Mix Formula - Combined Gradation (Sieve Size in.)

1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
Upper Tolerance										
100	100	100	95	77	55		27			5
<b>100</b>	<b>100</b>	<b>97</b>	<b>88</b>	<b>70</b>	<b>50</b>	<b>34</b>	<b>23</b>	<b>7.7</b>	<b>3.8</b>	<b>3.0</b>
100	100	90	81	63	45		19			1.0
Lower Tolerance										

Asphalt Binder Source and Grade:		FLINT HILLS OMAHA, NE PG 58-28S (AI = 3.6)					WMA Technology & Rate:	
		Gyrotory Data					[Water Injection System @ 0.5 by % of binder]	
% Asphalt Binder	5.25	5.50	<b>5.89</b>	6.25	6.50	<u>Number of Gyrotions</u>		
Gmb @ N-Des.	2.296	2.308	<b>2.321</b>	2.333	2.345	N-Initial		
Max. Sp.Gr. (Gmm)	2.438	2.430	<b>2.418</b>	2.407	2.396	7		
% Gmm @ N- Initial	88.8	89.5	<b>90.4</b>	91.2	92.0	N-Design		
%Gmm @ N-Max						50		
% Air Voids	5.8	5.0	<b>4.0</b>	3.1	2.1	N-Max		
% VMA	16.7	16.5	<b>16.4</b>	16.3	16.1	<u>Gsb for Angularity</u>		
% VFA	65.1	69.6	<b>75.6</b>	81.1	86.7	<u>Method A</u>		
Film Thickness	11.55	12.14	<b>13.01</b>	13.79	14.45	2.624		
Filler Bit. Ratio	0.61	0.58	<b>0.54</b>	0.51	0.49	<u>Pba / %Abs Ratio</u>		
Gse	2.636	2.636	<b>2.638</b>	2.640	2.637	0.35		
Pbe	4.91	5.16	<b>5.53</b>	5.86	6.14	<u>Slope of Compaction</u>		
Pba	0.36	0.36	<b>0.39</b>	0.42	0.38	<u>Curve</u>		
% New Asphalt Binder	100.0	100.0	<b>100.0</b>	100.0	100.0	<u>Mix Check</u>		
Combined Gb @ 25°C	1.0360	1.0360	<b>1.0360</b>	1.0360	1.0360	Excellent		
Aggregate Type Used	A	Contribution		From RAM		<u>Pb Range Check</u>		
G <sub>ab</sub>	2.612	% Friction Type 4 (+4)		11	0	1.25		
G <sub>sa</sub>	2.689	Or Better		11	0	<u>RAM Check</u>		
% Water Abs	1.10	% Friction Type 3 (+4)		0	0	OK		
S.A. m <sup>2</sup> / Kg	4.25	Or Better		0	0	<u>Specification Check</u>		
Angularity-method A	42	% Friction Type 2 (+4)		0	0	Comply		
% Flat & Elongated	1.8	% Friction Type 2 (-4)		0	0	<u>Hamburg Check</u>		
Sand Equivalent	92	Type 2 Fineness Modulus		0.0	0.0	Not Required		
Virgin G <sub>b</sub> @ 25°C	1.036	% Crushed		60.0	0			
Anti-Strip Dose (%)	0.00							
Stripping Inflection Point								

Disposition : An asphalt content of 5.9% is recommended to start this project. Target plant temp is 270 °F  
 Data shown in 5.89% column is interpolated from test data.

Comments : \_\_\_\_\_  
 \_\_\_\_\_  
 Copies to : Western Engineering Co., Inc

Mix Designer & Cert.# : Eric Labenz SW585 Signed : Marcia Buthmann District 4 Materials

**Iowa Department of Transportation**  
 Highway Division-Office of Materials  
 Proportion & Production Limits For Aggregates

County : Harrison Project No.: FM-C043(84)--55-43 Date: 10/22/18  
 Project Location: On F66 from L-20 E. 4.8 miles to Nixon Ave. Mix Design No.: ABD18-4057  
 Contract Mix Tonnage: 5,285 Course: Surface Mix Size (in.): 1/2  
 Contractor: Western Engineering Co., Inc Mix Type: ST Design Traffic: Standard Traffic

Material	Ident #	% in Mix	Producer & Location	Type (A or B)	Friction Type	Beds	Gsb	%Abs
5/8" Type A	A78002	10.0%	Schildberg Construction Co/Crescent	A	5	25B-25E	2.599	1.50
1/2" Type A	A78002	30.0%	Schildberg Construction Co/Crescent	A	5	25B-25E	2.599	1.50
Limestone Mansand	ANE010	20.0%	Martin Marietta Aggregates/Ft Calhoun	A	5	25B-25E	2.592	1.52
Oakland Sand	A78504	40.0%	Western Engineering Company/Oakland	A	4		2.635	0.50

Type and Source of Asphalt Binder: PG 58-28S FLINT HILLS OMAHA, NE

Material	Individual Aggregates Sieve Analysis - % Passing (Target)										
	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
5/8" Type A	100	100	80	58	27	11	6.6	5.5	5.0	4.9	4.4
1/2" Type A	100	100	95	73	37	15	11	8.1	7.0	6.3	5.5
Limestone Mansand	100	100	100	100	99	59	22	12	6.4	4.3	2.7
Oakland Sand	100	100	100	100	92	81	65	44	9.5	1.5	1.0

**Preliminary Job Mix Formula Target Gradation**

Upper Tolerance	100	100	100	95	77	55		27			5.0
Comb Grading	100	100	97	88	70	50	34	23	7.7	3.8	3.0
Lower Tolerance	100	100	90	81	63	45		19			1.0
S.A.sq. m/kg	Total	4.25		+0.41	0.29	0.41	0.56	0.66	0.47	0.47	0.99

**Production Limits for Aggregates Approved by the Contractor & Producer.**

Sieve Size in.	10.0% of mix 5/8" Type A		30.0% of mix 1/2" Type A		20.0% of mix Limestone Mansand		40.0% of mix Oakland Sand	
	Min	Max	Min	Max	Min	Max	Min	Max
1"	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0
3/4"	98.0	100.0	98.0	100.0	100.0	100.0	100.0	100.0
1/2"	73.0	87.0	88.0	100.0	100.0	100.0	100.0	100.0
3/8"	51.0	65.0	66.0	80.0	98.0	100.0	98.0	100.0
#4	20.0	34.0	30.0	44.0	92.0	100.0	85.0	99.0
#8	6.0	16.0	10.0	20.0	54.0	64.0	76.0	86.0
#30	1.5	9.5	4.1	12.1	8.0	16.0	40.0	48.0
#200	2.4	6.4	3.5	7.5	0.7	4.7	0.0	3.0

Comments: \_\_\_\_\_

Copies to: Western Engineering Co., Inc

The above target gradations and production limits have been discussed with and agreed to by an authorized representative of the aggregate producer.

Signed: \_\_\_\_\_  
 Producer

Signed: \_\_\_\_\_  
 Contractor

4/25/13 ver:11.07

11/13/2018
Active Project No.: FM-C043(84)-55-43
Contract ID: 43-C043-084
Mix Design No.: ABD18-4057

IOWA DOT ASPHALT PAVING DAILY PLANT REPORT
Contractor: Western Engineering Co., Inc
County: Harrison
RAP Stockpile ID:

Active Placement: Surface (Travel Lane)
Mix Type: ST Surface None 1/2 (HMA)
Active Bid Item: 2303-1033500 ST SURF 1/2IN NO (HMA)
Report No.: 4
Lab Voids Target: 4.0
Design Gyration: 50

11/20/18 10:42 AM

Table with columns for Hot Box I.D., Date Sampled, Time, Station, Bar Code ID, Sample (Tons), Gmb, Gmm, Gmm (DOT), Pa (%), Pa (% (DOT)), and Gradation (%Passing) with sieve sizes.

Table for COMPACTED JOINT with columns for Core #, Station, Joint ID, Gmb, Average Joint Gmb, Average Mat Gmb, % Mat Density, and Joint Price Adjustment.

USE D.O.T. RESULTS (Enter an 'X')

TEST STRIP (Enter an 'X')

Table for FILM THICKNESS (FT) [8.0-15.0] with columns for FT, um, and Price Adjustment.

Table for Gyratory VMA with columns for VMA, % and value 16.2.

Table for QUANTITY FOR PAYMENT with columns for Mix Unit Price (\$/ton), Binder Unit Price (\$/ton), Tons of Mix on Road, Tons of Binder, Tons of Waste, Tons of Binder to Date, and Tons of Mix to Date.

Table for BINDER with columns for Target, Actual, Spec, and Comply? for % Added Binder, % Total Binder, % RAP, % RAS, % Binder Replacement, and PG Grade.

Table for PLACEMENT RECORD with columns for From Station, To Station, Lane, and Width (ft).

Certified Tech: Nathan Underwood, Kay Petersen
Distributor: Dist. Materials, Proj. Engineer, Contractor

Table for COMPACTED MAT with columns for Core #, Date of Placement, Station, CL Reference, W1 Dry (g), W2 in H2O (g), W3 Wet (g), Gmb, % of Gmm, Pa (%), and Thickness (in.).

Summary table for Course Placed: Surface (Travel Lane), Intended Lift Thickness: 1.50, Date Placed: Multiple, Test Date/By: 11/20/18, Karley Arman, and calculations for Q.I. (lower), Q.I. (upper), PWL (total), and Pay Factor = 1.040.

Table for TEMPERATURE, °F with columns for Time (7:00, 9:00, 11:00, 1:00, 3:00, 5:00, 7:00), Spec, and Comply? for Air Temp, Binder Temp, Plant Temp, and Mat Temp.

Table for Old Target, New Target, Tons, Agg, Initial %, New %, Agg, Initial, New % with checkboxes for Break Down, Rain Out, and Re-start after mandatory shutdown.

Comments:
Road Waste- 0 Tons



**Iowa Department of Transportation**  
 Highway Division - Office of Construction & Materials  
 WMA Gyrotory Mix Design

Project : FM-C088(55)--55-88  
 Contractor : Henningsen Const. Inc.  
 Design Traffic : High Traffic  
 Location : On P-53 from US-34 north 6.4 miles to H-17 REA road  
 Letting Date : 1/17/2018  
 Mix No. : ABD18-4063  
 Contract # : 88-C088-058  
 Date : 10/25/18

Aggregate	% in Mix	Source ID	Source Location	Beds	Gsb	%Abs	FAA	Friction
sand	14.0%	A25518	Martin Marietta Aggregates/Raccoon		2.611	0.61	40.0	5
man sand	16.0%	A61002	Schildberg Construction Co/Early Cha	15A-15C	2.582	1.88	45.0	5
3/4" clean	18.0%	A63002	Martin Marietta Aggregates/Durham	101	2.519	2.62	45.0	4
3/8" chips	24.0%	A63002	Martin Marietta Aggregates/Durham	101	2.519	2.62	45.0	4
qtz man sand	13.0%	ASD002	L G Everist Inc/Dell Rapids-East		2.635	0.37	47.0	2
Classified RAP	15.0%	ABC2-208	15% ABC2-208 (4.45 % AC)		2.570	1.85	41.6	

Job Mix Formula - Combined Gradation (Sieve Size in.)

1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
Upper Tolerance										
100	100	100	97	84	46		19			4.6
<b>100</b>	<b>100</b>	<b>95</b>	<b>90</b>	<b>77</b>	<b>41</b>	<b>23</b>	<b>15</b>	<b>6.4</b>	<b>3.4</b>	<b>2.6</b>
100	100	88	83	70	36		11			0.6
Lower Tolerance										

Asphalt Binder Source and Grade:					BITUMINOUS MATERIALS TAMA, IA		PG 58-28H (AI = 2.6)		WMA Technology & Rate:		
					Gyrotory Data					[Water Injection System @ 1.8% added a/c]	
% Asphalt Binder	5.30	<b>5.36</b>	5.80							<u>Number of Gyration</u>	
Gmb @ N-Des.	2.294	<b>2.296</b>	2.307							N-Initial	
Max. Sp.Gr. (Gmm)	2.393	<b>2.391</b>	2.380							8	
% Gmm @ N-Initial	88.1	<b>88.2</b>	88.7							N-Design	
%Gmm @ N-Max		<b>96.1</b>								75	
% Air Voids	4.1	<b>4.0</b>	3.1							N-Max	
% VMA	15.3	<b>15.3</b>	15.2								
% VFA	72.9	<b>73.8</b>	79.9							<u>Gsb for Angularity</u>	
Film Thickness	14.25	<b>14.45</b>	15.52							<u>Method A</u>	
Filler Bit. Ratio	0.52	<b>0.51</b>	0.47							2.599	
Gse	2.582	<b>2.582</b>	2.586							<u>Pba / %Abs Ratio</u>	
Pbe	5.03	<b>5.10</b>	5.48							0.16	
Pba	0.28	<b>0.28</b>	0.34							<u>Slope of Compaction Curve</u>	
% New Asphalt Binder	88.0	<b>88.1</b>	89.1								
Combined Gb @ 25°C	1.0379	<b>1.0379</b>	1.0380								
Aggregate Type Used	A		Combined	Contribution From RAM						<u>Mix Check</u>	
G <sub>ab</sub>	2.564		% Friction Type 4 (+4)	71	0					Good	
G <sub>sa</sub>	2.689		Or Better	72	0					<u>Pb Range Check</u>	
% Water Abs	1.81		% Friction Type 3 (+4)	0	0					0.50	
S.A. m <sup>2</sup> / Kg.	3.53		Or Better	1	0					<u>RAM Check</u>	
Angularity-method A	44		% Friction Type 2 (+4)	1	0					OK	
% Flat & Elongated	7.5		% Friction Type 2 (-4)	17	0					<u>Specification Check</u>	
Sand Equivalent	91		Type 2 Fineness Modulus	0.4	0.5					Comply	
Virgin G <sub>b</sub> @ 25°C	1.039		% Crushed	80.0	8.7					<u>Hamburg Check</u>	
Anti-Strip Dose (%)	0.00									Not Required	
Stripping Inflection Point											

Disposition : An asphalt content of 5.4% is recommended to start this project. Target plant temp is 255 °F  
 Data shown in 5.36% column is interpolated from test data.

The % ADD AC to start project is 4.7%

Comments : Also for use on FM-C088(58)--55-88

Copies to : Henningsen Const. Inc.

Mix Designer & Cert.# : RW Hansn SW 046 Signed : Marcia Buthmann District 4 Materials

**Iowa Department of Transportation**  
 Highway Division-Office of Materials  
 Proportion & Production Limits For Aggregates

County : Union Project No.: FM-C088(55)--55-88 Date: 10/25/18  
 Project Location: On P-53 from US-34 north 6.4 miles to H-17 REA road Mix Design No.: ABD18-4063  
 Contract Mix Tonnage: 15,525 Course: Surface Mix Size (in.): 1/2  
 Contractor: Henningsen Const. Inc. Mix Type: HT Design Traffic: High Traffic

Material	Ident #	% in Mix	Producer & Location	Type (A or B)	Friction Type	Beds	Gsb	%Abs
sand	A25518	14.0%	Martin Marietta Aggregates/Raccoon River	A	5		2.611	0.61
man sand	A61002	16.0%	Schildberg Construction Co/Early Chapel-I	A	5	15A-15C	2.582	1.88
3/4" clean	A63002	18.0%	Martin Marietta Aggregates/Durham Mine	A	4	101	2.519	2.62
3/8" chips	A63002	24.0%	Martin Marietta Aggregates/Durham Mine	A	4	101	2.519	2.62
qtz man sand	ASD002	13.0%	L G Everist Inc/Dell Rapids-East	A	2		2.635	0.37
Classified RAP	ABC2-208	15.0%	15% ABC2-208 (4.45 % AC)	A			2.570	1.85

Type and Source of Asphalt Binder: PG 58-28H BITUMINOUS MATERIALS TAMA, IA

Material	Individual Aggregates Sieve Analysis - % Passing (Target)										
	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
sand	100	100	100	100	96	83	65	40	7.5	0.8	0.8
man sand	100	100	100	100	87	30	8.3	4.2	3.2	2.7	2.5
3/4" clean	100	99	78	55	12	2.0	1.5	1.4	1.3	1.1	0.9
3/8" chips	100	100	100	100	98	28	3.0	2.0	1.8	1.6	1.2
qtz man sand	100	100	100	100	99	74	47	29	12	2.7	0.7
Classified RAP	100	99	95	89	72	52	38	28	18	13	11

Preliminary Job Mix Formula Target Gradation

Upper Tolerance	100	100	100	97	84	46		19			4.6
Comb Grading	100	100	95	90	77	41	23	15	6.4	3.4	2.6
Lower Tolerance	100	100	88	83	70	36		11			0.6
S.A.sq. m/kg	Total	3.53		+0.41	0.31	0.33	0.38	0.43	0.39	0.41	0.87

Production Limits for Aggregates Approved by the Contractor & Producer.

Sieve Size in.	14.0% of mix sand		16.0% of mix man sand		18.0% of mix 3/4" clean		24.0% of mix 3/8" chips		13.0% of mix qtz man sand		15.0% of mix Classified RAP	
	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max
1"	100.0	100.0	100.0	100.0	98.0	100.0	100.0	100.0	100.0	100.0		
3/4"	100.0	100.0	100.0	100.0	92.0	100.0	100.0	100.0	100.0	100.0		
1/2"	100.0	100.0	100.0	100.0	71.0	85.0	100.0	100.0	100.0	100.0		
3/8"	98.0	100.0	98.0	100.0	48.0	62.0	98.0	100.0	98.0	100.0		
#4	89.0	100.0	80.0	94.0	5.0	19.0	91.0	100.0	92.0	100.0		
#8	78.0	88.0	25.0	35.0	0.0	7.0	23.0	33.0	69.0	79.0		
#30	36.0	44.0	0.2	8.2	0.0	5.4	0.0	6.0	25.0	33.0		
#200	0.0	2.8	0.5	4.5	0.0	2.9	0.0	3.2	0.0	2.7		

Comments: \_\_\_\_\_

Copies to: Henningsen Const. Inc. \_\_\_\_\_

The above target gradations and production limits have been discussed with and agreed to by an authorized representative of the aggregate producer.

Signed: \_\_\_\_\_  
 Producer

Signed: \_\_\_\_\_  
 Contractor

4/25/13 ver.11.07

11/8/2018

Active Project No.: FM-C088(55)--55-88  
Contract ID: 88-C088-058  
Mix Design No.: ABD18-40631



IOWA DOT ASPHALT PAVING DAILY PLANT REPORT

11/15/18 6:48 AM

Contractor: Henningsen Const. Inc.  
County: Union  
RAP Stockpile ID: ABC2-208 (4.45 % AC)

Active Placement: Surface (Travel Lane)  
Mix Type: Wma Ht Surface None 1/2 (WMA)  
Active Bid Item: 2303-1043500 HT SURF 1/2IN NO (HMA)  
Report No.: 3  
Lab Voids Target: 4.0  
Design Gyration: 75

UNCOMPACTED MIXTURE table with columns for Hot Box I.D., SU11-8A, SU11-8B, SU11-8C, Date Sampled, Time, Station, Bar Code ID, Sample (Tons), Gmb, Gmm, Pn (%), Pn (%)(DOT)

PWL=99.6

GRADATION (%Passing) table with columns for Sieve, Specs, CF 11-8-18, Avg, Use DOT District

BINDER table with columns for Target, Actual, Spec, Comply?

COMPACTED JOINT table with columns for Core #, Station, Joint ID, Gmb

USE D.O.T. RESULTS (Enter an 'X')

TEST STRIP (Enter an 'X')

FILM THICKNESS (FT) table with columns for FT, Price Adjustment

Gyratory VMA table with column for VMA, %

QUANTITY FOR PAYMENT table with columns for Mix Unit Price, Binder Unit Price, Tons of Mix on Road, Tons of Binder to Date

PLACEMENT RECORD table with columns for From Station, To Station, Lane, Width (ft)

Certified Tech: David Updike, Dawn Updike  
Distribution: Dist Materials, Proj Engineer, Contractor

COMPACTED MAT table with columns for Core, Date of Placement, Station, CL Reference, W1 Dry (g), W2 in H2O (g), W3 Wet (g), Gmb, % of Gmm, Pa (%), Thickness (in.)

Course Placed: Surface (Travel Lane) Thickness QI: 1.16  
Intended LIR Thickness: 1.50  
Date Placed: 11/08/18  
Test Date/By: 11/15/18 Jeff Eslinger

Q.I. (lower) = (0.965 x 2.394) / 0.020 = 4.86  
Q.I. (upper) = 2.213 / 0.020 = 1.12  
PWL (total) = 100.0 + 87.0 = 187.0  
Pay Factor = 1.000

Tons of Mix for PWL Field Voids Analysis (00.00 deducted)= 1,804.89 Field Voids Price Adjustment = \$0.00

TEMPERATURE, °F table with columns for Time, Air Temp, Binder Temp, Plant Temp, Mat Temp, Spec, Comply?

Break Down, Rain Out, Restart after mandatory shutdown, Mix Change Information

Table with columns for Old Target, New Target, Tons, Agg, Initial %, New %, Agg, Initial, New %

Comments:

425/13 ver.11.07

11/7/2018

Active Project No.: FM-C088(55)-55-88
Contract ID: 88-C088-058
Mix Design No.: ABD18-4063r1

IOWA DOT ASPHALT PAVING DAILY PLANT REPORT

Contractor: Henningsen Const. Inc.
County: Union
RAP Stockpile ID: ABC2-208 (4.45 % AC)

Active Placement: Surface (Travel Lane)
Mix Type: WMA HT Surface None 1/2 (WMA)
Active Bid Item: 2303-1043500 HT SURF 1/2IN NO (HMA)

11/8/18 1:27 PM

Report No.: 2
Lab Voids Target: 4.0
Design Gyrator: 75

UNCOMPACTED MIXTURE table with columns for Hot Box I.D., Date Sampled, Time, Station, Bar Code ID, Sample (Tons), Gmb, Gmm, Gmm (DOT), Pa (%), Pa (% (DOT))

AAD=0.4

GRADATION (%Passing) table with columns for Sieve, Specs, CF 11-7-18, Avg, Use DOT District

BINDER table with columns for Target, Actual, Spec, Comply?

COMPACTED JOINT table with columns for Core #, Station, Joint ID, Gmb

USE D.O.T. RESULTS (Enter an 'X')

TEST STRIP (Enter an "X")

FILM THICKNESS (FT) [8.0-15.0] table with columns for FT, Price Adjustment

Gyratory VMA VMA, % 15.5

QUANTITY FOR PAYMENT table with columns for Mix Unit Price, Binder Unit Price, Tons of Mix on Road, etc.

PLACEMENT RECORD table with columns for From Station, To Station, Lane, Width (ft)

Certified Tech: David Updike, Dawn Updike
Distribution: Dist. Materials, Proj. Engineer, Contractor

COMPACTED MAT table with columns for Core, Date of Placement, Station, CL Reference, W1 Dry (g), W2 In H2O (g), W3 Wet (g), Gmb, % of Gmm, Pa (%), Thickness (in.)

Course Placed: Surface (Travel Lane) Thickness CI: 1.15
Intended Lift Thickness: 1.50
Date Placed: 11/07/18
Test Date/By: 11/08/18 Jeff Eslinger

Q.I. (lower) = (0.965 x 2.397) / 0.024 = 4.05 -> PWL (lower) = 100.0
Q.I. (upper) = 2.216 / (0.915 x 2.397) = 0.95 -> PWL (upper) = 82.6
PWL (total) = 100.0 + 82.6 - 100.0 = 82.6

Pay Factor = 1.000
Tons of Mix for PWL Field Voids Analysis (00.00 deducted) = 1,809.56 Field Voids Price Adjustment = \$0.00

TEMPERATURE, °F table with columns for Time, Air Temp, Binder Temp, Plant Temp, Mat Temp, Spec, Comply?

Break Down, Rain Out, Re-start after mandatory shutdown, Mix Change Information

Table with columns: Old Target, New Target, Tons, Agg, Initial %, New %, Agg, Initial, New %

Comments:





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