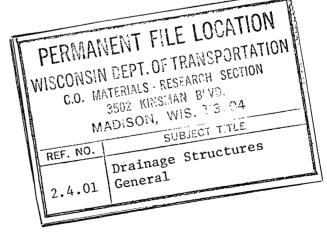
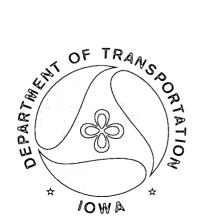


Progress Report Project HR-509



Highway Division May 1980



80-2

IOWA DEPARTMENT OF TRANSPORTATION

Director

Raymond Kassel

Vernon J. Marks

Materials-Research

D.O.T. Soils Unit

RECEIVEI

JUL 11 1980

Progress Report HR-509, "Use of Longitudinal Subdrains in the 3R Program"

Attached is one copy of the research report noted above. The research involved the installation of edge subdrain on 14 miles of I-80 in Poweshiek County. The objective was to alleviate pumping and faulting of the jointed pcc pavement. After periods of rainfall, there is substantial flow from the outlets. At this time, there is some data that would indicate a reduction in the rate of faulting but the data is not adequate to support a conclusion.

VJM/jc Attachment cc:attachment

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June 26, 1980

HR-509

PROGRESS REPORT FOR PROJECT HR-509

USE OF LONGITUDINAL SUBDRAINS IN THE 3R PROGRAM

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VERNON J. MARKS RESEARCH ENGINEER 515/296-1447

IOWA DEPARTMENT OF TRANSPORTATION HIGHWAY DIVISION OFFICE OF MATERIALS AMES, IOWA 50010

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APPENDIX

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USE OF LONGITUDINAL SUBDRAINS IN THE 3R PROGRAM

INTRODUCTION AND PROBLEM STATEMENT

Construction of the interstate highway system began in 1956. This U.S. network of highway consists of more than 41,000 miles with 790 miles in Iowa. There have been many benefits of the controlled access roadway, but probably the most significant is the improved safety for the motorist.

In Iowa, we have always endeavored to utilize quality locally available materials in our construction using the most economical or cost effective methods. Obviously when the effort is to build a cost effective system, there will be some portions of the network that will not perform as well as expected. In the design of our interstate, the main consideration for base construction under the pavement was structural capacity. The material was dense graded with the aim of supporting the pavement and distributing the load as it is transferred to the underlying grade. The drainage characteristic of the base was apparently not given adequate consideration. On jointed portland cement concrete (pcc) pavement, the water that is trapped immediately beneath the pavement causes severe problems. The traffic causes rapid movement of the water resulting in the hydraulic

pressures or "pumping" (movement and redeposit of base fine material) resulting in faulting between individual slabs.

Recognizing the need for maintaining this large national highway network, the Federal Highway Administration has initiated a funding program for resurfacing, restoration and rehabilitation (3R). Many miles of the system are more than 20 years old and in need of major maintenance. This new 3R Program necessitated a complete inventory of the Iowa interstate system to establish priorities and to identify those sections in need of immediate remedial treatments.

PROJECT LOCATION

One section of highway that was identified by the 3R inspection team was I-80 in Poweshiek County from Iowa 146 to the Brooklyn Interchange (13.6 miles). This pavement is a 10 inch thick mesh reinforced pcc with doweled transverse joints at a 76.5 foot spacing. The pavement was placed on a relatively dense graded 4 inch crushed limestone "granular subbase". The inspection team noted that many transverse joints were faulted. Edge pumping was evident along most of this section with damage to the shoulders. The shoulders had settled ½ to 1 inch below the edge of pavement. The pavement was constructed in 1964 and has a traffic volume of over 14,000 vehicles per day with about 4,000 of these being trucks. Many full depth patches were placed and pressure relief joints cut in the fall of 1977.

OBJECTIVE

The objective of this evaluation is to determine if longitudinal subdrains are effective in preventing or reducing pumping, faulting and related deterioration.

SUBDRAIN DESIGN

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The subdrain design utilized 6" diameter commercially available slotted polyethylene corrugated agriculture tubing complying with ASTM F-405. It was placed continuously adjacent to the outside edge of pavement for the entire 14 miles of the project. Subdrain was placed adjacent to the inside edge of pavement 500' either direction from the low point of vertical curves. The detailed design is given in Appendix Al. The gradation of the porous backfill is:

<u>Sieve Size</u>	<u>% Passing</u>
3/4"	100
1/2"	95 - 100
3/8"	50 - 100
#4	15 - 50
#8	0 - 5

A new detailed design (Appendix A2) has recently been developed with modifications to alleviate initial problems.

CONTRACT

The project was let on June 20, 1978, with a starting date of August 14, 1978. The successful low bidder was

- [...

Manatt's Incorporated of Brooklyn, Iowa. The total bid (Appendix B) was \$1,213,872. which included 159,347 lineal feet of subdrain at \$5.03 per lineal foot. The work period was set at 100 days.

CONSTRUCTION

For construction, the interstate traffic was restricted to one lane with appropriate signing and traffic control. Installation of the subdrain began on September 11, 1978. The contractor established a very efficient equipment train to accomplish the subdrain installation. The contractor's goal was to place 3000 lineal feet of subdrain per day. This was a new operation for the contractor and as with all new operations, there is a learning period. The first day only 240 feet were placed with about 700 feet the second day. On September 25, the contractor reached his goal of 3000 feet in one day.

The first operation utilized a Vermeer T-600C (Figure 1) trencher to cut the one foot wide, 2 foot deep trench. Initially, this trencher was equipped with a disc cutter wheel (Figure 2) to aid in maintaining proper alignment. Later, this was of questionable benefit. The trencher cut very neat side walls and alleviated some initial concern that chunks might be torn from the asphalt concrete shoulder surfacing. It was, however, relatively severe to the trencher's cutting teeth.

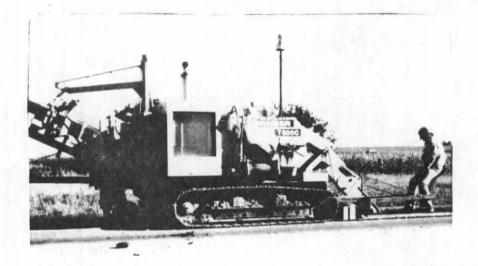


Figure 1: Vermeer T-600C Trencher

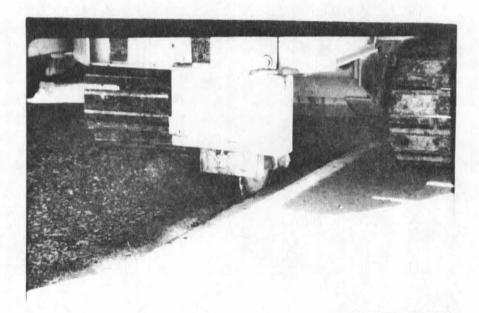


Figure 2: Disc Cutter Wheel to Aid in Alignment

A side elevator of the trencher deposited the material directly into trucks (Figure 3).

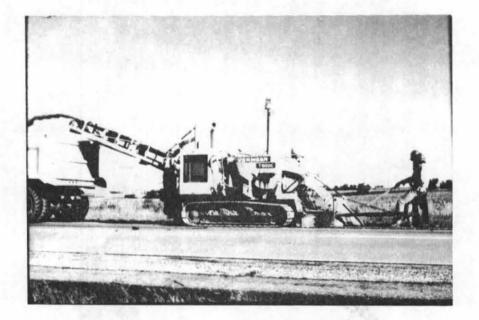


Figure 3: Loading Excavated Material.

Polyethylene tubing deteriorates if exposed to sunlight and therefore, a note on the plans required protected storage even though the producer claimed that an additive would protect the tubing for up to six months. The tubing was placed in the trench manually (Figure 4).



Figure 4: Hand Placement of the Tubing

The next operation in the train was the proper placement of the porous backfill material using a Blawknox RW-38 road widener (Figure 5) with a special box attachment. This operation caused the most problems and required special attention. With proper modifications, the tubing was threaded through a guide in the special attachment and the 3" bedding beneath the pipe was achieved. A vibrating pan unit (Figure 6) was attached to the special box for compaction of the porous backfill.



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Figure 5: Blawknox RW-38 Placing Porous Backfill

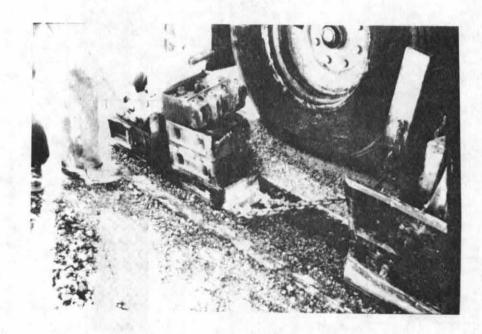


Figure 6: Vibrating Pan Compaction of Porous Backfill

The pavement was then broomed prior to placement of the 6" thick 3/4" type B asphalt concrete shoulder. The asphalt was placed with a second Blawknox RW-38 road widener (Figure 7). The asphalt concrete was compacted with a small 30" vibratory roller. The filled trench was very neat even before the ½" cover aggregate placement (Figure 8).



Figure 7: Placing Asphalt Concrete with Blawknox RW-38

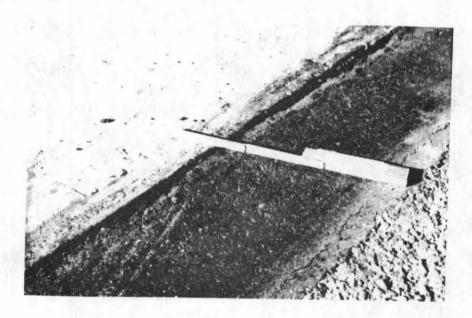


Figure 8: Finished Trench Prior to Cover Aggregate Placement

Preformed polyethylene T's (Figure 9) were used at outlet locations (at 1000' intervals). The porous backfill at the outlet was manually placed. Earth fill was tamped around the RF-22 subdrain outlets (Figure 10).

During construction, water would flow into the open trench and partially fill the new pipe overnight. Following a rain, outlets of completed sections would flow from a trickle to a depth of one to two inches. This was an early indication of their potential benefit.

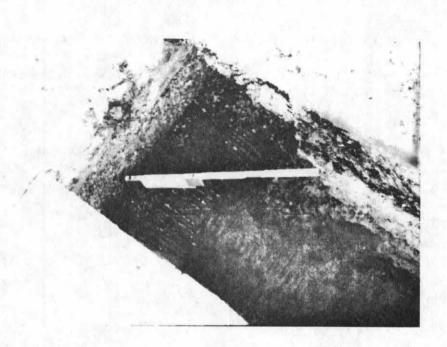


Figure 9: Preformed T for Outlet

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Figure 10: Tamping Earth Fill Around the RF-22 Outlets

The reinforced concrete pipe median drains caused some problem during construction. Some were not deep enough to allow a two foot deep trench. Other had cavities that would allow the loss of porous backfill resulting in subsequent early settlement. Without special treatment, these situations could also lead to future piping along the median drain. The remedy for the problem on this project was to excavate over the median pipe and tack coat the pipe with asphalt cement. Two layers of filter fabric were then placed on the tack coat followed by capping with asphalt concrete hot mix.

Construction was not completed during 1978. Another problem was recognized in the early spring of 1979. The RF-22 outlets froze shut during the winter period. Early spring flow from the subdrains eroded the earth fill around the RF-22 outlet (Figure 11). This problem was solved by carrying the porous backfill the total length of the RF-22 outlet.

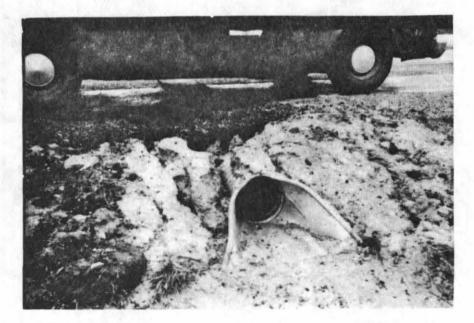


Figure 11: Erosion Around the RF-22 Outlet

SUBGRADE PERCOLATION TESTING

The 4" thick granular subbase material on the Poweshiek project was a crushed limestone with a typical grading as follows:

<u>Sieve Size</u>	<u>% Passing</u>	
1 1/2"	100	, Ma
1"	97	5.N
3/4"	93	* 4
3/4" 3/8"	80	16
#4	74	/
#10	60	
#40	37	
#200	23	

There was some question as to the percolation characteristic of this material. A somewhat crude test was used as a measure of this characteristic. A $4\frac{1}{4}$ " diameter core hole was drilled through the concrete slab taking care to quit drilling quickly after breaking through the slab to avoid disturbance of the granular subbase. The core hole was immediately filled with water. The subsidence was measured at 5 minutes (A). The core hole was refilled and the subsidence measured at 10 minutes (B). In some cases, the core hole was refilled and the subsidence measured at 15 minutes (C). This test was conducted at three locations with the results as follows:

				Reading	
			A	В	С
Sta.	434+70	EB	1-1/2"	1-1/4"	
Sta.	544+20	EB	5-1/2"	4"	3-9/16"
Sta.	323+96	WB	7-7/16	" 6"	6"
Sta.	1793+25	WB	5/8"	1/4"	
	Sta. Sta.	Sta. 544+20 Sta. 323+96	Sta. 544+20 EB	Sta. 434+70 EB 1-1/2" Sta. 544+20 EB 5-1/2" Sta. 323+96 WB 7-7/16	A B Sta. 434+70 EB 1-1/2" 1-1/4" Sta. 544+20 EB 5-1/2" 4" Sta. 323+96 WB 7-7/16" 6"

Dooding

The Jasper granular subbase was a blend of sand-gravel and limestone and is included for comparison. A typical gradation of the blended granular subbase material used in Jasper Co. is:

<u>Sieve Size</u>	<u>% Passing</u>
1"	100
3/4"	94
3/8"	87
#4	83
#8	78
#10	76
#40	39
#60	21
#100	12
#200	8.2

3. R 83

The Poweshiek subbase material has better percolation characteristics than the Jasper subbase. Obviously, better drainage characteristics are desirable in the Poweshiek project.

SUBDRAIN EVALUATION

The flow from the subdrain outlets has indicated their effectiveness. As noted, some flow began immediately after installation. Periodic flow checks have been made. Many of these have been made after periods of rainfall. A summary of those periodic checks is provided in Table I.

TABLE I: SUBDRAIN OUTLET FLOW SUMMARY

Date	5/3/79	8/20/79	8/23/7	9 <u>11/9/79</u>	4/11/80
Amount of Recent Rainfall FLOW: Dry	1.10" 9	4." 12	2." 24	fall 104	 63
Trace Small stream	83	28	65	24	56
(less than 1/8")	10	72	26	0	11
1/8" stream	0	7	4	0	0
1/4" stream	0	10	1	0	0
	10%	12		178	130

It is evident from the values in Table I that the outflow is very dependent on rainfall and subsequent runoff. It is also apparent from the August 20 and 23 results that the decrease in flow after rainfalls is relatively rapid. The 1980 spring rainfall has been substantially below normal.

The Present Serviceability Index (PSI) is a rating scale of pavement condition with 0 being bad and 5 being excellent. The PSI is obtained by combining a riding quality such as the Longitudinal Profile Value (LPV) with a deduction for cracking and patching (C&P) deterioration. The PSI was determined when the project was initiated (9/22/78) and will be determined annually thereafter.

	Subd	rain Pı	coject		ljacent Ne proj	
DATE	LPV	<u>C&P</u>	PSI	LPV	<u>C&P</u>	PSI
9-22-78	3.71	0.74	2.97	3.80	0.66	3.14
6-25-79	3.68	0.78	2.90	3.76	0.70	3.06

From the test results, there is still deterioration and related loss in riding quality on both the pavement included in the subdrain project and an adjacent pavement included in the subdrain project and an adjacent pavement section tested for comparison. There is presently no significant difference with regard to the subdrains.

One specific aim of the subdrains was to eliminate pumping and prevent increase in faulting.

Date	Subdrain Project (Avg. of 62)	Adjacent To The Project (Avg. of 6)
October, 1978	0.18"	0.12"
December, 1979	0.21"	0.18"

Even though the faulting has increased, the test values would indicate that the rate of increase is less than the rate for an adjacent pavement without subdrains. Additional testing will be necessary to verify this trend.

Initially there was concern that an edge rut problem may develop due to subsequent settlement of the trench area. There is no evidence of settlement as of this date.

EVALUATION SUMMARY

Based upon the flow from the outlets observed during periodic checks and evidence of water flow at the outlets, it appears that to date the subdrains are effective in draining the subbase and subgrade. Because of the limited data available at this time, the pavement condition and faulting results are inconclusive.

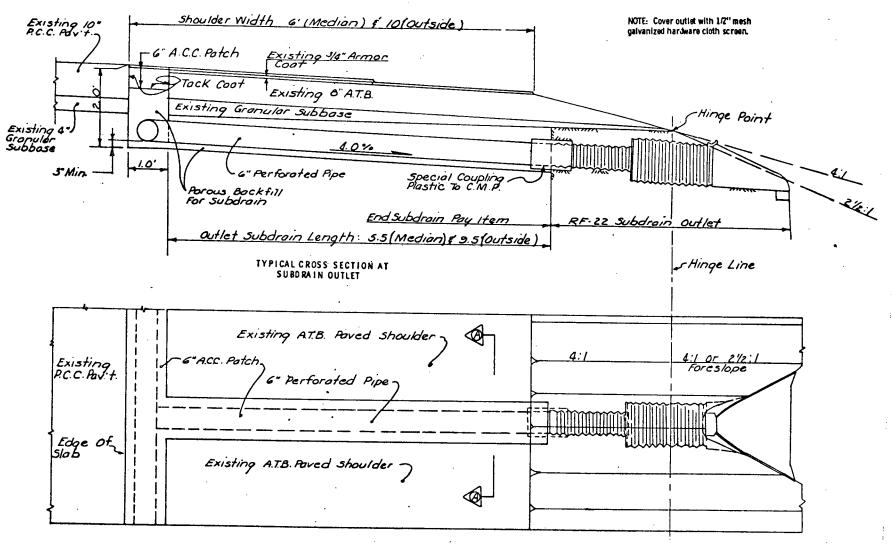
ACKNOWLEDGEMENTS

The project results from the initial promotion and subsequent design by Ralph Britson and Kermit Dirks of the Office of Road Design. Construction was under the direction of John Peters and the Marshalltown Construction personnel. The

contractor, Manatt's Incorporated, is to be complemented for implementing techniques that made construction of the project a success. Robert Choate and the Grinnel Maintenance personnel are obtaining periodic flow measurements. The data on riding quality and faulting is being obtained by Charles Potter and the Special Investigation personnel.

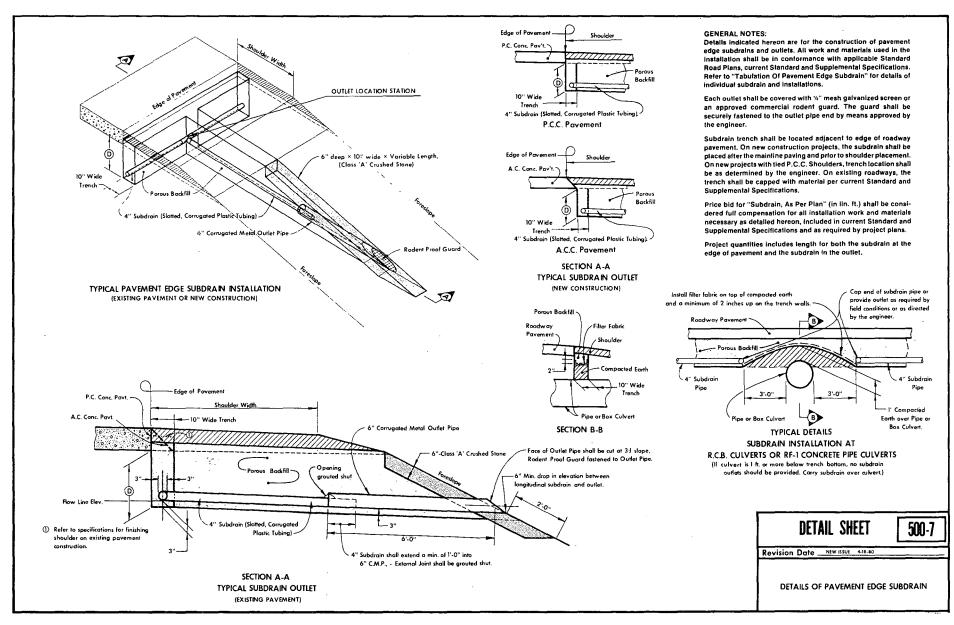
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PLAN VIEW OF SUBDRAIN OUTLET

Appendix A-



Appendix A-2

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