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ALTERNATIVE FLEXIBLE OVERLAYS

CONSTRUCTION REPORT
IOWA HIGHWAY RESEARCH BOARD
PROJECT HR-229

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Iowa Department
of Transportation

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PROJECT HR-229

ALTERNATIVE FLEXIBLE OVERLAYS

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Table of Contents

	<u>Page</u>
Acknowledgement - - - - -	1
Introduction - - - - -	2
Objective - - - - -	3
Project Description - - - - -	3
Plan Preparation - - - - -	3
Test Sections - - - - -	5
Mix Designs - - - - -	7
Construction - - - - -	8
Preparation for Road Mixing - - - - -	8
Road Mixing - - - - -	10
Plant Mixing and Paver Laying - - - - -	14
Construction Testing - - - - -	15
Plant Mix Testing - - - - -	15
Road Mix Testing - - - - -	16
Post Construction Performance - - - - -	16
Performance of Plant Mix Sections - - - - -	16
Performance of Road Mix Sections - - - - -	17
Construction Costs - - - - -	18
Discussion and Summary - - - - -	18
Plant Mixed Sections - - - - -	18
Road Mixed Sections - - - - -	20
Appendix	
A. Contract Quantities and Special Provisions - - - - -	22
B. Aggregate Test Reports - - - - -	27
C. Test Section Layout - - - - -	31
D. Mix Design Reports - - - - -	34
E. Asphalt Penetrations and Viscosities - - - - -	47
F. Density Test Results - - - - -	49
G. Maintenance Work and Seal Coat Construction - - - - -	51

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The authors wish to extend appreciation to the Osceola County Board of Supervisors and the Iowa DOT for their support in developing and conducting this project. We also wish to thank the Rohlin Construction Company for their cooperation during the project. The Osceola County inspection personnel also deserve recognition for the extra effort put forth on the project.

INTRODUCTION

Many of the first paved roads in Iowa, particularly in the northwest part of the state, were constructed by using a cutback asphalt mixed with crushed pit run gravel. With low traffic volumes, this type of flexible bituminous pavement has performed well showing little sign of transverse cracking or deterioration of the asphalt binder.

With time, the county road departments began constructing paved roads of hot mix that normally contained 85 to 100 penetration asphalts. The mixes were produced at a central plant and laid with an asphalt paver. The result was a smooth, hard, uniform asphalt concrete roadway. Transverse cracking of these pavements has become a costly maintenance problem. One reason for the cracks is the brittle pavement behaviour at low temperatures. As degradation occurs at the crack, a depression forms. The result is a reduction in riding quality and a loss of pavement life.

In an attempt to avoid the cracking problem, highway engineers are looking for ways of improving the low temperature characteristics of asphalt pavements with little sacrifice in the moderate to high temperature characteristics. One way to do this may be to return to a cutback or emulsified asphalt for light traffic county roads. Research Project HR-229 has been initiated to construct several flexible bituminous base sections which have the potential of resisting thermal cracking at low temperatures and resisting rutting, shoving and bleeding at high temperatures.

OBJECTIVE

The objective of the project is to construct and evaluate several bituminous concrete base overlays which have the potential to reduce future maintenance and construction costs.

PROJECT DESCRIPTION

Two roadways in Osceola County were selected for placement of the various overlays. The projects are a 2.6 mile section of county road A-34 and a 7.0 mile section of county road A-46 (Figure 1). The existing roadbeds of A-34 and the east four miles of A-46 consist of a 3" cold laid bituminous concrete base over a 6" rolled gravel base. The west three miles of A-46 were constructed as Iowa Highway Research Project HR-18 in 1952 and consist of various bases with a cold laid bituminous concrete base wearing surface. Average daily traffic is 138 to 195 vehicles for A-34 and 135 to 219 for A-46.

PLAN PREPARATION

The original concept for the project included four bituminous concrete overlay test sections and a control section of Type B asphalt cement concrete overlay to be constructed on two separate roadways. It was later decided to add test sections utilizing cold mix recycling on A-46. Four 1/2 mile test sections were added to the project. The additional sections were to be constructed by removing 1 1/2" of the existing 3" bituminous pavement, adding new aggregate and bituminous binder, and relaying the mix.

The construction plans and special provisions for A-46 were developed to allow for alternate construction. The first alternative was seven miles of bituminous overlay and the second alternative was five miles of bituminous

OSCEOLA COUNTY IOWA

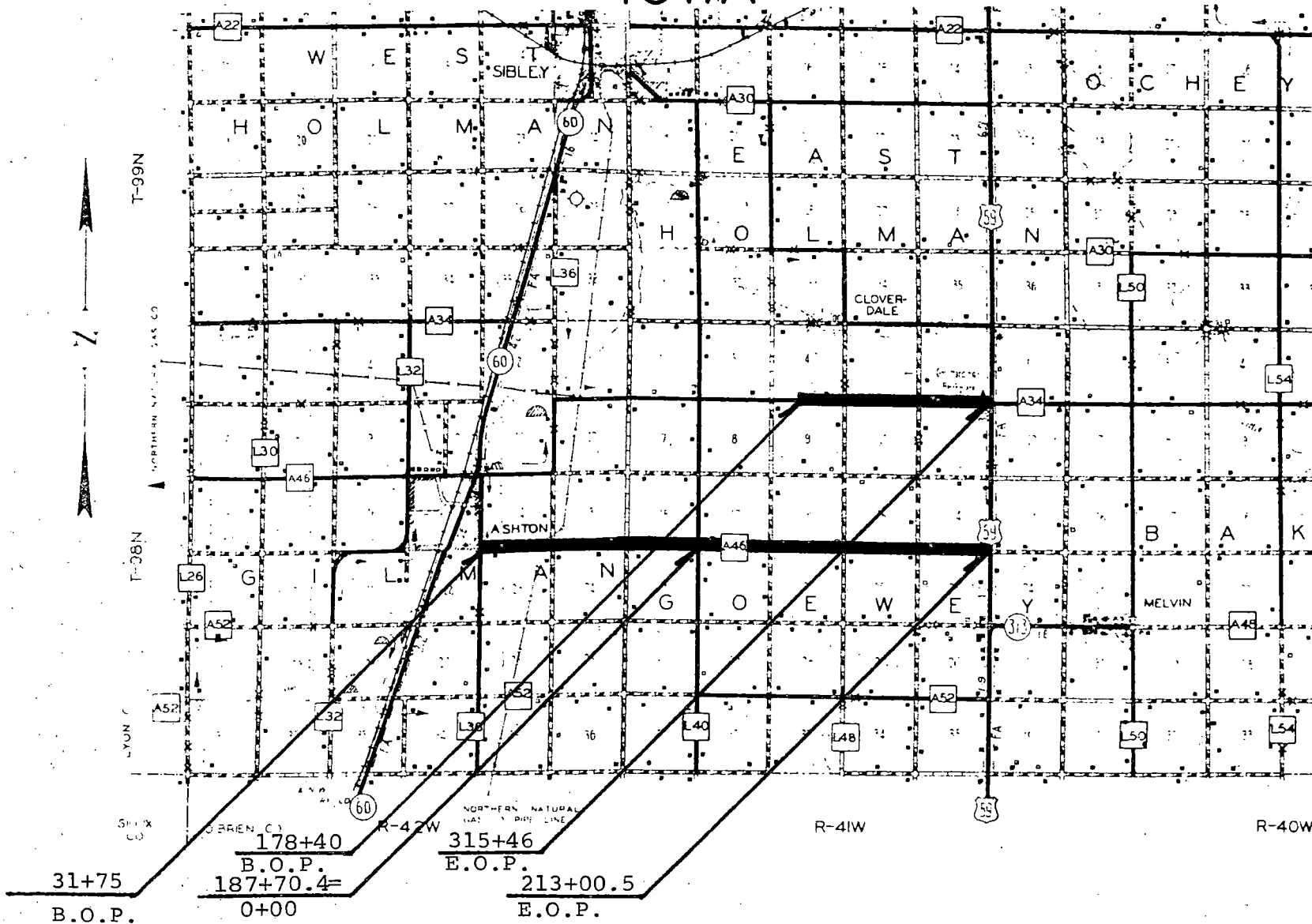


Figure 1
Project Layout

overlay and two miles of cold mix pavement recycling. Contractor bids for the A-46 project were to be submitted on the first construction alternative only. It was intended that, if determined feasible, alternative 2 would be constructed. Payment for all work in the recycled portion of alternative 2 was to be made on the basis of the contract quantities of alternative 1 for items in that area, with no measurement for payment. Special provisions and contract quantities for both A-34 and A-46 are in Appendix A.

TEST SECTIONS

The various bituminous concrete bases were mixed using the following six bituminous binders from Bituminous Materials of Algona, Iowa:

1. AC-5 grade asphalt cement. Penetration of the asphalt was to be a minimum of 140. The AC-5 asphalt was the control section for comparison.
2. MC-3000 grade cutback asphalt. Residue from the distillation test of this material was to be a minimum of 140 penetration.
3. MC-800 grade cutback asphalt. The MC-800 was added to the project after trial mixes with some of the intended aggregates indicated adequate performance could be achieved with the softer asphalt.
4. SC-800 grade liquid asphalt. ASTM D 2026 was the only requirement specified for this material.
5. HFMS - 2 anionic emulsified asphalt with a minimum of 5% oil distillate. Again a minimum penetration of 140 was specified for the residue from the distillation test.

6. CSS - 1 cationic emulsified asphalt with a minimum of 5% oil distillate. The cationic emulsified asphalt was also to have a penetration of at least 140 on the residue.

Gravel aggregate for the bituminous concrete sections, the bituminous recycled sections, and the Type B asphalt concrete control sections was produced by Maudlin Construction Company. Fifteen percent pea gravel from Floyd River Sand and Gravel was added to the 3/4" gravel for the Type B acc control section on A-46. All other sections were constructed using only Maudlin gravel. See Appendix B for aggregate test reports.

On A-46, ten test sections were constructed 22 foot wide using the bituminous binders. Six of the ten sections were mixed at a central plant with 3/4" gravel aggregate and laid with a paver to a 2" nominal thickness. The other four sections consisted of 67% milled bituminous pavement from the road and 33% virgin aggregate. This blend was mixed on the road with four of the bituminous binders and placed 2 1/4" thick with a motor patrol. The test sections are:

<u>Section No.</u>	<u>Binder</u>	<u>Asphalt Added %</u>	<u>Mix Type</u>	<u>Section Length (Ft.)</u>
1	AC-5	6.6	Plant Mix	5940
2	MC-3000	5.7 5.3	Plant Mix	1365 8550
3	HFMS-2	6.4	Plant Mix	2440
4	HFMS-2	4.7	Road Mix	2601
5	CSS-1	4.9	Road Mix	2524
6	CSS-1	6.5	Plant Mix	2905
7	MC-3000	5.5	Plant Mix	2620
8	MC-800	2.9	Road Mix	5214
9	SC-800	2.8	Road Mix	2556
10	SC-800	5.1 4.6	Plant Mix	1600 1085

On A-34, four test sections were constructed 23 foot wide. The sections were mixed at a central plant with 1/2" gravel aggregate and laid with the full width paver. Original plans specified a nominal 3/4" overlay, but due to construction problems, the thickness had to be increased to 1 1/8" and thicker. The test sections are:

<u>Section No.</u>	<u>Binder</u>	<u>Asphalt %</u>	<u>Thickness (In.)</u>	<u>Section Length (Ft.)</u>
11	HFMS-2	6.4	1 1/2	1520
*12	AC-5	6.4	1 1/4	2875
13	MC-3000	5.2	1 1/8	4570
14	SC-800	5.4	1 1/8	4876

*Constructed in 1982 due to failure of original section.

Plan layouts for the test sections are shown in Appendix C.

MIX DESIGNS

Fourteen mix designs were prepared for the research project. Preparing trial mixes for Marshall testing required some deviation from standard asphalt concrete mix preparation. The MC-3000 and SC-800 mixes with the 3/4" and 1/2" gravels were mixed at 180°F. A curing time of 16 hours at a temperature of 140°F was allowed before molding the Marshall specimens. Marshall testing was done at 77°F.

The 3/4" and 1/2" gravels for mixes with HFMS-2 and CSS-1 were wetted to 5.5 percent moisture prior to mixing. Mixing, curing and molding temperature for the emulsion mixes was 130°F. The cure time before molding specimens was 16 hours and the Marshall testing was done at 77°F.

Mixes for the blend of milled pavement and new aggregate were mixed, cured and compacted at room temperature. The MC-800 and SC-800 were heated to 160°F prior to mixing, while the HFMS-2 and CSS-1 emulsions were

applied at room temperature to the aggregate blend. The mixes were allowed to cure for 20 hours before compacting and were again tested at 77°F. The mix design reports are in Appendix D.

CONSTRUCTION

The construction began on September 14, 1981. Rohlin Construction Company of Estherville, Iowa was the contractor.

Preparation For Road Mixing

The contractor began construction by milling the two miles of pavement on A-46. A 12 foot wide CMI Rotomill was used to remove 1 1/2" of the existing 3" bituminous pavement (Figure 2). The milling was completed in two days. Milling for the sections was done without water to avoid adding excess moisture to the material.

After completion of the milling, virgin gravel was hauled to the road to be mixed at the rate of 1:2 with the milled bituminous material. Both a Seaman Pulverizer and a Bros Pulverizer were used to blend the materials and to further break up the millings. Despite many passes by the pulverizer very little reduction in maximum particle size was realized. The asphalt content of the combined materials was 3%.

The combined material for the MC-800 and SC-800 sections was spread across the roadway and allowed to dry. The additional drying time was necessary to lower the moisture content below 2% before applying asphalt. To tack the base, the aggregate was windrowed at one side of the road. The opposite side was broomed clean and tacked with MC-70. The material was then bladed onto the tacked surface allowing the other side to be cleaned and tacked.

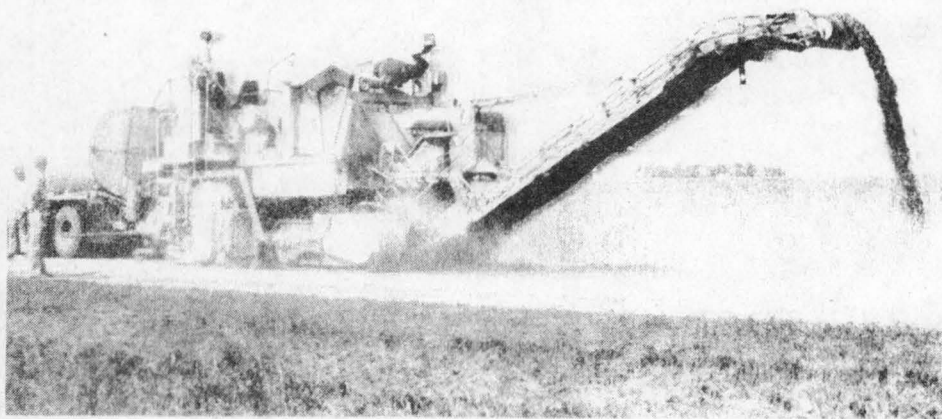


Figure 2. Milling on county road A-46

Road Mixing

In the special provisions, the preferred equipment for mixing and relaying the milled material was a traveling pug and a laydown machine. A traveling pug was not available so an asphalt distributor and a Seaman or Bros Pulverizer were accepted for asphalt application and mixing. The contractor opted to use a motor patrol to spread the mix rather than an asphalt paver.

Mixing of the milled material and the SC-800 began September 18. The air temperature ranged from 68° to 74°F. After cleaning and tacking the base, the milled material was spread across the roadway the width of the distributor bar (Figure 3). The SC-800 asphalt was heated to 170°F prior to application. Unfortunately, the distributor wasn't capable of delivering, in one pass, the specified 2.8 percent asphalt. Following the initial pass of the distributor, a patrol bladed the mix into a windrow for the pulverizer mixing. The first pass of the pulverizer left the asphalt "balled-up" with the fine portion of the aggregate. The material was again spread across the road and the remaining SC-800 was applied in two additional passes. Blading the mix back and forth and subsequent passes with the pulverizer did break up most of the asphalt balls (Figure 4). As is generally the case, 100 percent coating of the material was not achieved in the cold mix process.

After 96 hours of aeration (Figure 5), the mix was spread across the road to the 1/2" per foot cross slope. Initial compaction was by two rubber tired rollers, followed by a large steel vibrating roller (Figure 6). Four days later the surface was rerolled with the rubber tired rollers.

The second section mixed was the MC-800 section. In an attempt to avoid the balling problem experienced on the SC-800 section, the material

was split into three windrows and asphalt was added. The MC-800 asphalt was heated to 225⁰F prior to application. The distributor was then able to apply the 2.9 percent asphalt specified in one pass per windrow. The smaller windrows could also be handled much easier by the patrol and the pulverizer. Despite the change, some balling of the asphalt still occurred. The completed mix was spread and compacted the same as the previous section. Air temperature remained moderate, around 70⁰F, during mixing and placing of the MC-800.

The HFMS-2 and CSS-1 emulsions were mixed in a similar manner. Percentages of emulsion required in the mixes were 4.7 for the HFMS-2 and 4.9 for the CSS-1. This required six passes of the distributor on each section. The emulsions caused only minor balling in the mix. Air temperatures during mixing and placing were between 52⁰F and 65⁰F. The emulsions were heated to 140⁰F for application, but quickly cooled because of the air temperature and the strong wind. After several days the compacted surface exhibited a dark brown color and produced dust as traffic passed.



Figure 3. First application of SC-800 to road mix

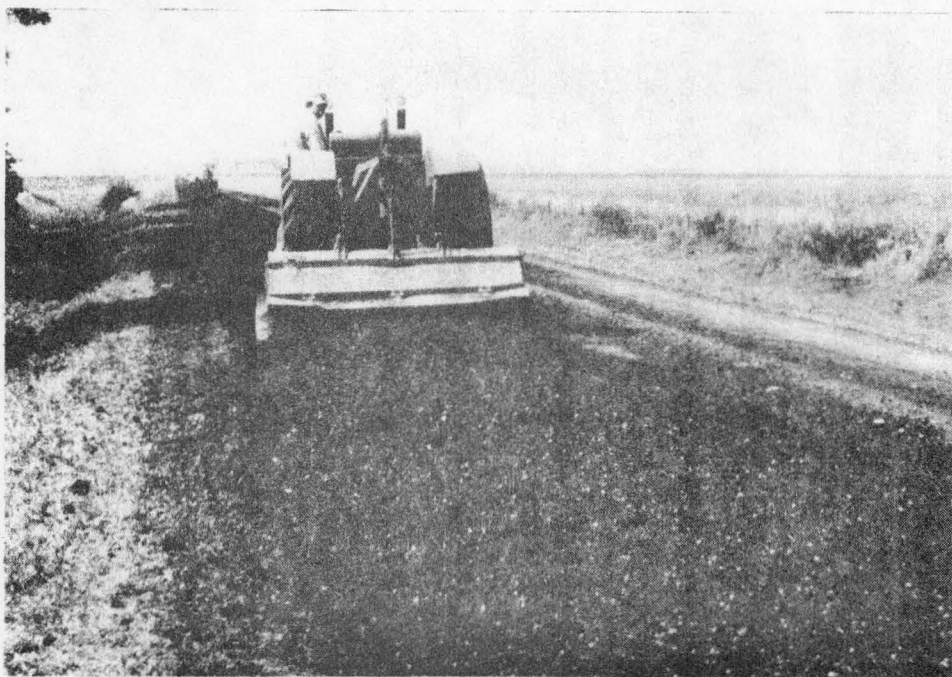


Figure 4. Mixing windrow with a pulverizer

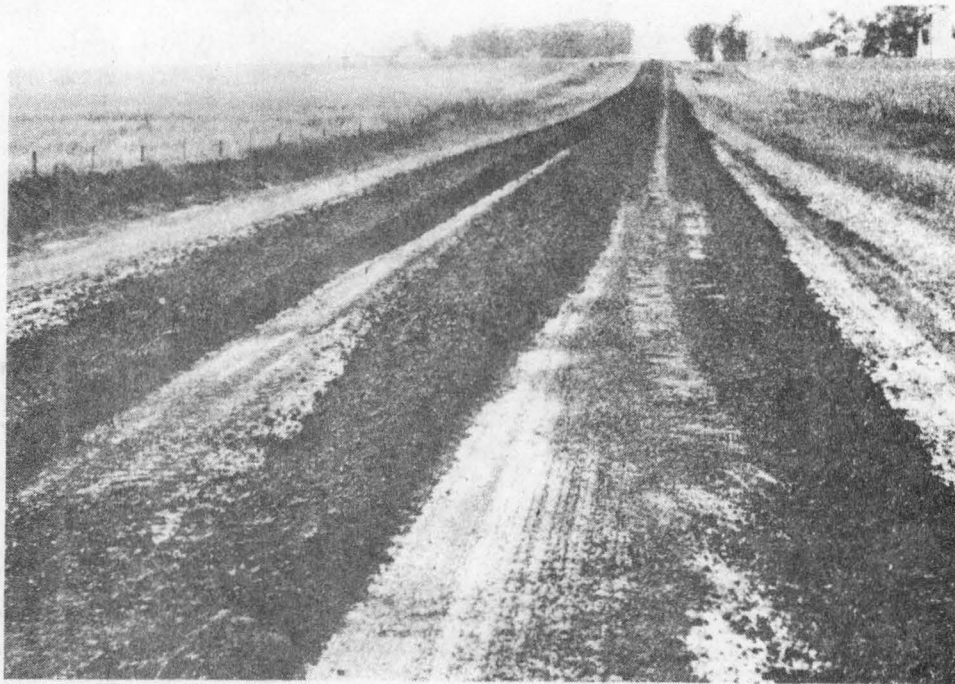


Figure 5. SC-800 road mix left to aerate after mixing.



Figure 6. Compaction of road mix section

Plant Mixing and Paver Laying

The mixes composed of 3/4" and 1/2" gravel were mixed in a continuous drum mix plant set up one-mile south of Ashton. Asphalt temperatures and mix temperatures for the various mixes are shown below:

<u>Binder</u>	<u>Asphalt Temp. °F</u>	<u>Mix Temp. °F</u>
AC-5	250° to 305°	280° to 350°
SC-800	210°	195° to 200°
MC-3000	230° to 250°	190° to 235°
HFMS-2	150°	180° to 210°
*CSS-1	150° to 175°	140° to 210°

*Mix temperature was raised above 190°F because poor coating and poor laying qualities of the mix resulted at lower temperatures.

The plant mix sections were laid with a Blaw Knox full width paver. To simplify storage of the asphalt binders, the paver was first used on A-34 to lay 1/2" mix with a binder and then moved to A-46 to place the 3/4" mix using the same asphalt binder. The initial problems occurred on the SC-800 section of A-34. A 1/2" mix could not be placed 3/4" thick as the plans had specified. The contractor increased the mat thickness to between 1 1/8" and 1 1/2" so that it could be laid without tearing. The problem was the same for each mix on A-34.

Another problem arose while mixing the CSS-1 material. At a mix temperature of 140° to 150°F, poor coating of the aggregate was observed. It was difficult to lay the mix at that temperature due to dragging and tearing of the mat even at the increased thickness. At a 190°F mix temperature the problems were reduced. No significant problems arose

during the resurfacing of A-46.

Initial compaction was with a vibratory steel roller, followed by a rubber-tired roller and final rolling with a static steel roller. Generally, the rollers were held back from the paver to allow the mats to cool to 120° to 140°F and gain stability.

CONSTRUCTION TESTING

The construction of fourteen different test sections necessitated substantial additional testing. Samples of each mix were taken from the roadways prior to rolling. Density samples for each section were obtained from the compacted mats.

Plant Mix Testing

From the mix samples obtained, the asphalt binders were extracted and tested for penetration and viscosity (see Appendix E). As was expected, the SC-800 was too fluid to test for penetration. The other extreme was the CSS-1 emulsion extracted from the 3/4" and 1/2" mixes. Penetrations of 78 and 83 indicated a relatively hard asphalt binder, similar to an AC-10 extraction. Penetrations ranging from 108 to 148 for the other three extracted asphalts were generally consistent with project expectations for the plant mixes.

The lab densities, field densities and field voids were determined for each section and are given in Appendix F. No minimum density requirements were specified for the bituminous concrete test sections. Four inch diameter cores were cut from the AC-5 Type B control section and weighed to obtain field densities and verify that it was at least 94% of Marshall density as required. The bituminous concrete sections were too soft to cut cores from so a nuclear density gauge was used to obtain field densities.

Road Mix Testing

Bituminous binders extracted from the road mixed sections constructed with 67% reclaimed bituminous pavement had relatively low penetrations except for the SC-800 (Appendix E). This was expected due to the presence of 3% old asphalt cement with a penetration of 40 in the mix. The very soft SC-800 had a dramatic effect on the old asphalt binder and produced a 140 penetration for the extracted asphalt combination.

The field densities for the road mix sections were obtained by use of the nuclear density gauge. Lab densities, however, were based on modified proctor density rather than Marshall density. Lab densities, field densities and field voids are given in Appendix F.

POST CONSTRUCTION PERFORMANCE

The late completion date of the paving forced the county to postpone the application of the seal coat surfacing planned for the project. A winter seal was applied only to the surface of the road mix sections before winter.

Performance of Plant Mixed Sections

It was apparent, shortly after construction, that the plant mixed CSS-1 emulsion sections were not performing well. Besides having disappointingly low penetrations, the sections experienced aggregate loss from the surface. The emulsion may not have been compatible with the gravel aggregate. Eventually the 1/2" mix of CSS-1 on A-34 had to be bladed off with a motor patrol. The CSS-1 sections on A-46 experienced the same problem, but to a much lesser extent. The other plant mixed sections are performing satisfactorily with little noticeable difference in appearance.

In early summer of 1982, County Road A-46 was used as a haul road for aggregate trucks transporting material to a four-mile pcc paving project. The heavy trucks caused some areas of the CSS-1 emulsion section to lose aggregate from the surface. The surface of the 1/2 mile CSS-1 section was corrected by resurfacing with an asphalt sand mix in July, 1982.

In July, 1982 1 1/4" of type B mix of AC-5 and 1/2" gravel was placed on A-34 where the CSS-1 section had earlier been removed. The resurfacing of A-46 and A-34 was completed with a seal coat surface over the test sections. One-half mile of the AC-5 section and 1200 foot of the SC-800 plant mix section on A-46 were left with no seal coat to observe the effects of traffic and weather. Specific locations of corrective maintenance are shown in Appendix G.

Performance of Road Mixed Sections

The two emulsion road mix sections performed better than expected through the winter with only a sand seal. The sections appeared to be very lean on asphalt, but samples from the roadway contained nearly 7% asphalt. It was evident that the emulsions did little to activate the old asphalt.

Both the SC-800 and MC-800 sections are performing satisfactorily. The heavy truck traffic caused no significant distress in either section. The construction of the two road mix sections was completed by applying a seal coat in July, 1982. A 1000 foot segment of both the SC-800 and MC-800 sections was double seal coated as an attempt at correcting surface distortions. These segments look very good and indicate that a double seal might be justifiable for the surface treatment.

The two emulsion road mix sections required surface patching. A 1300 foot ac patch was placed on the HFMS-2 section and the entire one-half mile CSS-1 section was resurfaced with asphaltic concrete. The one mile of emulsion road mix was then seal coated as originally planned. Specific areas of maintenance are shown in Appendix G.

CONSTRUCTION COSTS.

The construction costs for all plant mix sections were similar to the construction costs for the Type B acc overlay. Using bid prices for the different asphalt binders, and actual quantities used, the cost of binder per ton of mix ranged from \$13.53 for the HFMS-2 emulsion to \$16.15 for the MC-3000. Binder cost for AC-5 asphalt per ton of mix was \$15.31. The cost per ton of mix was \$13.74 for CSS-1 emulsion and \$14.42 for SC-800. Bid prices for mixing, placing and compacting the bases were the same for each of the respective plant mixed sections. Due to the bid procedure for the road mixed sections, no bid price cost could be developed.

DISCUSSION AND SUMMARY

The purpose of the project was to construct flexible bituminous concrete base overlays which have the potential to reduce future maintenance and construction costs. The recycled portions of the project were added as a possible alternative to overlay construction for a deteriorated road.

Plant Mixed Sections

The construction of the plant mixed sections was generally successful using standard asphalt construction equipment and procedures. One disappointment was the stripping of aggregate on the CSS-1 sections.

During trial mixing no special consideration was given to the compatibility of the aggregate and the binder. Certainly, in the future, emulsion mixes should be thoroughly tested to minimize the possibility of premature failure.

Another problem which was not completely expected, was the necessity to increase the thickness of the 1 1/2" mix to avoid tearing the mat. Common practice for paver laid hot mix is to use a maximum aggregate size which is no larger than 75 percent of the mat thickness and in many cases much less than 75 percent. The relatively low mix temperatures may have also contributed to the problem.

Future performance of the plant mixed sections will be influenced to some degree by the residual asphalt content, the asphalt penetration and the percent voids in the compacted mats. The residual asphalt contents were varied for the test sections. The emulsions, which are about 67 percent asphalt, resulted in a residual asphalt content in the mats of 4.2 percent to 4.5 percent. For the SC-800 and MC-3000 sections, asphalt added to the mixes was intentionally varied from 5.7 to 4.6 percent asphalt. Overall, the slow cure and medium cure asphalts, which contain 5 to 10 percent oil distillate, left a residual asphalt content about 0.5 to 1.0 percent higher than the emulsions. The AC-5 sections have an asphalt content of about 6.5 percent.

The asphalt penetration and viscosity is another factor which varied for the test sections. High penetration asphalts are desirable for their resistance to oxidation and low temperature cracking. The result of using high penetration asphalts is a reduced resistance to rutting and shoving during periods of high temperatures. On this project, no surface distortion has been observed on any test section.

The third characteristic of the test sections which varied was the percent voids in the compacted mats. The amount of voids is directly related to asphalt content of the mixes used. High voids were partially the result of low asphalt contents in the emulsion sections. High densities for the test sections were sacrificed for economy and stability of the pavement. To prevent premature deterioration of the pavements from surface moisture infiltration, the surfaces were seal coated.

Road Mixed Sections

The construction of the road mixed sections was somewhat disappointing. Equipment used on the job was not the optimum. The initial problem was how to eliminate oversize pieces of milled pavement. Passes by the pulverizers had only marginal success at reducing the amount of 1" plus large chunks. As a result of several passes by the pulverizer additional fine material was produced.

The other problem encountered was inadequate mixing. Addition of asphalt binder through an asphalt distributor caused the binder to flow on top of the aggregate and cool before the pulverizer could mix the materials.

The mixing equipment used would be suitable for normal road mix operations. However, for this project, which involved recycled pavement and the addition of a low percentage of the binder, the equipment was less than adequate. An improved procedure would have been to first screen off the oversized pieces of pavement after milling. A more effective means of mixing the materials, would be to use a traveling pug mill or a pulverizer equipped to apply the required percentage of binder directly into the mixing chamber.

Despite the difficulties during construction, the MC-800 and SC-800 produced a surprisingly good surface. The two emulsion sections, however, appeared very lean on asphalt. Both emulsion sections remained a dark brown color after construction and produced dust as traffic passed. The 1982 asphalt maintenance work on the emulsion road mixed sections leaves only 1300 feet of the HFMS-2 and none of the CSS-1 section for further comparison.

Future performance of the road mixed sections will be influenced by the asphalt content, asphalt penetration and void content. Another influencing factor on performance is the degree of rejuvenation of the old bitumen in the mixes. In the cases of the SC-800 and MC-800, it appeared that the combination of the heat and the oil distillate from the asphalts did activate the old bitumen to some extent. The emulsions however, appeared to have had little rejuvenating effect on the old bitumen.

Appendix A
Contract Quantities and Special Provisions

Contract Quantities

County Road A-34

ITEM	QUANTITY	UNIT	UNIT PRICE	AMOUNT
1 Base, Cleaning & Preparation of	6.817 Miles		100.00	681.70
2 Primer of Tack-Coat Bitumen	5.872 Gals.		.95	5,578.40
3 Base, Type B Class 2 Asphalt Cement Concrete	577 Tons		9.17	5,291.09
4 Base, Bituminous Concrete Class 2	3,381 Tons		9.17	31,003.77
5 Asphalt-Sand Surface Course	160 Tons		30.00	4,800.00
6 Base, Binder Bitumen HFMS-2	27,823 Gals.		.90	25,040.70
7 Base, Binder Bitumen CSS-1	9,966 Gals.		.90	8,969.40
8 Base, Binder Bitumen MC-3000	7,619 Gals.		1.25	9,523.75
9 Base, Binder Bitumen SC-800	6,940 Gals.		1.15	7,981.00
10 Asphalt Cement	50 Tons		232.00	11,600.00
Grand Total				\$110,469.81

Contract Quantities Co. Rd. A-46

ITEM	QUANTITY	UNIT	UNIT PRICE	AMOUNT
1. Base, Cleaning & Preparation of	6.988 Miles		100.00	698.80
2. Primer Or Tack-Coat Bitumen	7,313 Gals		1.00	7,313.00
3. Base, Type B Class 2 Asphalt Cement Concrete	1,437 Tons		9.07	13,033.59
4. Base, Bituminous Concrete Class 2	8,483 Tons		9.07	76,940.81
5. Asphalt-Sand Surface Course	70 Tons		30.00	2,100.00
6. Asphalt Cement	99 Tons		232.00	22,968.00
7. Base, Binder Bitumen HFMS-2	70,918 Gals		.90	63,826.20
8. Base, Binder Bitumen CSS-1	24,439 Gals		.90	21,995.10
9. Base, Binder Bitumen MC-3000	24,354 Gals		1.25	30,442.50
10. Base, Binder Bitumen SC-800	17,190 Gals		1.15	19,768.50
Grand Total				\$259,086.50

Alternate Construction Quantities

1. Base, Cleaning & Preparation of	4.981 Miles
2. Primer or Tack-Coat Bitumen	7,313 Gals
3. Base, Type B Class 2 Asphalt Cement Conc.	1,437 Tons
4. Base, Bituminous Concrete Class 2	5,713 Tons
5. Asphalt-Sand Surface Course	50 Tons
6. Asphalt Cement	99 Tons
7. Base, Binder Bitumen HFMS-2	67,057 Gals
8. Base, Binder Bitumen CSS-1	20,588 Gals
9. Base, Binder Bitumen MC-3000	21,367 Gals
10. Base, Binder Bitumen SC-800	14,491 Gals
11. Aggregate, For Bituminous Mix	969 Tons
12. Planing & Milling Existing Base	25,911 Sq. Yds.
13. Mixing & Relaying Bituminous Concrete Base	25,911 Sq. Yds.

IOWA DEPARTMENT OF TRANSPORTATION
Ames, Iowa



Special Provisions
for

ACC PROJECTS

Osceola County Projects:

FM-72(7) --55-72

SN-69(1) --51-72

May 27, 1981.

THE STANDARD SPECIFICATIONS, SERIES OF 1977, ARE AMENDED BY THE FOLLOWING ADDITIONS AND MODIFICATIONS. THESE ARE SPECIAL PROVISIONS AND SHALL PREVAIL OVER THOSE PUBLISHED IN THE STANDARD SPECIFICATIONS.

358.01 GENERAL. The work shall consist of the construction of two Type B asphalt cement concrete base sections and various compacted bituminous concrete base courses as specified on the plans. Section 2203 of the Standard Specifications will apply to Division 1 (Type B ACC base) and Section 2204 of the Standard Specifications will apply to Divisions 2, 3, 4, and 5 (various compacted bituminous concrete base courses) except where modified by these special provisions or other DOT current special provisions. Section 1109.03 of the Standard Specifications shall not apply to asphalt-sand mix, SC-800, or primer or tack coat. All or any part of the work may be eliminated at the discretion of the engineer.

It is intended that some wheel-track distortion be corrected by placing a heavy tack coat, blading a hot asphalt-sand mix into the areas, and rolling it up to six times with a rubber-tired roller. The areas to be corrected, mix designs, and construction procedures will be determined during construction.

It is proposed that two miles of Project RS-69(1) will be milled, mixed, and laid cold, if found feasible. This work may be done before other work is started and therefore need not delay other work. If the alternate is not found feasible, as determined by the engineer, these areas will be constructed according to the original plan; however milled depths other than the proposed 1 1/2 inches will be considered if the contractor and engineer can reach agreement on construction methods and payment.

358.02 MATERIALS.

A. Primer or Tack-Coat Bitumen - MC-70 meeting requirements of Section 4138 shall be used.

B. Division 1 - AC-5 meeting requirements of AASHTO M 226-78, Table 2, shall be used.

C. Division 2 - Anionic high-float emulsified asphalt meeting requirements of ASTM D 977 shall be used. Residue from the distillation test of this material shall be a minimum 140 penetration at 77°F. (25°C.) with 100g. for 5 seconds. The anionic high-float emulsified asphalt shall contain a minimum of 5% oil distillate. HFMS-2 is intended, but the grade will depend on the design and job-mix formula determinations.

D. Division 3 - Cationic emulsified asphalt meeting requirements of AASHTO M 208-72 shall be used. Residue from the distillation test of this material shall be a minimum 140 penetration at 77°F. (25°C.) with 100g. for 5 seconds. The cationic emulsified asphalt shall contain a minimum of 5% oil distillate. CSS-1 is intended, but the grade will depend on the design and job-mix formula determinations.

E. Division 4 - Medium curing cut-back asphalt meeting requirements of AASHTO M 82-75 shall be used. Residue from the distillation test of this material shall be a minimum 140 penetration at 77°F. (25°C.) with 100g. for 5 seconds. MC-3000 furnished in the upper half of the viscosity range is intended, but the grade will depend on the design and job-mix formula determinations.

F. Division 5 - Slow curing liquid asphalt meeting requirements of ASTM D 2026 shall be used. SC-800 is intended, but the grade will depend on the design and job-mix formula determinations.

G. Aggregate - The aggregate incorporated in the Type B, Class 2 asphalt cement concrete (asphaltic concrete) base and the various types of bituminous concrete bases, including virgin aggregate to be in mixtures for the milled areas, shall meet requirements of Section 4126 and Gradation No. 19, Section 4109, except Paragraph 4126.04C shall be deleted. All pit-run material passing an 8-inch screen shall be crushed and incorporated in the aggregate.

The aggregate incorporated in the asphaltic-sand mix shall meet requirements of Specification 4129 and Gradation No. 22, Section 4109.

H. Final Mixture - Refer to general notes on plans.

358.03 EQUIPMENT.

A. Divisions 2, 3, 4, and 5 - Article 2001.19 of the Standard Specifications shall apply where the material is paver laid.

358.04 CONSTRUCTION

A. Divisions 2, 3, 4, and 5 - It is intended the various bituminous concrete base courses shall be paver laid with the option to spread with motor patrols, if so approved by the engineer. Articles 2203.09, 2203.10, 2203.11, 2203.13, and 2203.15 of the Standard Specifications shall apply where the material is paver laid, except the second paragraph of 2203.10 shall not apply. Article 2204.07 will not apply.

B. Additional Construction Work on Project RS-69(1). The following additional construction work is intended on this project.

Milling - This work shall include all labor and equipment for milling or planing 25,911 square yards, 1½ inch in depth, of the existing bituminous concrete base on Project RS-69(1). Intended areas to be milled are from station 26+50, Division 2, to station 79+50, Division 3, and from station 133+00, Division 4, to station 186+00, Division 5. Over 95% of this milled material must pass a 1-inch sieve; large pieces not incorporated in the mix will be loaded on county trucks.

Mixing and Relaying - This work shall include all labor and equipment for mixing and relaying the milled bituminous concrete base. This work shall include adding a virgin aggregate to the milled material so that a 2½-inch lift will be re-laid by tacking the milled surface, adding asphalt to the combined mix, and re-laying and compacting the mix on the same areas. It is preferred that a traveling pug be used for mixing and that a laydown machine be used for laying; however other methods producing acceptable results may be used, if acceptable to the engineer.

This additional work and the revised quantities within this area are identified on the plans as alternate construction. Payment for all work in this area, if constructed as intended, will be made on the basis of the contract quantities for items identified on the plans as quoted construction, with no measurement for payment, as noted on the plans. This payment will be full compensation for furnishing all equipment, labor, and materials necessary to do this additional construction work within the area designated.

Appendix B
Aggregate Test Reports

IOWA DEPARTMENT OF TRANSPORTATION
OFFICE OF MATERIALS
TEST REPORT - BITUMINOUS MATERIALS
LAB LOCATION AMES

MATERIAL PEA ROCK

LAB NO. AAT1-532

INTENDED USE 10-15% ADDED TO #4126 AGGREGATE

COUNTY OSCEOLA

SN-29(3)
PROJ NO. FM-72(7)

DESIGN

CONTRACT NO. 18620, 18619
18618

PRODUCER FLOYD RIVER SAND & GRAVEL

CONTRACTOR ROHLIN CONST.

SOURCE

UNIT OF MATERIAL 3 SACKS FROM STOCKPILE

2,500 TON

SAMPLED BY BOB FREY

SENDER'S NO. BF-5

DATE SAMPLED 8-14-81

REC'D 8-17-81

REPORTED 9-25-81

SIEVE ANALYSIS - PER CENT PASSING

1 1/2"	
1"	
3/4"	
1/2"	
3/8"	100
NO. 4	22
NO. 8	1.5
NO. 16	1.0
NO. 30	0.7
NO. 50	0.8
NO. 100	0.7
NO. 200	0.7

% PASG. NO. 8 AFTER 16 CYCLES F & T, WATER-ALCO. SOL.
% PASG. NO. 8 AFTER 25 CYCLES F & T, WATER SOLUTION
% OF WEAR, LOS ANGELES ABRASION, GRADING

LIQUID LIMIT
PLASTIC LIMIT
PLASTICITY INDEX

COPIES

BIT. AGG.
J. BUMP
PAUL SCHWARTING
L. ZEARLEY
PROJECTS LISTED ABOVE

DISPOSITION

SIGNED: BERNARD C. BROWN
TESTING ENGINEER

IOHA DEPARTMENT OF TRANSPORTATION
OFFICE OF MATERIALS
TEST REPORT - BITUMINOUS MATERIALS
LAB LOCATION AMES

MATERIAL 3/4" CRUSHED AGGREGATE

LAB NO. AAT1-591

INTENDED USE TYPE B CLASS 2 & BIT. CONC. BASE

COUNTY OSCEOLA

SN-69(3)
PROJ NO. SN-29(3)

DESIGN

CONTRACT NO.

PRODUCER MAUDLIN CONST.

CONTRACTOR ROHLIN CONST.

SOURCE NE-1/4 28-98-42 OSCEOLA CO.

UNIT OF MATERIAL 2 SACKS 48,000 TL

SAMPLED BY BOB FREY

SENDER'S NO. 7/31-1 A&B

DATE SAMPLED 7-31-81

REC'D 9-1-81

REPORTED 9-25-81

SIEVE ANALYSIS - PER CENT PASSING

1 1/2"	
1"	
3/4"	100
1/2"	95
3/8"	87
NO. 4	71
NO. 8	58
NO. 16	45
NO. 30	29
NO. 50	14
NO. 100	8.2
NO. 200	6.5

% P.S.G. NO. 8 AFTER 16 CYCLES F & T, WATER-ALCO. SOL.
% P.S.G. NO. 8 AFTER 25 CYCLES F & T, WATER SOLUTION
% OF WEAR, LOS ANGELES ABRASION, GRADING

LIQUID LIMIT
PLASTIC LIMIT
PLASTICITY INDEX

COPIES:

BIT. AGG.
J. BUMP
P. SCHWARTING
L. ZEARLEY
PROJECTS LISTED ABOVE

DISPOSITION:

SIGNED: BERNARD C. BROWN
TESTING ENGINEER

IOWA DEPARTMENT OF TRANSPORTATION
OFFICE OF MATERIALS
TEST REPORT - BITUMINOUS MATERIALS
LAB LOCATION AMES

MATERIAL 1/2" CRUSHED AGGREGATE

LAB NO. AAT1-592

INTENDED USE BIT. CONC. BASE OVERLAY

COUNTY OSCEOLA

PROJ NO. FM-72(7)

DESIGN

CONTRACT NO.

PRODUCER MAUDLIN CONST.

CONTRACTOR ROHLIN CONST.

SOURCE NE-1/4 28-98-42, OSCEOLA CO.

UNIT OF MATERIAL 4 SACKS 4,000 T.

SAMPLED BY BOB FREY

SENDER'S NO. 7/31-2

DATE SAMPLED 7-31-81

REC'D 9-1-81

REPORTED 9-25-81

SIEVE ANALYSIS - PER CENT PASSING

1 1/2"	
1"	
3/4"	100
1/2"	98
3/8"	90
1/4"	69
NO. 8	50
NO. 16	42
NO. 30	26
NO. 50	14
NO. 100	8.7
NO. 200	7.7

% LOSS, NO. 8 AFTER 16 CYCLES F & T, WATER-ALCO. SOL.

% F&T, NO. 8 AFTER 25 CYCLES F & T, WATER SOLUTION

% OF WEAR, LOS ANGELES ABRASION, GRADING

LIQUID LIMIT

PLASTIC LIMIT

PLASTICITY INDEX

COPIES

101, AGL

J. EHRH

P. SCHWARTZ

L. ZEABLY

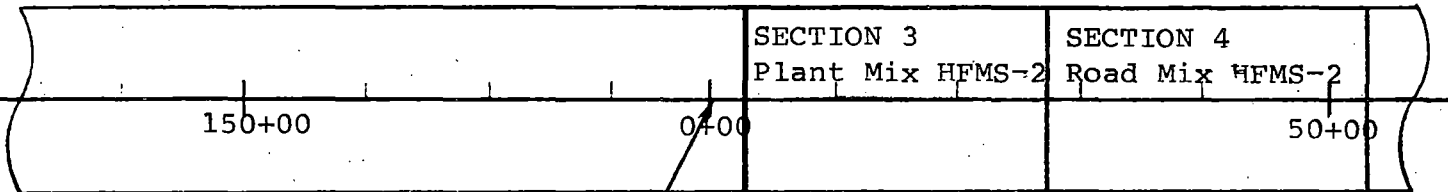
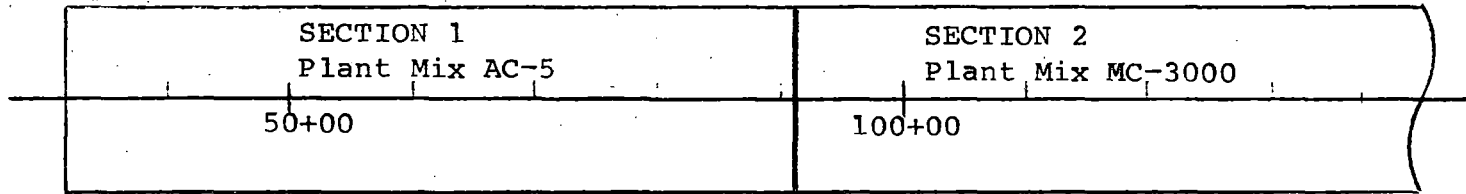
FM 72(7), OSCEOLA

DISPOSITION

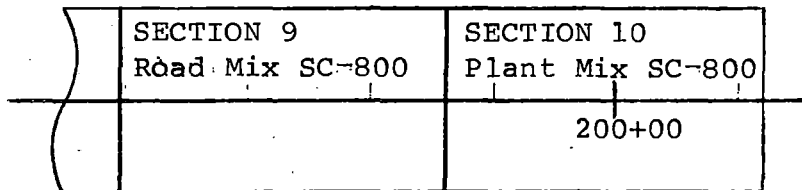
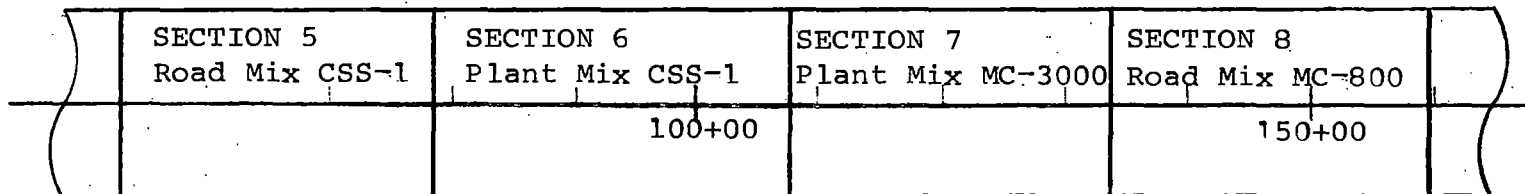
Appendix C
Test Section Layout

Test Section Layout

A-46

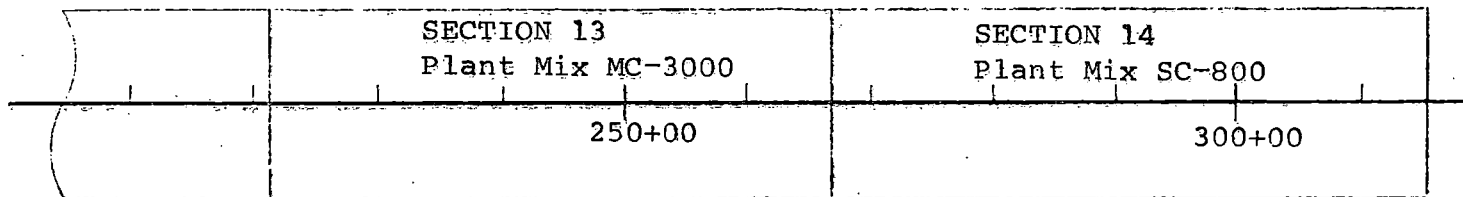
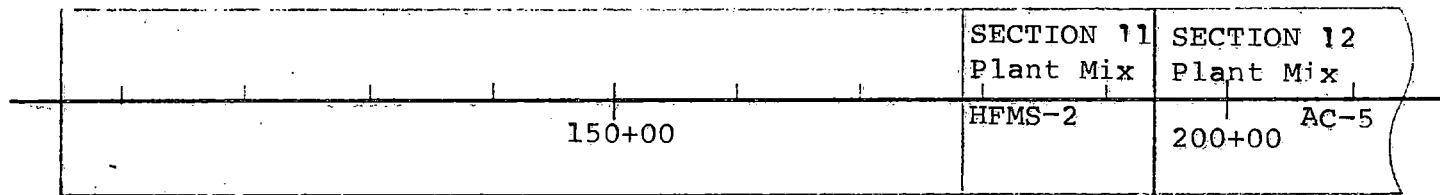


187+70 bk. =
0+00 ahd.



Test Section Layout

A-34



Appendix D
Mix Design Reports

IOWA DEPARTMENT OF TRANSPORTATION
OFFICE OF MATERIALS
ASPHALT CONCRETE MIX DESIGN
LAB LOCATION AMES

MIX, TYPE AND CLASS: TYPE B CLASS I

LAB NO. ABD1-140

INTENDED USE: AC-5

SIZE 3/4"

SPEC. NO.

DATE REPORTED 9/15/81

COUNTY OSCEOLA

PROJECT SN-29(3)--51-72

SN-69(3)--51-72

FM-72(7)--55-72

CONTRACTOR ROHLIN

PROJ. LOCATION

AGG. SOURCES 3/4" GRAVEL - ASHTON PIT - OSCEOLA CO.;

PEA GRAVEL - FLOYD RIVER SAND & GRAVEL

JOB MIX FORMULA AGGREGATE PROPORTIONS: 85% AAT1-482, 15% AAT1-532

JOB MIX FORMULA - COMBINED GRADATION

1-1/2"	1"	3/4"	1/2"	3/8"	NO.4	NO.8	NO.16	NO.30	NO.50	NO.100	NO.200
100	96	89	64	50	38	25	12	7.1	5.6		

TOLERANCE: 0.8/100

7

7

6

5

3

75 BL. MARSHALL DENSITY

2.32

ASPHALT SOURCE AND APPROXIMATE VISCOSITY

KOCH - 537 POISES

PLASTICITY INDEX

N. P.

% ASPH. IN MIX

5.0

6.0

7.0

NUMBER OF MARSHALL BLOWS

50

50

50

MARSHALL STABILITY - LBS

1933

1817

2047

FLOW - 0.01 IN.

7

7

8

SP. GR. BY DISPLACEMENT (LAB DENS.)

2.25

2.29

2.32

GULK SP. GR. CORR. DRY AGG.

2.634

2.634

2.634

SP. GR. ASPH. @ 77 F.

1.022

1.022

1.022

CALC. SOLID SP. GR.

2.48

2.44

2.41

% VOIDS - CALC.

9.3

6.3

3.6

RICE SP. GR.

2.47

2.43

2.39

% VOIDS - RICE

8.8

5.8

3.0

% WATER ABSORPTION - AGGREGATE

1.38

1.38

1.38

% VOIDS IN THE MINERAL AGGREGATE

18.8

18.3

18.1

% V.M. FILLER FILLED WITH ASPHALT

50.7

65.6

79.8

CALCULATED ASPH. FILM THICKNESS (MICRONS)

7.7

9.6

11.5

FILLER BITUMEN RATIO

0.9

A CONTENT OF 6.50% ASPHALT IS RECOMMENDED TO START THE JOB.

COPIES:

ASPH. MIX DESIGN

PROJECT LISTED ABOVE

J. RICE

P. SCHWARTZ

D. JORDISON

R. NIELQUIST

L. ZEARLEY

ROHLIN

C. JONES

IOWA DEPARTMENT OF TRANSPORTATION
OFFICE OF MATERIALS
ASPHALT CONCRETE MIX DESIGN
LAB LOCATION AMES

MIX. TYPE AND CLASS: TYPE B CLASS 2

LAB NO. ABD1-131

INTENDED USE: AC 5

SIZE 1/2"

SPEC. NO.

DATE REPORTED 9/15/81

COUNTY OSCEOLA

PROJECT SN-29(3)--51-72
SN-69(3)--51-72

FM-72(7)--55-72

CONTRACTOR ROHLIN

PROJ. LOCATION

AGG. SOURCE: 1/2" GRAVEL - ASHTON PIT - OSCEOLA CO.

JOB MIX FORMULA AGGREGATE PROPORTIONS: 100% AAT1-509

JOB MIX FORMULA - COMBINED GRADATION											
1-1/2"	1"	3/4"	1/2"	3/8"	NO.4	NO.8	NO.16	NO.30	NO.50	NO.100	NO.200
		100	98	90	69	56	42	26	14	8.7	7.6

TOLERANCE: 28/100 7 6 5 3

75 BLOW MARSHALL DENSITY

ASPH. SOURCE AND APPROXIMATE VISCOSITY

PLASTICITY INDEX

ASPH. IN MIX

NUMBER OF MARSHALL BLOWS

MARSHALL STABILITY - LBS.

FLOW 0.01 IN.

SP. GR. BY DISPLACEMENT (LAB DENS.)

BULK SP. GR. COMB. DRY AGG.

SP. GR. ASPH @ 77 F.

CALC. VOLUME OF ASPH.

% VOIDS - CALC.

% Voids - FILL

% Voids - FILL

% WATER ABSORPTION - AGGREGATE

% Voids IN THE MINERAL AGGREGATE

% Voids FILLED WITH ASPHALT

CALCULATED ASPH. FILM THICKNESS (MICRONS)

FILLER, BITUMEN RATIO

KOCH - 572 POISES

2

5.0

6.0

7.0

50

50

50

2072

2043

1907

8

8

8

2.26

2.28

2.29

2.641

2.641

2.641

1.022

1.022

1.022

2.48

2.45

2.41

9.0

6.9

5.1

2.48

2.42

2.36

8.9

5.7

3.1

1.32

1.32

1.32

18.7

18.8

19.4

51.6

63.6

73.8

6.6

8.2

9.8

1.1

A CONTENT OF 6.7% ASPHALT IS RECOMMENDED TO START THE JOB.

COPIES:

ASPH. MIX DESIGN

PROJECTS LISTED ABOVE

J. GUNP

P. SCHMIDT

D. BROTON

R. WELCH

L. EARLEY

ROHLIN

C. JONES

Rohlin
C. JonesIOWA DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION
(MATERIALS DEPARTMENT)
ASPHALT CONCRETE MIX DESIGN
AMES LABORATORYAsph. Mix Design
Projects Listed Below
J. Bump
P. Schwarting
D. Jordison
R. Shelquist
L. Zearley
Lab. No. ABD1-157Mix, Type and Class: Type B Class 2 Size 3/4"Intended Use: SC-800 Cold Mix Spec. No. SN-29(3)--51-72 Date Reported 9/28/81County: Osceola Proj. No. SN-69(3)--51-72 Contractor Rohlin
FM-72(7)--55-72

Proj. Location: _____

Agg. Sources: 3/4" Gravel - 28-98-42 Osceola Co.Job Mix Formula Aggregate Proportions: 100% AAT1-591

JOB MIX FORMULA - COMBINED GRADATION

1½"	1"	¾"	½"	3/8"	#4	#8	#16	#30	#50	#100	#200
		100	95	87	71	58	45	29	14	8.2	6.5
Tolerance											

Asphalt Source and Approximate Viscosity	Algona	
% Asph. In Mix	5.0	6.0
Number of Marshall blows	50	50
Marshall Stability - Lbs.	2242	2300
Flow - 0.01 In.	8	9
Sp. Gr. By Displacement (Lab. Dens.)	2.26	2.27
Bulk Sp. Gr. Comb. Dry Agg.	2.634	2.634
Sp. Gr. Asph. @ 77 F.	0.9744	0.9744
Calc. Solid Sp. Gr.	2.43	2.39
% Voids - Calc.	6.9	5.0
Rice Sp. Gr.	Mixing Temp. 180° F. Cure - 16 hrs. @ 140° F. Molding Temp. 140° F. Testing Temp. 77° F.	
% Voids - Rice		
% Water Absorption - Aggregate	--	--
% Voids in the Mineral Aggregate	18.5	19.0
% V.M.A. Filled with Asphalt	62.7	73.6
Calculated Asph. Film Thickness (Microns)	7.8	9.4

A content of 5.50% SC-800 is recommended to start the job.

-37- SIGNED: _____

(TESTING ENGINEER)

Rohlin Constr.
C. JonesIOWA DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION
(MATERIALS DEPARTMENT)
ASPHALT CONCRETE MIX DESIGN
AMES LABORATORYAsph. Mix Design
Projects Listed Below
J. Bump
P. Schwarting
D. Jordison
R. Shelquist
L. ZearleyMix, Type and Class: Type B Class 2 Size 1/2" Lab. No. ABD1-159Intended Use: SC-800 Cold Mix Spec. No. SN-29(3)--51-72 Date Reported 9/28/81County Osceola Proj. No. SN-69(3)--51-72 Contractor Rohlin
FM-72(7)--55-72

Proj. Location: _____

Agg. Sources: 1/2" Gravel 28-98-42 Osceola Co.Job Mix Formula Aggregate Proportions: 100% AAT-592

JOB MIX FORMULA - COMBINED GRADATION

1 1/2"	1"	3/4"	3/8"	3/16"	#4	#8	#16	#30	#50	#100	#200
		100	98	90	69	56	42	26	14	8.7	7.3
Tolerance											

Asphalt Source and Approximate Viscosity	Algona - SC-800	
% Asph. In Mix	5.0	6.0
Number of Marshall blows	50	50
Marshall Stability - lbs.	1940	1960
Flow - 0.01 in.	8	10
Sp. Gr. By Displacement (Lab Dens.)	2.24	2.25
Bulk Sp. Gr. Comb. Dry Agg.	2.641	2.641
Sp. Gr. Asph. @ 77 F.	0.9744	0.9744
Calc. Solid Sp. Gr.	2.43	2.40
% Voids - Calc.	7.9	6.1
Rice Sp. Gr.	Mixing Temp. 180° F. Cure - 16 Hrs. 140° F. Molding Temp. 140° F. Testing Temp. 77° F.	
% Voids - Rice		
% Water Absorption - Aggregate	--	--
% Voids in the Mineral Aggregate	19.4	19.9
% V.M.A. Filled with Asphalt	59.2	69.6
Calculated Asph. Film Thickness (Microns)	7.6	9.2

A Content of 5.25% SC-800 is recommended to start the job.

IOWA DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION
(MATERIALS DEPARTMENT)
ASPHALT CONCRETE MIX DESIGN
AMES LABORATORYAsph. Mix Design
SN-29(3)--51-72
SN-69(3)--51-72
FM-72(7)--55-72; Osceola
J. Bump, Schwarting
D. Jordison, R. Shelquist
L. Zearley, RohlinMix, Type and Class: Type B Class 2 Size 3/4" Lab. No. ABD1-156Intended Use: MC-3000 Cold Mix Spec. No. SN-29(3)--51-72 Date Reported 9-28--81County Osceola Proj. No. SN-69(3)--51-72 Contractor Rohlin
FM-72(7)--55-72

Proj. Location: _____

Agg. Sources: 3/4" Gravel - 28-98-42 Osceola Co.Job Mix Formula Aggregate Proportions: 100% AAT1-591

JOB MIX FORMULA - COMBINED GRADATION

1 1/2"	1"	3/4"	1/2"	3/8"	#4	#8	#16	#30	#50	#100	#200
		100	95	87	71	58	45	29	14	8.2	6.5
Tolerance											

Asphalt Source and Approximate Viscosity	Algona MC-3000 93.7% Residue	
% Asph. In Mix	5.0	6.0
Number of Marshall blows	50	50
Marshall Stability - Lbs.	2955	3450
Flow - 0.01 In.	13	17
Sp. Gr. By Displacement (Lab Dens.)	2.10	2.14
Bulk Sp. Gr. Comb. Dry Agg.	2.634	2.634
Sp. Gr. Asph. @ 77 F.	1.020	1.020
Calc. Solid Sp. Gr.	2.44	2.41
% Voids - Calc.	14.0	11.0
Rice Sp. Gr.	Mixing temp. 180°F. Cure-16 hrs. @ 140°F. Molding Temp. 140°F. Testing Temp. 77°F.	
% Voids - Rice		
% Water Absorption - Aggregate	--	--
% Voids in the Mineral Aggregate	24.3	23.6
% V.M.A. Filled with Asphalt	42.4	53.3
Calculated Asph. Film Thickness (Microns)	7.8	9.4

A Content of 5.5% MC-3000 is recommended to start the job.

IOWA DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION
MATERIALS DEPARTMENTRohlin Constr. Co.
C. JonesASPHALT CONCRETE MIX DESIGN
AMES LABORATORYAsph. Mix Design
Projects listed below
J. Bump
P. Schwarting
D. Jordison
R. Shelquist
L. Zearley
Lab. No. ABD1-158

Mix, Type and Class: Type B Class 2 Size 1/2" Lab. No. ABD1-158

Intended Use: MC-3000 Cold Mix Spec. No. SN-29(3)--51-72 Date Reported 9/28/81

County Osceola Proj. No. SN-69(3)--51-72 Contractor Rohlin
FM-72(7)--55-72

Proj. Location:

Agg. Sources: 1/2" Gravel - 28-98-42 Osceola Co.

Job Mix Formula Aggregate Proportions: 100% AAT1-592

JOB MIX FORMULA - COMBINED GRADATION

1 1/2"	1"	3/4"	3/8"	3/8"	#4	#8	#16	#30	#50	#100	#200
		100	98	90	69	56	42	26	14	8.7	7.3
Tolerance											

Asphalt Source and Approximate Viscosity	Algona - MC-3000	
% Asph. In Mix	5.0	6.0
Number of Marshall blows	50	50
Marshall Stability - Lbs.	3180	3480
Flow - 0.01 In.	10	14
Sp. Gr. By Displacement (Lab Dens.)	2.10	2.11
Bulk Sp. Gr. Comb. Dry Agg.	2.641	2.641
Sp. Gr. Asph. @ 77 F.	1.020	1.020
Calc. Solid Sp. Gr.	2.45	2.41
% Voids - Calc.	14.2	12.5
Rice Sp. Gr.	Mixing Temp. 180° F. Cure - 16 Hr. @ 140° F. Molding Temp. 140° F. Testing Temp. 77° F.	
% Voids - Rice	--	--
% Water Absorption - Aggregate	--	--
% Voids in the Mineral Aggregate	24.5	24.9
% V.M.A. Filled with Asphalt	42.1	49.8
Calculated Asph. Film Thickness (Microns)	7.6	9.2

A Content of 5.25% MC-3000 is recommended to start the job.

IOWA DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION
(MATERIALS DEPARTMENT)
ASPHALT CONCRETE MIX DESIGN
AMES LABORATORYAsph. Mix Design
SN-29(3)--51-72
SN-69(3)--51-72
FM-72(7)--55-72, Osceola
J. Bump, Schwarting
D. Jordison, R. Shelquist
L. Zearley, RohlinMix, Type and Class: Type B Class 2 Size 3/4" Lab. No. ABD1-160Intended Use: HFMS-2 Cold Mix Spec. No. SN-29(3)--51-72 Date Reported 9-28-81County: Osceola Proj. No. SN-69(3)--51-72 Contractor Rohlin
FM-72(7)--55-72

Proj. Location: _____

Agg. Sources: 3/4" Gravel -- 28-98-42 Osceola Co.Job Mix Formula Aggregate Proportions: 100% AAT1-591

JOB MIX FORMULA - COMBINED GRADATION

1 1/2"	1"	3/4"	3/8"	3/8"	#4	#8	#16	#30	#50	#100	#200
		100	95	87	71	58	45	29	14	8.2	6.5
Tolerance											

Asphalt Source and Approximate Viscosity	Algona HFMS-2 (65.6% Residue)	
% Total Emulsion in Mix % Asph. in Mix	5.5	6.5
Number of Marshall blows	50	50
Marshall Stability - lbs.	2175	2470
Flow - 0.01 in.	12	11
Sp. Gr. By Displacement (Lab Dens.)	2.07	2.08
Bulk Sp. Gr. Comb. Dry Agg.	2.634	2.634
Sp. Gr. Asph. @ 77 F.	1.020	1.020
Calc. Solid Sp. Gr.	2.422	2.39
% Voids - Calc.	14.6	12.9
Rice Sp. Gr.	5.5% water added to agg. before mixing	
% Voids - Rice	Mixing temp. 130°F.	
% Water Absorption - Aggregate	Cured 16 hrs. @ 130°F.	
% Voids in the Mineral Aggregate	Molding temp. 130°F.	
% V.M.A. Filled with Asphalt	Testing temp. 77°F.	
Calculated Asph. Film Thickness (Microns)	8.6	10.3

A content of 7.0 HFMS-2 emulsion is recommended to start the job.

IOWA DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION
(MATERIAL DEPARTMENT)
ASPHALT CONCRETE MIX DESIGN
AMES LABORATORYAsph. Mix Design
SN-29(3)--51-72
SN-69(3)--51-72
FM-72(7)--55-72, Osceola
J. Bump
Schwartz, D. Jordison
R. Shelquist, L. Zearley
Rohlin

Mix, Type and Class: Type B Class 2 Size 1/2" Lab. No. ABD1-163

Intended Use: HFMS-2 Cold Mix Spec. No. SN-29(3)--51-72 Date Reported 9-28-81

County Osceola Proj. No. SN-69(3)--51-72 Contractor Rohlin
FM-72(7)--55-72

Proj. Location:

Agg. Sources: 1/2" gravel - 28-98-42 Osceola Co.

Job Mix Formula Aggregate Proportions: 100% AAT1-592

JOB MIX FORMULA - COMBINED GRADATION

1 1/2"	1"	3/4"	3/8"	3/8"	#4	#8	#16	#30	#50	#100	#200
		100	98	90	69	56	42	26	14	8.7	7.3
Tolerance											

Asphalt Source and Approximate Viscosity	Algona - HFMS-2 (65.6% residue)	
% Total Emulsion in Mix XXXXXX	5.5	6.50
Number of Marshall blows	50	50
Marshall Stability - Lbs.	2060	2362
Flow - 0.01 In.	11	11
Sp. Gr. By Displacement (Lab Dens.)	2.04	2.09
Bulk Sp. Gr. Comb. Dry Agg.	2.641	2.641
Sp. Gr. Asph. @ 77 F.	1.020	1.020
Calc. Solid Sp. Gr.	2.43	2.39
% Voids - Calc.	16.0	12.7
Rice Sp. Gr.	5.5% water added to Agg. before mixing	
% Voids - Rice	Mixing Temp. 130°F	
% Water Absorption - Aggregate	Cured 16 hrs. @ 130°F	
	Molding temp. 130°F	
	Testing Temp. 77°F	
% Voids in the Mineral Aggregate	27.0	26.0
% V.M.A. Filled with Asphalt	40.7	51.2
Calculated Asph. Film Thickness (Microns)	8.4	10.0

A content of 7.0% HFMS-2 emulsion is recommended to start the job.

IOWA DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION
(MATERIALS DEPARTMENT)
ASPHALT CONCRETE MIX DESIGN
AMES LABORATORY

Asph. Mix Design
SN-29(3) --51-72
~~SN-69(3) --51-72~~
FM-72(7) --55-72, Osceola
J. Bump, Schwarting
D. Jordison, R. Shelquist
L. Zearley, Rohlin
Lab. No. ABD1-161

Mix, Type and Class: Type B Class 2 Size 3/4" Lab. No.

Intended Use: CSS-1 Cold Mix Spec. No. SN-29(3) --51-72 Date Reported 9-28-81

County: Osceola Proj. No. SN-69(3) --51-72 Contractor Rohlin
FM-72(7) --55-72

Proj. Location:

Agg. Sources: 3/4" Gravel - 28-98-42 Osceola Co.

Job Mix Formula Aggregate Proportions: 100% AAT1-591

JOB MIX FORMULA - COMBINED GRADATION

1 1/2"	1"	3/4"	3/8"	3/8"	#4	#8	#16	#30	#50	#100	#200
		100	95	87	71	58	45	29	14	8.2	6.5
Tolerance											

Asphalt Source and Approximate Viscosity	Algona - CSS-1 (67.3% Residue)	
% Total Emulsion in Mix	5.5	6.5
Number of Marshall blows	50	50
Marshall Stability - Lbs.	2320	2825
Flow - 0.01 in.	16	15
Sp. Gr. By Displacement (Lab. Dens.)	2.03	2.07
Bulk Sp. Gr. Comb. Dry Agg.	2.634	2.634
Sp. Gr. Asph. @ 77 F.	1.020	1.020
Calc. Solid Sp. Gr.	2.42	2.39
% Voids - Calc.	16.2	13.3
Rice Sp. Gr.	5.5% water added to agg. before testing	
% Voids - Rice	mixing Temp. 130°F.	
% Water Absorption - Aggregate	Cured 16 hrs. @ 130°F.	
% Voids in the Mineral Aggregate	Molding Temp. 130°F.	
% V.M.A. Filled with Asphalt	Testing temp. 77°F.	
Calculated Asph. Film Thickness (Microns)	--	--
	27.2	26.5
	40.3	49.7
	8.6	10.3

A Content of 7.0% CSS-1 or less is recommended to start the job.

IOWA DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION
(MATERIALS DEPARTMENT)
ASPHALT CONCRETE MIX DESIGN
AMES LABORATORYAsph. Mix Design
SN-29(3)--51-72
SN-69(3)--51-72
FM-72(7)--55-72, Osceola
J. Bump, Schwarting
D. Jordison, R. Shelquist
L. Zearley, RohlinMix, Type and Class: Type B Class 2 Size 1/2" Lab. No. ABD1-162Intended Use CSS-1 Cold Mix Spec. No. SN-29(3)--51-72 Date Reported 9-28-81County: Osceola Proj. No. SN-69(3)--51-72 Contractor Rohlin
FM-72(7)--55-72

Proj. Location: _____

Agg. Sources: 1/2" gravel - 28-98-42 Osceola Co.Job Mix Formula Aggregate Proportions: 100% AAT1-592

JOB MIX FORMULA - COMBINED GRADATION

1 1/2"	1"	3/4"	3/8"	3/8"	#4	#8	#16	#30	#50	#100	#200
		100	98	90	69	56	42	26	14	8.7	7.3
Tolerance											

Asphalt Source and Approximate Viscosity	Algona - CSS-1 (67.3% Residue)	
% Asph. In Mix	5.5	6.5
Number of Marshall blows	50	50
Marshall Stability - Lbs.	2190	2392
Flow - 0.01 In.	17	22
Sp. Gr. By Displacement (Lab Dens.)	2.03	2.03
Bulk Sp. Gr. Comb. Dry Agg.	2.641	2.641
Sp. Gr. Asph. @ 77 F.	1.020	1.020
Calc. Solid Sp. Gr.	2.43	2.39
% Voids - Calc.	16.4	15.2
Rice Sp. Gr.	5.5% water added to agg. before mixing	
% Voids - Rice	Mixing Temp. 130°F.	
% Water Absorption - Aggregate	Cured 16 hrs. @ 130° F.	
% Voids in the Mineral Aggregate	Molding Temp. 130°F.	
% V.M.A. Filled with Asphalt	Testing Temp. 77°F.	
Calculated Asph. Film Thickness (Microns)	8.4	10.0

A Content of 7.0% CSS-1 emulsion is recommended to start the job.

IOWA DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION
(MATERIALS DEPARTMENT)
ASPHALT CONCRETE MIX DESIGN
AMES LABORATORYAsph. Mix Design
SN-29(3)--51-72
~~SN-69(3)--51-72~~
FM-72(7)--55-72; Osceola
J. Bump, Schwarting
R. Shelquist, D. Jordison
L. Zearley, Rohlin
Lab. No. ABD1-165B

Mix, Type and Class: Type B Class 2 Size: 3/4"

Intended Use: Cold-Mix Spec. No. SN-29(3)--51-72 Date Reported 9-28-81

County: Osceola Proj. No. SN-69(3)--51-72 Contractor Rohlin
FM-72(7)--55-72

Proj. Location:

Agg. Sources: Aggregate From roadway after milling and addition of new aggregate

Job Mix Formula Aggregate Proportions: 100% ABC1-293 (Contains 3.0% Asphalt)

JOB MIX FORMULA - COMBINED GRADATION

1 1/2"	1"	3/4"	3/8"	3/8"	#4	#8	#16	#30	#50	#100	#200
		100	94	86	66	50	38	26	15	11	9.2
Tolerance											

Asphalt Source and Approximate Viscosity	CSSL-H	Emulsion
% Asph. In Mix	6.5	7.2
Total Emulsion Added	5.0	6.0
Number of Marshall blows	50	50
Marshall Stability - Lbs.	680	650
Flow - 0.01 in.	21	19
Sp. Gr. By Displacement (Lab Dens.)	2.11	2.10
Bulk Sp. Gr. Comb. Dry Agg.	2.65	2.65
Sp. Gr. Asph. @ 77 F.	1.02	1.02
Calc. Solid Sp. Gr.	2.39	2.37
% Voids - Calc.	11.8	11.3
Rice Sp. Gr.		
% Voids - Rice		
% Water Absorption - Aggregate	--	--
% Voids in the Mineral Aggregate	25.5	26.5
% V.M.A. Filled with Asphalt	53.7	57.1
Calculated Asph. Film Thickness (Microns)	9.0	10.0

Emulsion & Agg. mixed at room temp. - Mixture Cured 20 hrs. at room Temp. and compacted at room Temp.

SIGNED: 

(TESTING ENGINEER)

IOWA DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION
(MATERIALS DEPARTMENT)
ASPHALT CONCRETE MIX DESIGN
AMES LABORATORYAsph. Mix Design
SN-29(3)--51-72
SN-69(3)--51-72
FM-72(7)--55-72; Osceola
J. Bump, Schwarting
D. Jordison, R. Shelquist
L. Zearley, Rohlin
Lab. No. ABD1-165AMix, Type and Class: Type B Class 2 Size 3/4" Lab. No. ABD1-165AIntended Use: Cold-Mix Spec. No. SN-29(3)--51-72 Date Reported 9-28-81County: Osceola Proj. No. SN-69(3)--51-72 Contractor Rohlin
FM-72(7)--55-72

Proj. Location: _____

Agg. Sources: Aggregate from roadway after milling and addition of new aggregateJob Mix Formula Aggregate Proportions: 100% ABC1-293 (Contains 3.0% Asphalt)

JOB MIX FORMULA - COMBINED GRADATION

1½"	1"	¾"	½"	3/8"	#4	#8	#16	#30	#50	#100	#200
		100	94	86	66	50	38	26	15	11	9.2
Tolerance											

Asphalt Source and Approximate Viscosity	MC-800		SC-800		HFMS-2 Emulsion	
% Asph. In Mix	4.9	5.25	5.5	6.0	6.5	7.2
Total Emulsion or cutback Added	2.5	3.0	2.5	3.0	5.0	6.0
Number of Marshall blows	50	50	50	50		
Marshall Stability - Lbs.	680	515	650	640	540	460
Flow - 0.01 in.	21	23	20	19	19	19
Sp. Gr. By Displacement (Lab Dens.)	2.02	2.08	2.06	2.07	2.14	2.15
Bulk Sp. Gr. Comb. Dry Agg.	2.65	2.65	2.65	2.65	2.65	2.65
Sp. Gr. Asph. @ 77 F.	1.00	1.00	1.00	1.00	1.02	1.02
Calc. Solid Sp. Gr.	2.45	2.44	2.43	2.41	2.39	2.37
% Voids - Calc.	17.6	14.7	15.2	14.2	10.6	9.2
Rice Sp. Gr.						
% Voids - Rice						
% Water Absorption - Aggregate	--	--	--	--	--	--
% Voids in the Mineral Aggregate	27.5	25.6	26.5	26.6	24.5	24.7
% V.M.A. Filled with Asphalt	35.9	42.6	42.7	46.7	56.8	62.6
Calculated Asph. Film Thickness (Microns)	6.6	7.1	7.5	8.2	9.0	10.0

Cutbacks heated to 160°F before mixing with Agg. @ room Temp. Emulsion & agg. mixed at room temp. - mixture cured 20 hrs. at room temp and compacted @ room temp.

SIGNED: _____

TESTING ENGINEER

Appendix E
Asphalt Penetrations and Viscosities

PENETRATION/VISCOSITY TEST RESULTS

Extracted Binder From 3/4" Mixes

<u>Asphalt</u>	<u>Penetration</u>	<u>Absolute Viscosity</u>
AC-5	126	891
MC-3000	148	763
SC-800	-*	-*
HFMS-2	133	767
CSS-1	78	1610

Extracted Binder from 1/2" Mixes

<u>Asphalt</u>	<u>Penetration</u>	<u>Absolute Viscosity</u>
MC-3000	139	777
SC-800	-*	-*
HFMS-2	108	1050
CSS-1	83	1490

Extracted Binder from Road Mix

<u>Asphalt</u>	<u>Penetration</u>	<u>Absolute Viscosity</u>
Existing Asphalt	40	11,630
MC-800	68	2,840
SC-800	145	682
HFMS-2	64	3,640
CSS-1	56	3,860

*To soft to test

Note: Penetration at 77°F. .100 gms., 5 sec.

Absolute Viscosity at 140°F., 300 mm. HG(Poises)

Appendix F
Density Test Results

Section No.	Binder	Lab Density ¹	Field Density ²	Percent Field Voids
1	AC-5	2.39	2.26	7.4
2	MC-3000	2.22	2.07	16.6
3	HFMS-2	2.22	2.06	17.6
4	HFMS-2	2.11	2.09	13.0
5	CSS-1	2.11	2.03	15.3
6	CSS-1	2.21	1.96	22.2
7	MC-3000	2.24	2.06	16.6
8	MC-800	2.00	1.90	21.6
9	SC-800	2.03	1.93	20.2
10	SC-800	2.29	2.09	15.1
11	HFMS-2	2.25	2.07	18.3
12	AC-5	-	-	-
13	MC-3000	2.22	2.16	13.6
14	SC-800	2.36	2.22	11.3

1. Lab densities for section 4, 5, 8 and 9 by Modified Proctor.

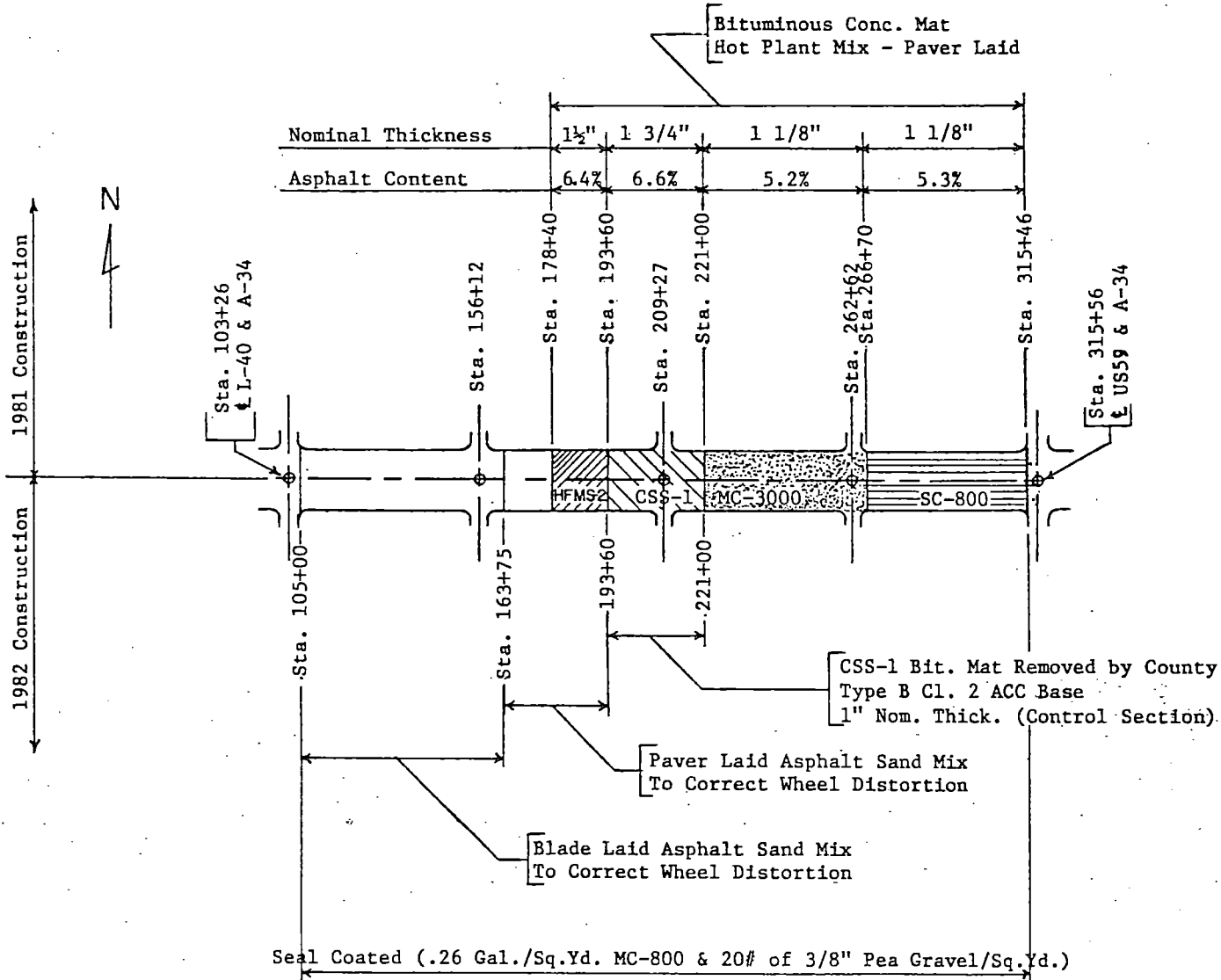
2. Field densities for section 1 by cores.

Field densities for other section by nuclear gauge.

Appendix G
Maintenance Work
and
Seal Coat Construction

PROJECT FM-72(7)-55-72
RESEARCH PROJECT NO. HR229
COUNTY ROUTE NO. A-34

Note: The Type B and Bituminous Mats are 1/2" Gravel Mixes.



PROJECT SN-69(3)--51-72
RESEARCH PROJECT NO. HR229
COUNTY ROUTE NO. A-46

Note: The Type B and Bituminous Concrete Materials are 3/4" Gravel Mixes.

